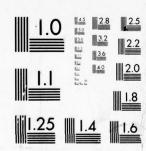


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TECHNICAL REPORT

June, 1977

FUTURE PERFORMANCE TREND INDICATORS:
A CURRENT VALUE APPROACH TO HUMAN RESOURCES ACCOUNTING

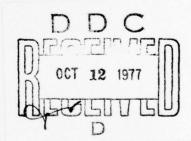
REPORT IV

AN EXAMINATION AND EVALUATION OF THE STATISTICAL MODEL

By:

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This report uses predictive relationships between the Survey of Organizations and measures of organizational effectiveness established in earlier reports (Pecorella & Bowers, 1976a, 1976b, 1977) to develop the formal equations, including parameter values, to be used in the value attribution phase. Preliminary to this a series of issues arising from the theoretical and statistical bases of the current value approach are examined. These include: characteristics of variables to be included in the model, assumptions required for prediction of future performance, extension of the univariate methodology to the multivariate case, and the consequences of applying the methodology to this particular data file, for example, standardization of variables and elimination of outliers. A summary of previous and current analyses is also provided. A particular issue is how well the assumptions underlying the multivariate model are met in this particular data file. Analyses show there is no reason to believe the assumptions of multivariate linearity and normality are not met. Other analyses show that one cannot significantly reduce the number of predictor variables in the model. It is concluded that the presented model is appropriate, and the data set is ready to begin the value attribution steps.

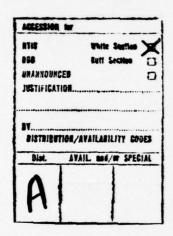


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INTRODUCTION

Organizations have two systems of resources: the technical system which includes the physical plant, available knowledge and techniques, inventories, financial investments, etc., and the human system which includes not only the individuals who are part of the organization, but their skills, knowledge, established relationships and motivation to accomplish the organization's goals. Managers are becoming increasingly aware of the necessity to optimally utilize both resource systems. The variety of techniques, ranging from accounting to industrial engineering and systems analysis, that focus on fuller utilization of the organization's physical, technical and financial resources are well known. Information systems which provide knowledge necessary for fuller utilization of an organization's human or social system are in a relatively primitive state. The purpose of the present study is to explore and demonstrate a method for providing this type of information.

While Brogden and Taylor suggested as early as 1950 the development of indices measuring the value of an employee to an organization, it has not been until recently that much activity has taken place. Presently, there are three substantially different approaches to what has become known as human resources accounting.

(1) The "Incurred Cost" method--measuring the amounts already invested in the human organization (Brummet, Pyle, & Flamholtz, 1968; Pyle, 1970a, 1970b).

- (2) The "Replacement Cost" method--estimating the cost of replacing the organization's human resources (Flamholtz, 1969).
- (3) The "Present Value" method--estimating the future productive potential of today's human resources (Likert, 1967; Likert, Bowers, & Norman, 1969; Likert & Bowers, 1973).

The purpose of the present study is to demonstrate the appropriateness and the feasibility of the "Present Value" technique. Also called a current value approach, its purpose is to predict the future productive capacity of the organization based upon the current assessment of human resources. The study has two highly related, but sequential parts. The first phase examined the relationship between organizational effectiveness and measures of the human organization. This analysis included both simple and multiple correlations, and investigation of the time lag between the causal and intervening variables. These results are provided in the work of Pecorella and Bowers (1976a, 1976b, 1977). They were able to establish the existence of a significant relationship between the human variables as measured by the Survey of Organizations (SOO) and the two effectiveness measures, total variable expense (TVE) and absenteeism (ABS). This analysis was based on data from several different organizations with different technologies and included investigation of the relationships within these organizations as well as for the entire group. Additionally, the effectiveness measures were examined across time to see how the relationship to the human variables changed over time. The results show a strongly similar pattern of relationships within organizations and a definite time lag effect which produces the strongest relationships seven to ten months after the measurement of

the human variables. The next strongest relationship was found at the time surrounding the measurement of the human variables.

The second phase of the study involves the use of the observed relationships between the SOO and organizational effectiveness measures to demonstrate the current value methodology. [This approach is also termed Future Performance Trend Indicators (FPTI) since it involves the prediction of future organizational performance from current indicators of the state of the human organization.]

This report presents and examines in detail the technical and statistical implications of operationalizing a multivariate version of Future Performance Trend Indicators. First, some theoretical considerations of the current value model will be discussed. This will be followed by an extension of the univariate model to a multivariate situation. Next, the interplay between the current value methodology and the characteristics of the data file will be discussed. Finally, the mathematical model selected to estimate the FPTI will be presented. The assumptions underlying the model and how well they are met will be examined, as will the selection of an efficient set of predictors which are consistent across time. The next report will include the value attribution using the equations developed herein and a test, where sufficient data exists, of the assumptions that the predictor-criterion relationship estimated at one point in time is an adequate estimate of that same relationship at a subsequent point in time.

THE CURRENT VALUE METHOD

The conceptual and statistical bases of the current value methodology have been discussed elsewhere (Likert, 1973; Likert & Bowers, 1973; Bowers & Pecorella, 1975). However, it seems appropriate to review certain features implicit in this technique as applied herein to develop FPTI. Some theoretical and conceptual issues will be discussed followed by an extension of the univariate statistical procedures to the multivariate case.

Theoretical Issues

One of the distinguishing characteristics of FPTI is the prediction of future performance based on current knowledge. If this is to be done, several characteristics of the nature of the relationship between the predictor and criterion variables must be determined. This relationship is established by measuring the predictor variables at some point in time (T_0) and then measuring the criterion variables at one or more subsequent points in time $(T_0+1, T_0+2,...T_0+k...T_0+t)$. The nature and extent of the relationship between the predictors at T_0 and the criterion at T_0+k , etc., are then established using an appropriate statistical methodology. A different equation for each value of k is assumed necessary. In order to make predictions the predictor variables are measured at some time subsequent to T_0 , say T_0 , and these values are then used to predict the state of the criterion variable at times $T_0'+k$. To do this it is assumed that the nature of the relationship between predictor and criterion is invariant from T_o +k to T_o +k. In other words, we assume a constant relationship between the measurement of the human organization at some point in time and the measurement of organizational

effectiveness taken at a fixed subsequent time. As evidenced by the findings of Pecorella and Bowers (1977) in their analysis of time lag effects, it is important that the FPTI developed acknowledge the change in the predictive relationship from T_0+i to T_0+k . Thus we are not assuming a constant predictor-criterion relationship for the time periods between the collections of the predictive data.

The purpose of FPTI is to provide input about the human system to management information systems. With this in mind, it makes sense that only those costs which can be affected by the predictors would be included. Thus, variable, not fixed, costs (as in Total Variable Expense) must be used as criteria regardless of whether these costs are computed on a unit basis (Likert & Bowers, 1973) or in some other manner. Furthermore, it would seem useful to include as predictors only those variables which the organization can influence. While general economic conditions may affect turnover, any given organization has little influence on these conditions. Thus, one would not expect a change in organizational effectiveness to be effected through the impact of organizational practices on general economic conditions, and the subsequent effect on turnover since the initial impact on economic conditions is generally quite low. The conclusion is that predictors selected should be at least potentially subject to organizational influence and the criteria should be variable costs which can be impacted by changes in employee behavior.

An exception to these general guidelines for selection of predictors is suggested by the above example of the influence of external economic conditions on turnover. It may be desirable to include as predictors certain variables which, while not subject to organizational influence, modify the nature of the relationship between the criterion and those predictor variables subject to organizational influence. If these modifying variables are to be included, however, care must be taken when attributing value to changes in the state of the human organization to include changes in value attributable only to causal variables and not to the modifying variables which are only indicative of the changed relationship between the causal variables and the criterion. An alternative to including these modifying variables in the equation would be to develop a set of equations for different combinations of values on these modifying variables. This is essentially the approach herein with regards to the modifying variable "time since administration of the SOO." Different equations are developed to describe the SOO-criterion relationship for different periods of time subsequent to the S00 administration.

There are two issues which are somewhat related to the one above: the level at which phenomena are measured and the theoretical model relating the measured dimensions of the human system to changes in organizational effectiveness. As stated by Pecorella and Bowers (1976) and by Mirvis and Lawler (1977), a causal model where links between the predictors and the criterion are known is desirable for accurate prediction. Mirvis/ Lawler prefer a model which operates at the individual level. Attitude change is seen as leading to individual behavior change which leads to changes in organizational costs. What is omitted are the conditions subject to organizational control which lead to the attitude change. In the model used herein,

In the present study it was found that inclusion of certain structural variables, e.g., organizational size, permitted an increase in the ability to predict ABS. An investigation of two such variables is presented in Section 4, after the data set and the mathematical model have been discussed.

organizational conditions are viewed as leading to behavior change both directly and via attitude change. A related difference is that the present model is concerned with changes in the behavior of the group, not of the individual, even though the measures of group behavior may be computed by aggregating individual level measures. The necessity of aggregating individual measures to arrive at group or higher level measures does not invalidate the group concepts. The issue is not the arithmetic of score calculation but rather the researcher's theoretical perspective and its ability to explain what causes the observed phenomena. It seems unnecessary to point out that certain phenomena may be explained at the work group level while others are better explained at individual or organizational levels.

Multivariate Model

Likert (1973) presents the statistical methodology for relating a single measure of the human organization to a measure of organizational effectiveness. Briefly, this consists of (1) computing the Pearson product moment correlation between the measures, (2) converting both measures to standard scores $(\frac{Z_X = X - \overline{X}}{SD})$, (3) multiplying the standard score change in the predictor measure $(\frac{Z_X - Z_X}{SD})$ by the correlation coefficient to arrive at the predicted standard score change in the cost measure $(\Delta \widehat{Z}_y)$. This change is then converted to raw score form by multiplying it by the standard deviation of the Y scores. Mathematically:

X = human organization predictor score at time 1.

X' = human organization predictor score at time 2.

Y = actual criterion score at time 1+k

Y' = actual criterion score at time 2+k

 \hat{Y} = predicted Y score

 $\frac{Z}{X} = \frac{X - \overline{X}}{\overline{SD}_{X}} = \text{standardized predictor score}$

 $\frac{Z}{y} = \frac{Y - \overline{Y}}{\overline{SD}_y} = \text{standardized criterion score}$

 $\Delta X = X - X \qquad \Delta \hat{Y} = \hat{Y} - \hat{Y}$

 $\Delta Z_x = Z_x - Z_x \qquad \Delta \hat{Z}_y = \hat{Z}_y - \hat{Z}_y$

 r_{xy} = Pearson product moment correlation between X and Y.

 B_0 = regression constant

 B_1 = regression weight for X.

 $\hat{Y} = B_0 + B_1 X \qquad (1)$

 $\hat{Z}_{y} = r_{xy} \cdot Z_{x} \qquad (2)$

 $\triangle \hat{Z}y = r_{xy} \cdot \Delta Z_x \qquad (3)$

 $\Delta \hat{Y} = \Delta \hat{z}_{v} \cdot SD_{v} \qquad (4)$

Equation (1) is the univariate linear regression model in raw score form. Equation (2) is the same model in standard score form. Equation (3) is the calculation of change in the predicted standardized value of Y attributable to change in X. Equation (4) is conversion of the predicted standardized change in Y to raw score change. The conversion to standard scores makes B_0 equal to 0 and B_1 equal to $r_{\rm xy}$ and thus makes the strength of the predictor-criterion relationship more evident. In a multivariate situation, however, the regression weight associated with each predictor will generally not be equal to either the zero order or partial correlation coefficients even if all variables are in standardized form. The regression weight will generally not give the amount of change in \hat{Z}_y for a unit change in standard predictor scores

unless all predictors are orthogonal (Gordon, 1968; Linn, Werts & Tucker, 1971). Therefore, there is generally no advantage to standardizing any of the variables in a multivariate case. Because of the nature of the data peculiar to this study, however, it was necessary to standardize the scores. This is dealt with in the next section.

The multivariate methodology follows directly from the more simple univariate case. Remaining in a raw score format and using a _ to indicate a matrix of scores corresponding to the predictor variables, we have:

$$\frac{\hat{Y}}{\hat{Y}} = \underline{B}_{O} + \underline{B}X \qquad (5)$$

$$\Delta \hat{Y} = \underline{B}\Delta X \qquad (6)$$

$$\Delta \hat{\mathbf{Y}} = \underline{\mathbf{B}} \Delta \underline{\mathbf{X}} \tag{6}$$

where \underline{B}_0 is a constant valued vector.

Equation (5) estimates the relationship between Y and X. Equation (6) applies this relationship to an observed change in \underline{X} , $\Delta \underline{X}$, to arrive at a change in the predicted value of Y. It should be noted that this procedure is algebraically equivalent to computing $\hat{\underline{Y}}$ as the product of \underline{B} and \underline{X} and then computing $\Delta \hat{\underline{Y}} = \hat{\underline{Y}} - \hat{\underline{Y}}$. Mathematically:

$$\frac{\hat{Y}}{\hat{Y}} = \underline{B}_0 + \underline{B}\underline{X} \tag{5}$$

$$\underline{\hat{Y}}^{-} = \underline{B}_{0}^{-} + \underline{B}_{1}^{-} \underline{X}^{-} \tag{7}$$

$$\Delta X = X' - X \tag{8}$$

$$\Delta \underline{\hat{Y}} = \underline{\hat{Y}} - \underline{\hat{Y}} = \underline{B}_{0} + \underline{B} \underline{X} - (B_{0} + \underline{B} \underline{X})$$

Assuming $\underline{B}' = \underline{B}$ and $\underline{B}'_0 = \underline{B}_0$ then:

$$\Delta \hat{\underline{Y}} = \underline{B}(\underline{X}^{-}X) = \underline{B}\Delta \underline{X}. \tag{9}$$

The assumptions $\underline{B}'=\underline{B}$ and $\underline{B}_o=\underline{B}'_o$ are the same as the assumption discussed earlier, namely that the predictor to criterion relationship is the same at T_0 +k as it is at $T_0'+k$. The appropriateness of a multiple linear regression model for the present data file will be discussed in Section 4.

Use of Change Scores

As indicated by previous conceptual discussions (Pecorella & Bowers, 1976a; Likert & Bowers, 1973) and the above statistical explication, the current value methodology rests on the observation of change in causal predictor variables which is then used to estimate a future change in some criterion of employee or work group behavior. Attention to issues in the measurement and analysis of change has increased with its popularity. A change score is defined as the difference between two measurements of the same attribute taken at different points in time. Thus, in the present study $\Delta X = (X^2-X)$ is a change score.

Cronbach and Furby (1970) and Kessler (1977) both list four basic uses of change scores: (1) in the analysis of experimental data, (2) as criterion scores in correlational studies, (3) as indicators of theoretical constructs which cannot be measured directly and (4) to identify exceptional individuals (Cronbach & Furby, pg. 77). They do not, however, address themselves to the use of change scores as predictors of change in a criterion.

It is clear that the problems associated with the computation of change scores will exist regardless of their intended use. These problems center about two issues: (1) the reliability of change scores, and (2) the effects of "regression towards the mean."

As shown in equation (10), the reliability of a change score is a function of its component score (the scores on the attribute at T_0 and again at T_0) reliabilities (R_X & R_{X^-}) and its component score intercorrelations (r_{XX^-}).

$$R_{\Delta X} = \frac{VAR(X)R_{X} + VAR(X')R_{X'} - 2SD(X)SD(X')r_{XX'}}{VAR(X) + VAR(X') - 2SD(X)SD(X')r_{XX'}}$$
(10)

SD = standard deviation

VAR = variance

R = reliability

 r_{XX} = Pearson product-moment correlation between X and X

These effects may be more easily seen if we assume that $VAR(X)=VAR(X^{\prime})$, and $R_{X}=R_{X^{\prime}}$ (Kessler, 1977). Doing so, equation (10) becomes equation (11).

$$\frac{R_{\Delta X}}{2VAR(X) - 2VAR(X)r_{XX}} = \frac{R_{X}-r_{XX}}{1-r_{XX}}$$
(11)

From equation (11) we see that the upper limit of the change score reliability is the reliability of its component scores (if $R_\chi \neq R_\chi$, then the larger of the two is the limit of $R_{\Delta X}$). This is not a surprising result since we would hardly expect the difference between two component scores to be more reliable than the most reliable of the component scores. Equation (11) also demonstrates that as the correlation between X and X´ $(r_{\chi\chi})$ increases, the reliability of their observed difference decreases. This may be seen intuitively if one considers that when $r_{\chi\chi}$ is very high, we would say that X and X´ are almost identical to each other. Any observed difference between two nearly identical quantities will reflect little more than measurement error. Since the difference is our change score, it follows than when $r_{\chi\chi}$ is high, the change score reliability, $R_{\Lambda\chi}$ will be low.

It is interesting to note a potential fallacy here. Test-retest reliability, which is a measure of stability over time, is perhaps the most common conception of component score reliability. Any attempt to measure reliability in this manner while attempting to measure change results in conceptually (and often algebraically) equating R_v and r_{vv} . This necessarily produces low change score reliabilities which can be attributed to low component score reliabilities (if $R_x = r_{xx}$ is low) or to high component score intercorrelations (if $R_x = r_{xx}$ is high). Thus, the reliability of the change scores will inevitably suffer if component score stability (the most common definition of reliability) and change are measured at the same time. The alternative, assuming a decision to use change scores, is to use a measure of reliability other than stability measured at the same time at which change is being measured. In the present study, R is measured by Cronbach's alpha, a measure of internal consistency. Thus, the potential fallacy described above is not of concern here. The change score reliabilities herein, reported in Table 1 along with component score reliabilities and intercorrelations, are necessarily a function of R_x , R_x , and r_{xx} . However, since the definition and computation of component score reliability $(R_x, R_{x'})$ is clearly distinct from that of component score stability over time (r_{xx}) , we are able to obtain generally high reliabilities for both the component and change scores. The figures reported in Table 1 were computed for the 797 work groups which have S00 measures available for T_0 and T_0 . These are the work groups for which change scores will be calculated and value attribution made.

The second problem associated with gain scores is a "regression toward the mean" effect which produces a negative correlation between ΔX and X. Kessler (1977) describes three mechanisms by which this effect occurs

Table 1
SOO CHANGE SCORE RELIABILITIES¹

NDEX	² R _X	2 R _x -	³r _{xx} -	⁴ R _{∆x}
Supervisory Support	.91	.93	.43	.86
Supervisory Goal Emphasis	.83	.89	. 49	.73
Supervisory Work Facilitation	.90	.92	.44	.84
Supervisory Team Building	.91	.93	.49	.84
Peer Support	.85	.88	.33	.80
Peer Goal Emphasis	.80	.82	.36	.69
Peer Work Facilitation	.89	.88	.32	.83
Peer Interaction Facilitation	.89	.90	.35	.84
Human Resources Primacy	.91	.91	.69	.71
Communication Flow	.81	.86	.54	.64
Motivational Conditions	.80	.86	.59	.59
Decision Making Practices	.65	.88	.62	.36
Satisfaction	.84	.89	.51	.73

 $^{^{1}}$ Figures shown are for all work groups with S00 scores at 7 0 and 7 0 (N=797)

 $^{^2{\}rm R}_{_{\rm X}}$ and ${\rm R}_{_{\rm X}}$ are the alpha coefficients for S00 indices measured at T $_{_{\rm O}}$ and T $_{_{\rm O}}$ respectively.

 $^{^3} r_{\chi\chi}$ is the inter-wave correlation of $\rm T_0$ and $\rm T_0^{\prime}$ S00 index scores.

⁴R_{ΔX} is the reliability of the change score $\Delta X (=X^2-X)$ computed as shown on page 11.

and discusses the most popular correction for this the effect. Briefly, this correction involves the use of the residuals of the gain scores after they have been regressed on the T_0 component scores. Thus, the quantity $(\Delta X - \Delta \hat{X})$, where $\Delta \hat{X} = B_0 + B X$, is used as a "residualized" gain score. Both Cronbach and Furby (1970), and Kessler (1977) argue that this correction is of limited or no use.

While the problems inherent in change score computation are fairly well known, their implications for the various uses of change scores are still being actively debated (Kessler, 1977). Furthermore, the debate centers on the four uses of change scores listed above and whether and how they should be corrected; to our knowledge the debate has not yet touched on change scores as used in the present study, i.e., as predictors in a regression equation developed from one wave of the component scores. Given this lack of guidance, our strategy has been to use the raw or uncorrected gain scores $(\Delta X = X - X)$ as opposed to applying one of the various "correction formulae." Our rationale for this is two-fold: first, these correction formulae are shown to be of extremely limited use (Cronbach & Furby, 1970). Second, the current use of change scores does not fall into any of the previously examined purposes and there is no advantage in simply applying a correction formule without an explicit theoretical and/or statistical rationale.

DATA FILE CHARACTERISTICS

The conditions necessary for operationalization of the current value methodology have been enumerated by Likert and Bowers (1973). The extent to which these conditions can be met given the current state of knowledge is further described by Pecorella and Bowers (1976a). Pecorella and Bowers (1976a, 1976b, 1977) have also assessed the extent to which the data used in the present study meet these conditions and concluded this data file does meet the requirements for the development of future performance trend indicators using the current value approach to human resources accounting. Our purpose in this section is to describe the characteristics of the data in order to demonstrate the effect these characteristics have on the analyses and to provide a base from which the necessity and appropriateness of subsequent operations may be considered.

Previous Analyses

A brief review of previous analyses and a discussion of their implications for the development of FPTI is presented here. The analyses themselves and a more complete discussion are presented by Pecorella and Bowers (1976a, 1976b, 1977).

Data File Content

The data file contains two waves of scores from five organizations on 13 predictor variables from the Survey of Organizations (SOO) (Taylor & Bowers, 1972). These two waves of data were collected 11 to 24 months apart.

The file also includes scores on two criterion variables, Total Variable Expense (TVE), an ultimate criterion of organizational effectiveness and Absenteeism (ABS), a penultimate criterion of organizational effectiveness. Each criterion measure was collected from a different subset of four of the five organizations on a monthly basis, though not all months were collected for all organizations.

The 13 SOO indices were selected from 16 possible indices based on their internal consistency and the availability of complete data sets. ABS and TVE were selected from a set of five possible criteria as the ones for which sufficient data across time and across organizations was available. The existence of significant, directionally correct relationships was established by examination of the Pearson product moment correlations between each index and the criterion variables.

TVE measures are available for a total of 19 periods (A-S) covering 38 months and ABS measures are available for 10 periods (A-J) covering 28 months. This report will deal with periods A through I for TVE and A-J for ABS since these periods cover the duration of time (1 year) for which the FPTI's will be developed.

Performance Periods

It was desirable that the performance measure not reflect minor month to month fluctuation while still being capable of showing changes over time. Thus the decision was made to group consecutive months into periods in such a way as to maximize the consistency of the performance measure within each period. The monthly TVE and ABS data from each organization were subject

to a Smallest Space Analysis (Roskam & Lingoes, 1970). The results of the analysis were used to define multi-month performance periods where two criteria had to be met for a group of months to be assigned to a period: first, all months in a period had to be sequential; second, the values for the months had to be located empirically close together in N dimensional space (Pecorella & Bowers, 1976a). The period performance score (TVE & ABS) for each cost center was computed as the mean of that cost center's performance scores for the months included in that period. Thus, a total of 151 and 73 month by organization cells for TVE and ABS were reduced to 56 and 29 period by organization cells for TVE and ABS, respectively. Table 2 shows the resulting number of cases available from each organization for computation of the prediction equation for each TVE and ABS period.

We note that while the periods across organizations are similar the months contained in a period from each organization are not identical. Thus month T_0^{+3} (three months after the first wave of the S00 was administered) in one organization does not necessarily fall in the same period as does month T_0^{+3} for another organization. Also, since the size of periods varies from one to 11 months, it is possible, for example, to have an eight month period in one organization which corresponds to two four month periods in another organization.

One effect of defining performance periods in this manner was seen in the analyses examining the existence and generalizability of the multivariate relationships between 13 SOO indices and the criterion measures of ABS and TVE (Pecorella & Bowers, 1977). Given the hypothesis that this relationship changes as one gets further away in time from the collection of the SOO data, it was desirable to combine the periods from each organization which were similar, if not identical, in their distance from $T_{\rm O}$ (first SOO administration) when computing the regression problems by period across organizations.

Table 2 NUMBER OF CASES BY PERIOD AND ORGANIZATION

TVE	A	æ	S	0	ш	ш	ග	Ŧ	н	
ORGANIZATION II	61	1	61	61	61	1	1	1	1	
III	;	ł	254	254	254	!	1	1	248	
ΙV	}	!	1	29	;	29	!	1	1	
VI	127	127	127	127	127	131	51	51	191	
Total	188	127	442	209	442	198	12	12	409	
ABS	A	В	u	D	ш	ш	5	Ŧ	н	רי
ORGANIZATION I	1	21	21	21	12	12	12	18	18	18
II	1	ł	46	107	46	9/	19	24	;	;
III	254	254	254	;	254	254	254	248	248	248
VI	1	114	114	1	114	1	1	1	1	1
Total	254	389	435	128	435	351	336	290	566	566

Therefore, the alphabetic labels assigned to each period were assigned so as to maximize the correspondence of the distances from T_0 of periods assigned the same labels. As a result, some periods are assigned two labels. Additionally, in any given organization two consecutive periods will always be labelled sequentially but not necessarily consecutively. This is demonstrated in Pecorella and Bowers (1977, pg. 22). The major implication of this feature is in the designation of which period regression equation will be used to predict performance for a given month. This will be discussed in the next report where changes in performance predicted by period will be converted to predictions by month.

Imputation

S00 data were collected by work group and criterion data were collected by cost center. Each cost center consists of one or more work groups. In order to relate the state of the organization as measured by the S00 to organizational effectiveness the cost center criterion scores were assigned to all work groups in the cost center. This imputation process provides a relatively large N (equal to the number of work groups) for analysis. However, it also reduces criterion variance by causing an artificially large number of tied scores. As a result, a conservative limit is placed on the size of the multiple correlation between the S00 indices and the criteria.

The alternative to imputation would have been to assign the average of the work group SOO scores to the cost center and perform the analyses at the cost center level. As indicated by the imputation rates (Pecorella & Bowers, 1977, pg.20), however, this would have drastically reduced the number of cases below the number necessary for this analysis. Therefore the imputation alternative was selected, despite the minimizing effect it has on the size of R.

Current Analyses

Standardization

As previously described, the data file contains predictor and criterion scores from five different organizations which for the purposes of this study are merged together to represent one hypothetical organization (Pecorella & Bowers, 1976a). In order to do this the relationships between predictors and criteria and the measures themselves must be in some sense comparable. This requirement will be discussed separately for criterion and predictor measures.

Criterion Standardization

The definitions of TVE and ABS have been listed previously for each organization (Pecorella & Bowers, 1977, p. 19). While not identical, each of these measures is similar to the same measure for the other organizations. However, the different bases from which these measures were computed and the different metrics used for each do indicate that these measures are not directly comparable. In order to merge these different score distributions into one data file, therefore, each organization's scores are standardized against its own distribution. This transforms each organization's 'scores to Z scores and allows comparison of the measures from the different organizations by giving them equal means (\overline{Z} =0) and standard deviations (SD=1) and eliminating their units of measurement. The necessity of performing this transformation raises the question of whether the transformation computed for each organization will be done within each performance period or across all performance periods.

Theoretically one would want to standardize within periods if each period's scores were sampled from different distributions and across periods if each period's scores were sampled from the same distribution. While it would be possible to test the null hypothesis (H_0) that the scores for each period are all drawn from the same distribution, the results would be of little practical use. Failure to reject the H_0 using a test of unknown power would say nothing about the probability of error in accepting the H_0 . Rejection of the H_0 would not tell us which periods' scores were sampled from different distributions and which from the same distribution. Any post hoc analysis would most likely indicate standardization across some periods and within others. When compounded by the merging of four organizations together, the resulting standardization scheme would be so intricate as to be unmanageable and senseless in practical terms.

Returning to the practical choice of standardizing either within or across periods (and not some combination thereof), it can be seen that standardizing within assumes a maximum number of different performance score distributions, i.e., each one different from all others. Where the performance scores of two or more periods are actually drawn from the same distribution, standardization within will provide results identical with standardization across those periods except for the effects of sampling error on the mean and standard deviation of the performance scores for the different periods. Thus standardization within was the method selected by Pecorella and Bowers (1977) to compute the regression of the performance measures on the SOO indices.

Computation of the current value of future performance will require that predicted changes in performance made in standard score form be converted to raw scores. This conversion will be accomplished using the same linear transformations that were used to standardize the performance data originally. If the scores are standardized within periods, a different transformation will be required for each period-organization cell and no transformation will be available to convert predicted standard scores to raw scores for those period-organization cells where the performance data is missing.

As shown in Table 2, there are a total of 30 period by organization cells where the predicted change in standard score could not be converted to a raw score for inclusion in the value attribution phase. Standardization across periods will result in a single transformation being used for each organization (on each performance measure). This transformation will thus be available to convert all predicted standard score changes to predicted raw score changes, regardless of whether criterion data was originally available for that particular period by organization cell. Thus the original requirement for standardization plus the problem of missing data indicates that standardization of criterion data across periods is preferable in this study.

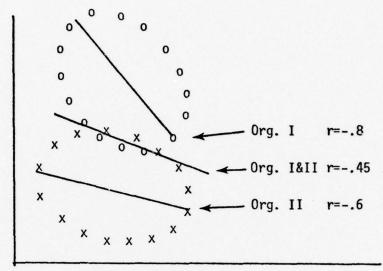
The effect of the two different methods of standardization on the multiple R of the regression equations also requires exploration. Since standardization of the performance scores, whatever the method, is a linear transformation the particular method selected (within or across) will have no effect on the R for the prediction equation as long as only one organization's data is used in computing the equation. However, when two or more organizations

are merged to compute the prediction equation, standardization within each organization will result in a different linear transformation being applied to each organization's scores. In the multiple organization case the shift from one standardization scheme to the other does change the R's for the equations as shown in Table 3. This effect is best illustrated graphically. In figure 1 a simplified case with two organizations and only one predictor variable is depicted. In Figure 1A the predictor-criterion r's for organizations I and II are -.8 and -.6 respectively, and the r for the merged data is -.45. In Figure 1B a different linear transformation has been applied to each organization's criterion data as indicated by the change in the slopes of the individual regression lines. Since this does not effect the variation about each individual regression line, the r's for the individual organizations remain the same. However, when considered as one data set the variation about the regression line for the merged data has clearly changed. In this example variation about the regression line for the merged data in Figure 1B is reduced and the absolute value of r is increased from .45 to .55. Obviously, the net change will depend upon a number of factors including the N's for each organization and the specific transformations employed. The point is that there is a change. As can be seen by comparing R_{μ} and R_{a} in Table 3, in the present study the changes in the positive direction are of greater magnitude and frequency than those in the negative direction.

Figure 1

Effect of Different Standardization Procedures

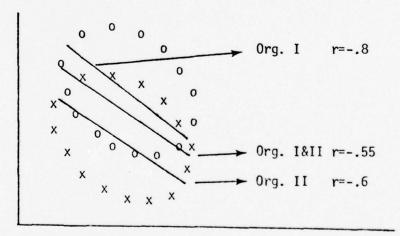




Predictor

A. Standardization Within

Criterion



Predictor

B. Standardization

Table 3
EFFECT OF CRITERION STANDARDIZATION ON MULTIPLE R

11					TVE					
	А	В	ပ	O	ш	L	5	=	-	
Z	188	127	442	509	442	198	51	51	409	
2	. 46	.38	.34	.27	.27	.40	.57	.49	.26	
۵	10.	.16	.01	.01	10.	10.	.23	.58	.00	
A _a	.51	.34	. 39	.25	.27	.52	.57	.49	.28	
۵	10.	.35	.01	.01	.01	10.	.23	.58	.01	
					ABS					
	А	В	υ	0	Ш	L	5	=	-	0
Z	254	N 254 389	435	128	435	351	336	290	566	566
æ×	.47	.30	.33	.34	.20	.32	.33	.43	.53	.43
۵	10.	10.	.01	.33	.18	.01	.00	10.	.01	.00
S. B.	.47	.48	.28	.39	.26	.33	.34	.35	.56	. 45
م	.00	.01	.00	.10	10.	10.	.01	.00	.00	.00
-										

 $R_{_{\mathrm{M}}}=$ Multiple R for equations with criterion standardized within periods. $R_{\rm a}$ = Multiple R for equations with criterion standardized across periods.

Standardization of SOO Data

The original rationale for standardization of predictor scores (Likert & Bowers, 1973) and its inapplicability to the multivariate situation has been discussed in Section 2. An alternative reason for standardization would be that the SOO is in some sense a different measure when applied to different organizations. Although the manner in which the concepts the SOO measures are manifested may vary across organizations, the concepts themselves and the theory which ties them together are common to a large variety of organizations (Taylor & Bowers, 1972), including the organizations represented in the present study. Given this, differences in SOO scores across organizations are due to quantitative differences in the concept measured and not merely the metric employed; therefore, there is no real reason to standardize each organization's SOO scores against its own distribution to equate means at zero and standard deviations at one.

An alternative scheme would be to standardize the SOO across organizations. Since this would apply a single linear transformation to all organizations' SOO scores (for each of the 13 indices), this would have no effect on the SOO criteria correlations. Therefore, the SOO scores were left unstandardized in the present study.

In conclusion, it should be noted that the entire standardization issue is more an artifact of the combination of data from different organizations to illustrate the current value methodology than it is a feature of the method itself. The analogue of TVE for any single organization would likely be internally consistent, thus eliminating the need for standardizing. Should different measures be required, perhaps for different types of work, an empirical investigation of their inter-relationships would likely provide the best answer to combining the measures into a single data file. Should standardization be the method of choice, it would most likely be preferable

to standardize within different time periods, unless, as in the present study, situational constraints preclude this.

Work Group Level

Cost center scores on TVE and ABS reflect the contribution of all work groups in the cost center to its performance on these measures. Reporting the criterion in this manner has some specific advantages, particularly in regards to supervisory performance. Since TVE is measured at the cost center level, it includes both the direct effects of changes in supervisors' behavior at their work group level (other supervisors) and the indirect effects of their changed behavior at the subordinate work group level. The potential problem of distinguishing these direct and indirect changes and costing them separately is thus avoided as is the very real problem of identifying and costing a supervisory level analogue of TVE. There is a similar benefit with regards to ABS in that some of the effects of changes in supervisory absenteeism will appear at subordinate levels. Cost center reporting lumps these effects together with those that appear at the supervisors' level, again eliminating any need for measuring and costing supervisory and subordinate levels separately.

Despite the above advantages, this reporting procedure potentially introduces several sources of error into the value attribution for supervisory groups. First, it is unlikely that supervisor absenteeism has the same cost to the organization as does worker absenteeism. Second, the appropriateness of any given TVE-like measure for supervisors probably varies greatly across organizational levels. Third, supervisory leadership is a causal variable in the present theoretical model. The process of imputing cost center scores to all groups does not address the problem of attributing an appropriate portion of changed subordinate group value to changed supervisory behavior.

Thus it is likely that the error in the value attributed specifically to supervisory groups is increased, although this is not necessarily so for the attribution at the organizational level. Finally, while there are virtually no empirical studies bearing the relationship of organizational level to TVE or ABS type measures (Porter & Lawler, 1965; Berger & Cummings, in press), it can be plausibly hypothesized that organizational level does influence the nature of the relationship between the SOO predictors and performance. To the extent that this hypothesis is true, it suggests the use of different prediction equations at different organizational levels. However, it is impossible to implement this procedure unless the criteria are measured at the work group level.

Thus, while criterion measurement at the cost center level resolves several issues around measurement and costing of supervisory performance, it raises others. In the present study there was no option about how the criteria would be measured and, practically speaking, it is a moot point. However, in an actual implementation of a current value type of Human Resources Accounting, measurement of the criteria, especially at the supervisory level, is an issue that will require careful consideration from a variety of perspectives.

INVESTIGATION OF THE MODEL

The purpose of this section is to explore the application of our selected mathematical model to the data set at hand. Inherent in any model are assumptions about the way different characteristics or variables interrelate. The initial selection of the model is independent of the data in that it is derived primarily from a theoretical construct. Thus it naturally follows to examine the data set at hand for confirmation, or at least non-contradiction, of these assumed relationships.

The model selected to represent the relationship between S00 measures $(\underline{X}, \text{ where } \underline{X} \text{ represents the matrix of indices with ith row } (X_{1i}, X_{2i}, \ldots, X_{13i})$ and productivity measure (Y_i) is

(1)
$$\underline{Y} = \underline{B}_0 + \underline{B} \underline{X} + \underline{\varepsilon}$$

Actually, this is a model for 19 relationships in that we are investigating nine TVE and 10 ABS performance periods. However, from a theoretical standpoint, it follows that the type of model which is appropriate for one time period ought to be appropriate for all other periods. It is possible, though, that the relationship between absenteeism (ABS) and SOO may have a different form than that for total variable expense (TVE) and SOO. The analyses reported below each bear on a specific characteristic or assumption of the model. The areas investigated are: assumed linearity, distribution of the $\underline{\varepsilon}$ terms, variables to be included as predictors, modifier variables, and outlying data points.

Linearity

The model given by equation (1) includes the assumption of linearity both in the parameters B_i and in the variables X_i . (One may have linearity in the parameters, but not in the variables. For example, $Y = B_1X + B_2X^2$ is linear in the B's, but not in the X's. Some authors call this linear, second order. For the purposes of this study, we will use linearity to mean both linear in the parameters B_i and in the variables X_i .) In the univariate case, the assumption of linearity can easily be viewed by the examination of a scatter diagram. In the multivariate case, other techniques must be used.

An earlier report (Pecorella & Bowers, 1977) used the statistic $(eta)^2$ as a measure of linearity, and concluded that there was insufficient evidence to disprove linearity. Due to the theoretical and practical importance of this assumption, it is further examined here.

While with 13 predictor variables, linearity is in 14-dimensional space and impossible to explore directly using graphical procedures, it is possible to examine the residuals (the differences $Y_j - \hat{Y}_j$ where Y_j is an observed value and \hat{Y}_j is the estimated value obtained by use of the fitted regression equation). The two classical techniques used here are to plot the residuals against the predicted or fitted values, \hat{Y}_j , and also against each of the independent variables. The plots against the independent variables focus on the linearity with respect to each of the S00 indices, while the plot against the predicted values will show any cumulative effects of non-linearity which are either not captured in a plot of $Y_j - \hat{Y}_j$ versus any single X_i or are due to a variable not included in the predictors, e.g., type of work.

The plots of the residuals with the predicted values will yield a horizontal band evenly distributed about the line $Y-\hat{Y}=0$ if the model fits the data. For instance, if the relationship is not linear, but should have

either a cross-product term or quadratic term, the plot would have a parabolic shape (Draper & Smith, 1966). In Figure 2, several of the plots of the residuals against the predicted values are presented. (A complete compiliation is given in Appendix A.) At first glance, the appearance of the negatively sloped bands prominent. However, these bands are an artifact of imputing cost center values to each of the work groups of which it is comprised. This can be easily seen from the following graphs, using just one of the S00 indices. Assume there are three cost centers (A, B, & C) with four, five, and three work groups each. The overall relationship between S00 and either criterion (TVE or ABS) is negative, as indicated by the regression line. Each work group from a cost center will have a different S00 score but the same criterion score. This situation is shown in Figure 3.

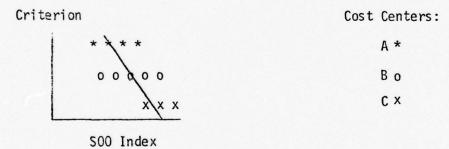
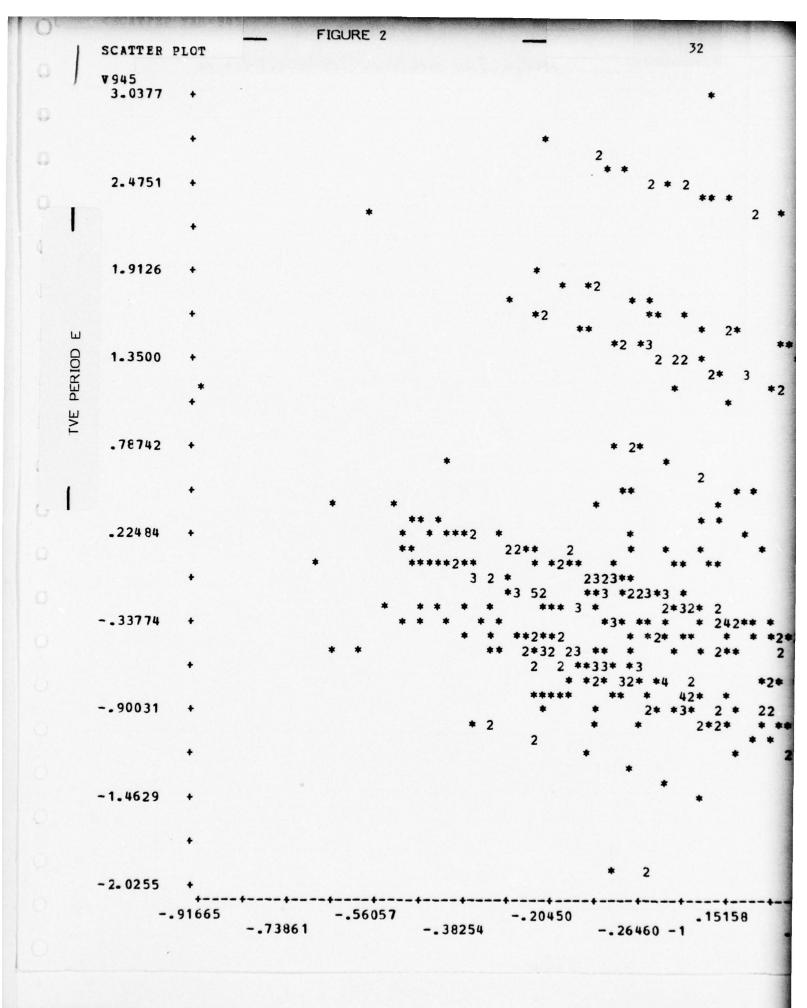


Figure 3

As can be seen in Figure 3, in any given cost center, the work group with the lowest S00 index score will have a relatively large negative residual, while the work group with the highest S00 score will have a relatively large positive residual. Because of the negative relationship between the two variables, the work groups with the lower S00 scores will have higher predicted criterion values than will the work groups with the higher S00 scores.



2 * 2 * * *

*2 *3 2 22 *

*2

2323**

* 42* * 2* *3* 2 *

2

.15158 .50765 V915 .68569 -.26460 -1 .32962

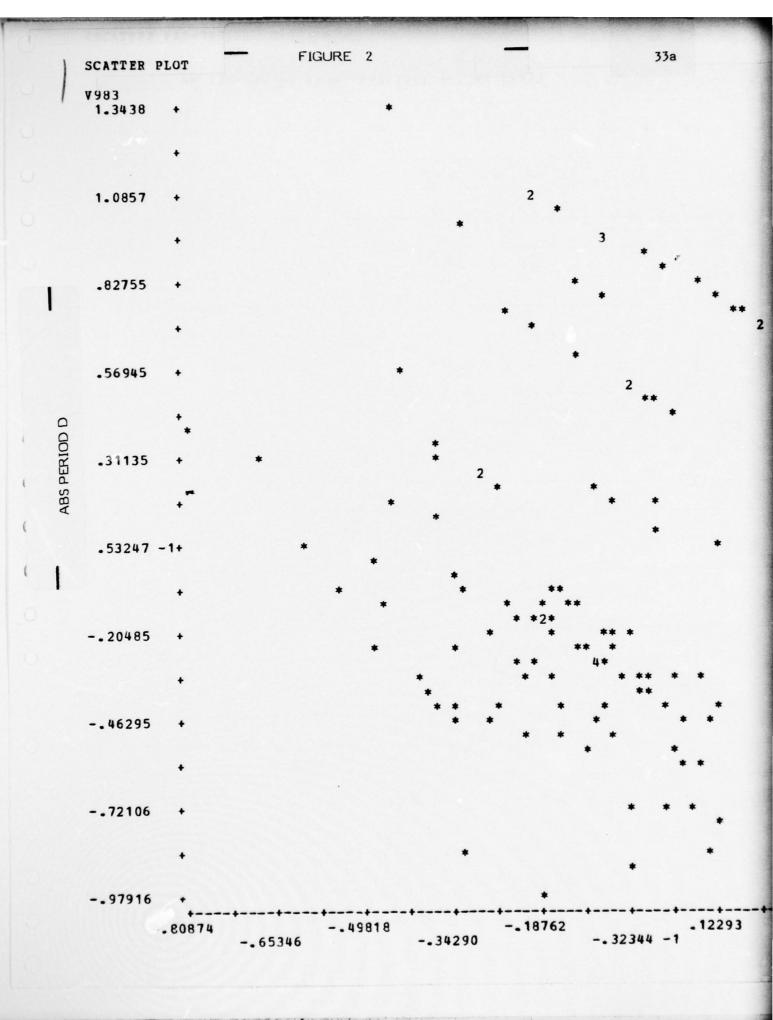
*
342
2*33
**4*2
*222
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.22028 -41158 -.95652 -1

.53621

.85214

v916 1.1681



3

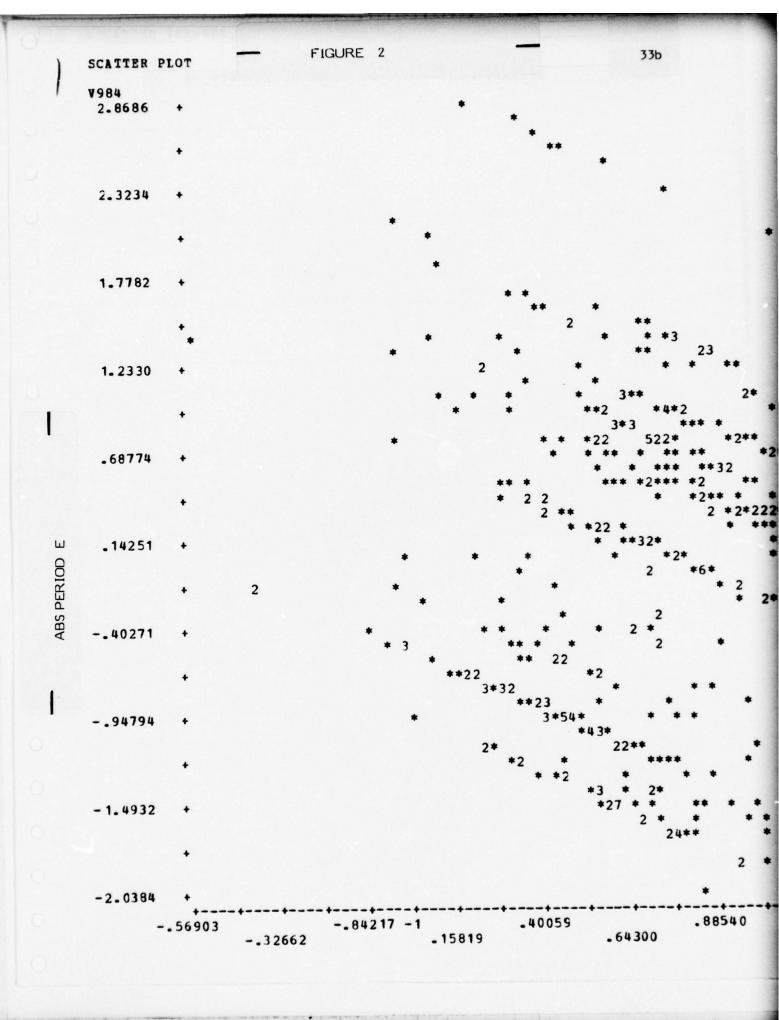
2

762 .12293 -. 32344 -1

. 27821

.43349

v973 .58877

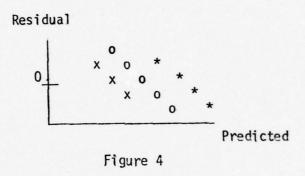


```
v974
1.6126
10059
                                                 1.3702
                       .88540
```

1.1278

.64300

Thus, the work groups within a cost center with low S00 scores have high predicted criterion scores and relatively <u>negative</u> residuals while work groups from the same cost center with high S00 scores have low predicted criterion values and large <u>positive</u> residuals. When graphing the residuals versus the predicted values, this produces negatively sloped bands as demonstrated in Figure 4.



With this inherent pattern in mind, the interpretation of the plots in Figure 2 and Appendix A is that there is no evidence of non-linearity.

The second method of using the residuals to examine the linearity assumptions is to plot the residuals for both TVE and ABS against each of the 13 S00 indices individually. The 13 plots for each criterion-period are contained in Appendix B. An inspection of these 247 plots shows a basic pattern of a horizontal band of points which is considered supportive of model adequacy.

The examination of these plots and those of the residuals versus the predicted values, plus the previously reported analysis using eta², lends strong support to our assumption of multivariate linearity for the data set in hand.

Error Distribution

In investigating the normality of the error term ε in equation (1) the standard technique is to graph the frequency distribution of the residuals. Appendix C contains these histograms, a selected group of which are presented in Figure 5. The graphs can be seen to be basically symmetric and bell shaped, supporting the assumption of normality of the error terms. While the assumption of normality is not necessary for fitting the model, most, if not all, of the classical techniques for testing hypotheses related to the model are dependent on the accuracy of this assumption.

Predictor Variables

A third area of investigation is the number of predictors involved. In particular, it was of interest to explore the possibility of using only a significantly smaller subset of the 13 S00 predictor variables. The statistical methodology selected to analyze this issue was to apply a backward regression technique to a selected sample of performance periods for both criterion variables. The backward regression technique, in essence, begins with all 13 predictor variables in the model, and then begins to eliminate those which have little or no predictive value. This elimination process continues until only those variables with a predetermined level of statistically significant predictive ability remain. If a particular group of predictors were continually omitted from the model during this procedure, this would be considered evidence to support their omission from the final model.

HISTOGRAM	FIG	SURE 5	5															
MIDPOINT	HIST%	COUNT	FOR	943.V	943	(EACH	X=	1)										
-1.7102	.2	1	+ X															
-1.4602	0.	0	+															
-1.2102	.7	3	+ X X X															
96021	3.2	14	+XXX	XXXXXX	XXXX	X												
71021	13.1	58	+XXX	XXXXXX	XXXX	XXXXXX	XXX	XXXX	XXX	XXX	XXX	XXXX	XXX	XX	XXX	XXX	XXXX	X
46021	16.7	74	+ X X X	XXXXXX	XXXX	XXXXXX	XXXX	XXXX	XXX	XXX	XXX	XXXX	XXX	XXX	XXX	XX	XXX	K
21021	18.1	80	+XXX	XXXXXX	XXXX	XXXXXX	XXXX	XXXX	XXX	XXX	XXX	XXXX	(XX)	XXX	XXX	XXX	XXXX	X
.39789 -1	13.3	59	+XXX	XXXXXX	XXXX	XXXXXX	XXXX	XXXX	XXX	XXX	XXX	XXXX	XXX	XXX	XXX	XXX	XXXX	X
-28979	10.9	48	+ X X X	XXXXXX	XXXX	XXXXXX	XXX	XXXX	XXX	XXX	XXX	XXXX	XXX	XXX	XXX	X		
.53979	9.3	41	+ X X X	XXXXXX	XXXX	XXXXXX	XXXX	XXXX	XXX	XXX	XXX	XXXX	XX					
.78979	5.0	22	+ X X X	XXXXXX	XXXX	XXXXXX	XXX											
1.0398	3.2	14	+ X X X	XXXXXX	XXXX	X												
1.2898	2.9	13	+XXX	XXXXXX	XXXX													
1.5398	2.5	11	+ X X X	XXXXXX	XX													
1.7898	.7	3	+XXX															
2.0398	.2	1	+ X															
MISSING		1877																
TOTAL		2319	(IN	TERVAL	WID	TH= .2	5000))										

TVE PERIOD C

XXXXXXXXXXXXXXXXX

))

1)

HISTOGRAM	F	IGURE	5
MIDPOINT	HIST%	COUNT	r FOR 947. V947 (EACH X= 1)
61570	2.0	1	+ x
36570	13.7	7	+ X X X X X X X
11570	41.2	21	+ XXXXXXXXXXXXXXXXXXXXXXX
.13430	29.4	15	* X X X X X X X X X X X X X X X X X X X
-38430	7.8	4	+ X X X X
-63430	3.9	2	+ X X
.88430	2.0	1	+ X
MISSING		2268	
TOTAL		2319	(INTERVAL WIDTH= .25000)

TVE PERIOD G

```
FIGURE 5
HISTOGRAM
         HIST% COUNT FOR 980. V980 (EACH X= 1)
MIDPOINT
-2.1432
           1.2
                   3 + X X X
-1.8932
            .8
                   2 + XX
-1.6432
           4.3
                  11 +XXXXXXXXXXX
- 1. 39 32
           2.4
                  6 +XXXXXX
-1.1432
            5.9
                  15 +XXXXXXXXXXXXXXXX
-.89323
            5.9
                  15 +XXXXXXXXXXXXXXX
-.64323
           8.3
                  21 +XXXXXXXXXXXXXXXXXXXXX
-.39323
           8.7
                  22 +XXXXXXXXXXXXXXXXXXXXXXX
                  -.14323
           13.0
                  .10677
           13.8
           9.1
                  23 +XXXXXXXXXXXXXXXXXXXXXXXX
 .35677
                  21 +XXXXXXXXXXXXXXXXXXXXXX
 .60677
           8.3
                  15 +XXXXXXXXXXXXXXX
 .85677
            5.9
                 1 + X
 1.1068
            -4
 1.3568
                  8 +XXXXXXXX
           3.1
 1.6068
           3.1
                 8 +XXXXXXXX
 1.8568
                  5 + XXXXX
           2.0
2.1068
           2.4
                   6 +XXXXXX
 2.3568
            . 8
                   2 + X X
 2.6068
            .8
                   2 + X X
 MISSING
                2065
 TOTAL
                2319 (INTERVAL WIDTH= .25000)
```

ABS PERIOD A

MIDPOINT	HIST%	COUNT	FOR 987. V987 (EACH X= 1)
-1.5548	1.4	4	+ X X X X
-1.3048	2.1	6	+ X X X X X
-1.0548	3.5	10	+ X X X X X X X X X
80482	2.1	6	+ XXXXXX
55482	7.6	22	+ X X X X X X X X X X X X X X X X X X X
30482	17.6	51	*XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
54823 -1	19.4	56	+ X X X X X X X X X X X X X X X X X X X
. 19518	18.0	52	+ X X X X X X X X X X X X X X X X X X X
.44518	18.0	52	+ * * * * * * * * * * * * * * * * * * *
-69518	6.9	20	+ X X X X X X X X X X X X X X X X X X X
.94518	1.0	3	+ X X X
1.1952	1.7	5	+ XXXXX
1.4452	.3	1	+ X
1.6952	0.	0	
1.9452	0.	0	
2.1952	0.	0	
2.4452	.3	1	+ X
MISSING		2030	
TOTAL		2319	(INTERVAL WIDTH= .25000)

ABS PERIOD H

The backward regression technique was applied to four selected TVE and three selected ABS periods. The periods were selected so that they included different organizations, (in particular, one period with all organizations, one with a few, and one with only one organization) and covered the entire time span.

For this collection of seven analyses (of a possible 19), there were no subsets of even two or three variables which were omitted in all instances while all variables were omitted at least once. The significance level used for retaining a variable was liberal (.1). The conclusion is that there is insufficient evidence from the data at hand to consistently remove any set of three or more predictor variables (SOO) from this model.

Modifier Variables

As suggested in Chapter 2, it is possible that certain non-causal variables may act as modifiers of the relationship between the SOO indices and the criteria. It may be desirable to either compute separate FPTI equations for different values of the modifier(s), as was done for the performance periods, or to include these modifiers in the model itself. An example of a modifier that might be treated in the second manner is suggested by a previous analysis. Pecorella and Bowers (1977, pp. 27-31) found that the proportion of significant SOO index to criterion correlations decreased as capital intensity (CAPINTEN) increased. CAPINTEN is defined as the ratio of total dollar value of assets to total number of employees. In order to illustrate the inclusion of a modifier variable in the model, an analysis of CAPINTEN is presented here.

Before presenting the results of the analysis, some characteristics of CAPINTEN should be noted. The values on this variable were computed from Fortune 500 figures for 1971, the end of the period of S00 and performance data collection. As such, CAPINTEN is computed for the entire corporations to which the particular organizations in this study belonged. Thus, while CAPINTEN undoubtedly has a strong relationship to the capital intensity of the organizations in this study, it is actually a feature of the corporation as a whole. Another feature of the CAPINTEN variable is its limited variance. The four sites from Organization II all receive the same corporate score on CAPINTEN as do the three sites from Organization VI. Thus, for each criterion there is a maximum of four levels of CAPINTEN, and often fewer, that enter into the analysis. In fact, in TVE periods B, G, and H, and ABS period A there is only one level of the CAPINTEN variable present and therefore it cannot be included in equations for these periods.

Since it is our purpose to examine the predictive ability of a model including CAPINTEN and 13,500 indices against a model containing only the 13 S00 indices, the terminology of Bottenberg and Ward (1963) and Draper and Smith (1966) will be used herein. Briefly, these authors define a restricted model as the model with the variables which have already been included in the prediction equation. The full model consists of the restricted model plus a set of one or more variables to be tested for inclusion in the equation. This test uses the sum of squared deviations from the mean (SS) associated with each model in a "partial" or "sequential" F-test (Draper & Smith, 1966, p. 71) to determine the significance of the increased prediction provided by the variables in the full model but not in the restricted model. The models will be referred to here by a subscripted R:

 R_{13} means the model with 13 S00 indices (restricted model) or the multiple R for that model, depending on the context; $R_{\rm C}$ means the model with CAPINTEN plus the 13 S00 indices (full model) or its multiple R, again depending on the context. Finally $R_{\rm C}-R_{13}$ means comparisons of the full model with the restricted model or the change in the value of R from one model to the other. The value of p reported for $R_{\rm C}-R_{13}$ is determined by the sequential F-test described above.

Table 4 shows the effect of including CAPINTEN in the model for TVE. There are seven periods where its effect could be examined. $R_{\rm C}$ - R_{13} was significant (p<.05) in only two of the seven periods (E & F). Examinations of the organizations represented in each period (Table 2) shows that periods E and F had three and two levels of CAPINTEN, respectively, while periods A, C, D, and I had two, three, four, and two levels, respectively. Therefore, it does not appear that the failure of CAPINTEN in periods A, C, D, and I is due to limited variance. Rather, in general, it seems that CAPINTEN does not aid in predicting TVE, although close examination of periods E and F might reveal particular circumstances where we could expect CAPINTEN to have some predictive value.

Table 5 shows the results of the analysis for absenteeism (ABS) plus some other results discussed below. Of the nine periods where $R_{\rm c}$ could be compared to R_{13} , seven show a significant (p<.01) value for $R_{\rm c}-R_{13}$. Furthermore, where $R_{\rm c}-R_{13}$ is significant, its size is moderate to large (.07 $\leq R_{\rm c}-R_{13} \leq$.26; mean $[R_{\rm c}-R_{13}]=.16$). Thus, the addition of the modifier CAPINTEN to the model significantly improves our ability to predict ABS. This is despite the fact the CAPINTEN is measured at the corporate level and has limited variance.

Table 4
EFFECT OF CAPINTEN ON PREDICTION OF TVE

									-
	A	В	v	0	IJ	ᄕ	5	Ξ	I
Z	188	127	442	509	442	198	51	51	409
R _{1 3}	.51	.34	.39	.25	.27	.52	.57	.49	.28
۵	.01	.35	.01	.01	.01	.01	.23	.58	.01
ي م	.51	NOTE ²	.40	.26	.34	.67	NO TE ²	NOTE ²	.28
۵	.01	1	.00	10.	.01	.01	1	1	.01
Rc-R13	0	1	٠٥٠	٠٥.	.07	.15	1	1	0
e.	NS 1	1	NS	NS	.01	.00	1	1	NS
NOTE 1	NS = not	NS = not significant at	the	.05 level.					

CAPINTEN has only one level for the cases in this period, therefore, it does not enter into the equation. NOTE²

Table 5
EFFECT OF CAPINTEN AND SIZE ON PREDICTION OF ABS

	5	266	.51	.0	1.00	.51	90.	.00	NOTE 4	1	;	:	:
	п	266	.56	NS	1.00	.56	0.0		NOTE 4				
	王	290	.42	.00	76.	.43	80.	.01	.53	F.	.01	01.	.o.
	5	336	.60	.01	76.	09.	.26	10.	09.	0.0	NS	0.0	NS
	ഥ	351	.13	.01	76.	. 44	E.	10.	.52	90.	.01	.12	10.
	ш	435	.23	.01	16.	.45	.19	10.	.49	0.0	NS	.04	10.
	O	128	.41	NS ²	42	.62	.21	.01	.62	.21	.01	0.0	NS
	ပ	435	.50	.01	16.	.47	.19	10.	.50	0.0	NS	.03	10.
	В	389	.64	.01	.87	.56	60.	.01	.65	.01	10.	60.	.01
	А	254	NOTE 3	;	1	NOTE 3	1	;	NOTE 3	;	!	1	1
-		N R ₁₃	R _c -R ₁₃	, _—	So	Z,	R - R13	4	R S	RR	, ,	RR	5 0-

NOTE¹ p<.01 for all values of R and r shown in this table.

NOTE² NS = not significant at the .05 level.

CAPINTEN has only one level for all cases in this period, therefore, it does not enter into the equation. NOTE 3

 r_{cs} =1.00 for this period. Therefore, SIZE and CAPINTEN cannot both be in the model.

NOTE 4

The definition of CAPINTEN as a ratio with total number of people in the corporations as the denominator suggests that it may not be CAPINTEN but rather corporate or organizational size or total assets that is increasing our ability to predict absenteeism. A positive relationship between organization size and absenteeism has been reported consistently in the literature (Porter & Lawler, 1965; Berger & Cummings, in press). Therefore an analysis examining the ability of a model including a SIZE variable to predict ABS was conducted. An estimate of the size of each organization and each site within each organization was available from the number of individuals responding to the SOO at each site. Therefore, another variable, SIZE, was so defined and entered into a model with the 13 SOO indices to predict ABS. This variable has more levels (10) than CAPINTEN and reflects a structural feature of the specific organizations and sites rather than of the entire corporations.

The investigation of models for ABS including SIZE is two-fold. First, $R_{\rm S}$ is compared to R_{13} to determine if SIZE does increase our ability to predict ABS. Second, a model including SIZE and CAPINTEN ($R_{\rm CS}$) is compared to the models including either SIZE or CAPINTEN. This allows us to investigate the increase in predictions of a model containing both variables over a model containing either one of the variables but not the other.

The Pearson product moment correlation between SIZE and CAPINTEN over all sites is .85 (p<.01). This correlation (r_{cs}) will not be constant over periods since different organizations and sites within organizations enter the analysis in different periods. Therefore, the values of r_{cs} for each ABS period are listed in Table 5.

The comparison of R_s to R_{13} shows that in eight of the nine periods where the analysis is possible, R_s-R_{13} is significant. As with R_c-R_{13} , the significant values are generally moderate to large (.06 \leq R_s-R₁₃ \leq .26; mean $[R_s-R_{13}] = .15$). The values of R_s-R_{13} and R_c-R_{13} are generally similar. This overall pattern of similar magnitudes for ${\rm R}_{\rm C}\text{-}{\rm R}_{\rm 13}$ and R_s - R_{13} and the high values of r_{cs} indicate that SIZE and CAPINTEN are accounting for approximately the same additional variance in ABS over and above the variance accounted for by the SOO for which variables. The notable exception to this pattern is period D where r_{cs} is of moderate size (-.42) and R_c is not larger than R₁₃ but R_s is considerably larger than R₁₃. This is probably an artifact of the manner in which SIZE and CAPINTEN were defined. Examination of ABS period D in Table 2 shows that CAPINTEN will have only two levels while SIZE will have five levels (one for Organization I and four for Organization II). Thus, CAPINTEN does not add to the model's ability to predict but SIZE does. Because of this unique situation, period D will not be considered in the following discussion.

Additionally periods I and J are not included in the comparison of $R_{\rm CS}$ to $R_{\rm C}$ and $R_{\rm S}$ because $r_{\rm CS}$ for these periods equal 1.00. Thus, entry of SIZE into the model for periods I and J is completely redundant with entry of CAPINTEN and vice-versa. This leaves us with periods B, C, E, F, G, and H in which to compare $R_{\rm CS}$ to $R_{\rm C}$ and $R_{\rm S}$.

Comparison of R_{cs} to the larger of the two values of R_c and R_s (thus looking at the smaller of the two values of R_{cs} - R_c and R_{cs} - R_s) shows that inclusion of both predictors generally adds little to the prediction of ABS over the inclusion of whichever predictor (SIZE or CAPINTEN) is most effective alone. The statistical significance of these values (R_{cs} - R_s & R_{cs} - R_c) is

high (p<.01) despite the small magnitude of $R_{\rm CS}$ - $R_{\rm S}$ and $R_{\rm CS}$ - $R_{\rm C}$ because of the large N involved. Periods F and H do show a moderate increase in $R_{\rm CS}$ over $R_{\rm S}$ and $R_{\rm C}$. This is unexpected since $r_{\rm CS}$ is extremely high (.97) in both these periods. Apparently the variances that are unique to SIZE and CAPINTEN are both common to ABS in these periods. However, there is no increase in $R_{\rm CS}$ over $R_{\rm C}$ or $R_{\rm S}$ for period G, which includes the same organizations as periods F and H.

In summary, the three models, $R_{\rm CS}$, $R_{\rm S}$, and $R_{\rm C}$ are strikingly similar in their ability to predict ABS. However, whether CAPINTEN or SIZE adds more to the S00 model is a function of the particular period and the organizations in the period. Exceptions to this include period D which has a unique combination of CAPINTEN and SIZE values, and periods F and H where $R_{\rm CS}$ does offer some moderate improvement over both $R_{\rm C}$ and $R_{\rm S}$.

The above analyses demonstrate two variables, closely related, which improve the ability of a model containing the 13 SOO indices to predict ABS. A variety of hypotheses as to how this improvement occurs could be generated but any causal link between either CAPINTEN or SIZE and ABS would be mere conjecture at this point. Therefore, even if e.g., SIZE, were included in the model, change in value of the organization's human resources would not be attributed to a change in SIZE. Rather, the effects of change in SIZE would have to be partialled out so that value would be attributed only to changes in the SOO indices (or other causal variables). This is a rather complex procedure and would go considerably beyond the already intricate analyses that have been conducted and well beyond the intended scope of this study.

The analysis presented here is offered only as an example of some possible modifying variables. In an actual application the modifier(s) considered and selected would be a function of both empirical and theoretical considerations.

Outliers

When one encounters a few data points which are deviant from the bulk of the sample or from expectations one is always faced with the decision of whether or not to retain the data or eliminate it. A variety of strategies for making this decision are available. The one selected depends on the source of the data, the purposes for which it will be used and the bent of the researchers.

Given that one is willing to consider eliminating deviant data, perhaps the most common approach is to identify questionable data and determine if an explanation can be found for its deviance. This approach has already been used in the present study in the examination of the SOO data and the various criterion measures from different organizations to determine if the data set was suitable for the application of the current value methodology. A prime example of this is the elimination of the TVE measures from Plant 2 in Organization VI for periods A through E due to organizational practices which resulted in increases in TVE for high producing cost centers and decreases in TVE for low producing cost centers. [This issue of organizational practices which reverse the expected relationship of SOO to organizational functioning is covered more thoroughly in Taylor & Bowers, (1972)]. Thus, the source of the data and the effects of "intrusive factors" have already been considered in establishing the data file.

In examining the plots of the residuals, the existence of extreme values or outliers became apparent. When investigating the nature of outliers (defined as values in excess of 3.5), no systemic reasons could be found. (An example of systemic reasons would be the same cost center over time.) Thus, these deviant values are presumably a result of misreporting, transcription error, or statistical quirk. However, upon examination of the actual criterion standard scores, it was found that they ranged from 4.8 to 10 (in absolute value), implying inaccuracy rather than probabilistic deviance. Table 6 presents the information concerning these outliers as well as the Multiple R values when including and excluding these cases. Results reported in Tables 2 through 5 are for analyses conducted prior to elimination of the data shown in Table 6. The plots shown in Figure 2 and Appendices A through C are the results of analyses conducted after the elimination of these data. As statistical theory predicts, these outliers have unusual leverage in fitting the regression model to the data, and therefore, distort the results. It is for this reason that these cases were removed from the analysis.

Deletion of some cases from each organization's file will alter the mean and standard deviation of the performance score distribution for that organization. The particular transformation used and therefore the standard scores arrived at are a function of these statistics. Since different transformations are used for and different data is deleted from each organization, the effect of deleting data on the standard scores will vary across organizations. Obviously, when standard scores from one organization shift in one manner and those from another organization shift differently, the relationship between these scores and the SOO scores will change. Necessarily, this will only happen if the performance score distributions are restandardized after the data are deleted. To avoid this unpredictable change in

the predictor-criterion relationship, performance score distributions have not been restandardized after deletion of the data. Because of this, the actual mean and standard deviations of the performance score distributions with the data deleted are not exactly zero and one respectively for some organizations and some periods. Since so few cases were deleted, however, the parameters will be quite close to these values. The changes in R shown in Table 6 are thus solely the result of the deletion of outliers and not the result of deletion plus restandardization.

Table 6
CHARACTERISTICS OF DELETED DATA

Criterion	Period	Criterion Standardized Score of Deleted Cost Centers ¹	Before Deletion	eletion	After Deletion	eletion
			Z	~	Z	~
TVE	O	9.15	509	.25	505	.28
	Ŧ	7.79	51	.49	45	.57
ABS	v	7.13	435	.28	434	.31
	0	4.84 6.26	128	.39	121	.40
	ш	-10.15	435	.26	434	.30
	æ	6.9	290	.35	289	. 42

¹In all periods except ABS-D, only one cost center was eliminated. In ABS-D, two cost centers were eliminated.

CONCLUSIONS

The analyses and discussions presented thus far can be divided into two somewhat overlapping categories. First, a variety of statistical considerations necessary for the development of FPTI's from identified relationships between the SOO and performance criteria have been addressed. Second, a variety of theoretical issues involved in the current value approach have been investigated. The statistical methodology associated with the current value approach was extended from a univariate to a multivariate situation. The issues around change scores, especially their reliability, were also addressed. Section 3 dealt primarily with the rationale for and effect of various operations that have been performed on the data set. Most of these operations were not an implicit part of the current value method, but rather the result of an interaction between requirements of the method and the nature of our data set. Finally, in Section 4, we examined how well the assumptions implicit in our linear model are met by the data set. Here it was concluded that a linear model adequately describes the SOO performance relationships for both TVE and ABS. It was also concluded that the number of SOO dimensions included could not be greatly decreased without affecting the ability to predict the criteria. Finally, the examination of the data set revealed the existence of a few data points with extremely large standardized criterion values, and these points were consequently removed from their respective periods.

Simply stated, the result of these analyses, plus those previously reported (Pecorella & Bowers, 1976a, 1976b, 1977) is that we are now able to define the FPTI equations which will be used in the value attribution phase of this study. Table 7 presents values of N, R, and p for the regression of criterion variables (standardized within organizations and across periods) on the 13 S00 predictors (unstandardized) with the data listed in Table 6 deleted from the analysis. Thus, these are the summary characteristics of the FPTI equations for the data from which they were developed. Tables 8 and 9 list the values for the parameters of the FPTI equations, $(B_0, B_1, B_2, ... B_{13})$ for TVE and ABS respectively. These equations will be used to predict changes in future performance from changes in measures of the human organization. Table 10 presents the number of work groups from each organization for which SOO scores at T_0 and T_0 are available. Thus, the FPTI equations represented in Tables 8 and 9 will be applied to the SOO change scores for these work groups. The predicted changes in performance thus computed will then be converted to dollar values and discounted to present value.

The theoretical issues discussed ranged from those involved in the development of the FPTI's in this study to those which, while not of direct concern in this study, are of importance in any implementation of a current value human resources accounting system. Taken as a whole, the analyses

 $^{^2}$ The ABS and TVE FPTI's were developed using data from data from different organizations and in some cases from different sites of the same organizations. Since the TVE and ABS FPTI's will each be applied only to the subgroup of organizations and sites on which they were developed, some organizations have different numbers of groups with T $_{\rm o}$ and T $_{\rm o}$ S00 scores for the ABS and TVE FPTI value attribution, as shown in Table 10.

VALUES OF N, R, AND p FOR THE REGRESSION EQUATIONS USED TO DEFINE FPTI'S Table 7

					TVE					
	А	В	၁	D	ш	L	5	Ŧ	-	
z	188	127	442	505	442	198	51	45	409	
8	.51	.34	.39	.28	.27	.52	.57	.57	.28	
а	.01	.35	.01	.01	10.	.01	.23	.35	10.	
					ABS					
	А	8	၁	D	ш	ഥ	5	=	1	2
Z	254	389	434	121	434	351	336	588	592	566
8	. 47	.40	.31	.40	.30	.33	.34	. 42	.56	.45
Q.	.01	.00	.01	01.	.01	10.	.01	10.	.01	.0

Table 3
BETA WEIGHTS FOR PERIOD FPTI'S OF TVE

	А	8	၁	0	ш	Ŀ	5	Ŧ	1
Regression Constant	.00247	.16430	.49197	1.0669	.94343	83179	71201	.60534	.57522
Supervisory Support	18483	11610	17555	04021	02063	.24337	29418	29767	07030
Supervisory Goal Emphasis	.11443	.11000	.20353	.24248	.16634	.10592	12580	43941	.04352
Supervisory Work Facilitation	.11195	.12490	00630	06977	02334	,15926	.34966	.32313	.10334
Supervisory Team Building	.12577	21590	.02611	.00948	06070	48260	06603	.49962	10963
Peer Support	.39078	.03359	15249	09380	10912	.25140	.08940	.29487	08029
Peer Goal Emphasis	12371	.13237	24554	25009	11746	.42923	.15495	14403	31091
Peer Work Facilitation	-,43689	36955	05815	19456	12499	97722	04795	-,31268	19232
Peer Interaction Facilitation	60060	.18499	.44040	.38398	.36051	.51046	19970	.13590	.57676
Human Resources Primacy	08535	09361	16294	16463	36936	.56292	.23469	01118	17215
Communication Flow	26790	18887	38943	48789	25253	.14878	.08824	.12399	15804
Motivational Conditions	12977	20126	01472	.22501	19181.	-, 19849	.02421	37802	.08388
Decision Making Practices	-,35838	12199	.02672	.02686	.05695	90434	20198	.15358	.20576
Satisfaction	.62770	. 40399	.33829	.03748	00535	03477	.15442	08274	07647

Table 9 BETA WEIGHTS FOR PERIOD FPII'S OF ABSENCE.

	А	В	ပ	0	Ш	Ŀ	ច	н	I	5
Regression Constant	1.5179	.49961	1.0282	1.0352	.22473	1.0094	.67690	.45852	-1.0411	.30370
Supervisory Support	48979	09379	35387	12286	09911	.14929	21582	07133	.39141	22864
Supervisory Goal Emphasis	.04810	.18358	.12241	21631	.36472	.14842	.16558	-,07054	.05707	00076
Supervisory Work Facilitation	.15065	.05978	.18522	.27108	46797	11026	.01772	.13328	16584	.13054
Supervisory Team Building	.10312	20706	04771	.07458	.19924	06599	.11636	02617	20138	76180.
Peer Support	56715	.27172	17250	09903	.14298	.17288	06851	17588	.46732	20608
Peer Goal Emphasis	.06387	13370	27301	.02057	19864	01931	.24858	-,11328	.02489	.04345
Peer Work Facilitation	.18083	62019	25236	.18299	.30477	.16537	.28413	13064	12974	02875
Peer Interaction Faciliation	.52212	.44863	.44705	25277	27005	27351	15285	.50633	36227	.23559
Human Resources Primacy	28960	.03289	02992	16707	37616	12823	12451	18422	.01404	16442
Communication Flow	18017	.25347	.06572	.30429	10363	.02381	29979	11554	.41686	07937
Motivational Conditions	.12527	18171	24122	13253	.46093	.04377	.19541	96960	03654	.14282
Decision Making Practices	30246	22958	12186	08815	.44863	-, 18535	32057	11913	.33242	10209
Satisfaction	.33982	-,16062	.32023	02581	26313	21633	.03280	.20076	62103	.01809

Table 10 WORK GROUPS WITH T $_{\rm O}$ AND T $_{\rm O}$ SOO SCORES

		TVE	ABS	
Organization 1			27	
	II	233	233	
	III	176	176	
	١٧	115		
	/I	246	197	
Tota	al	770	633	

presented herein allow us to move forward to the value attribution phase in the present study and to remain aware of issues of potential concern in an actual FPTI implementation.

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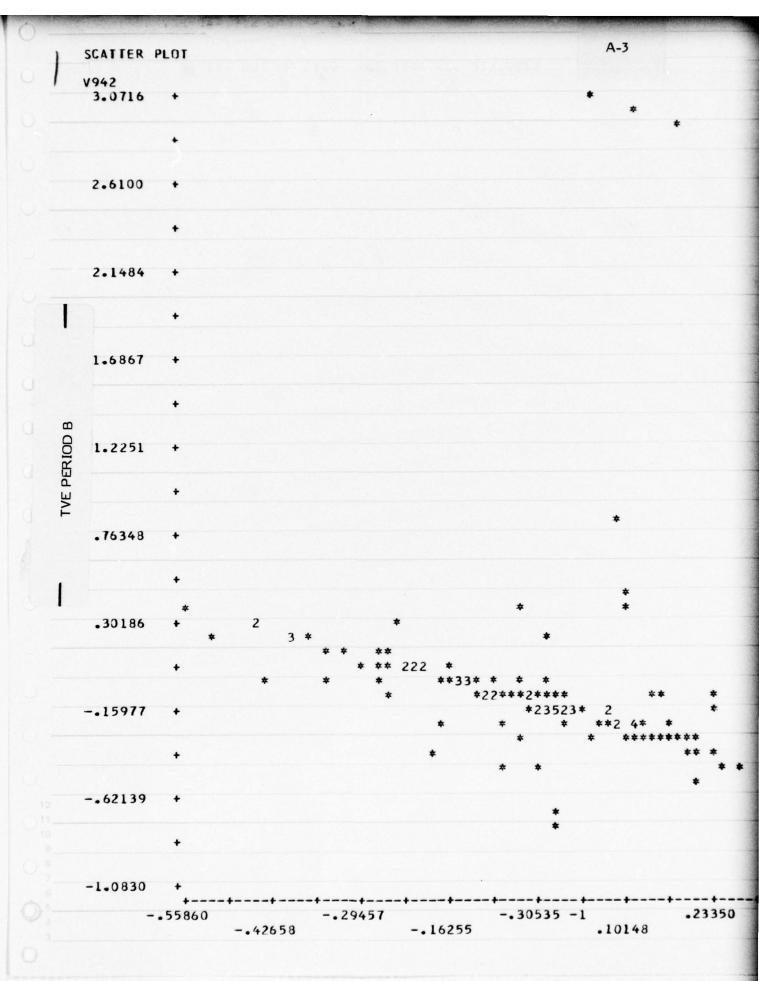
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APPENDIX A

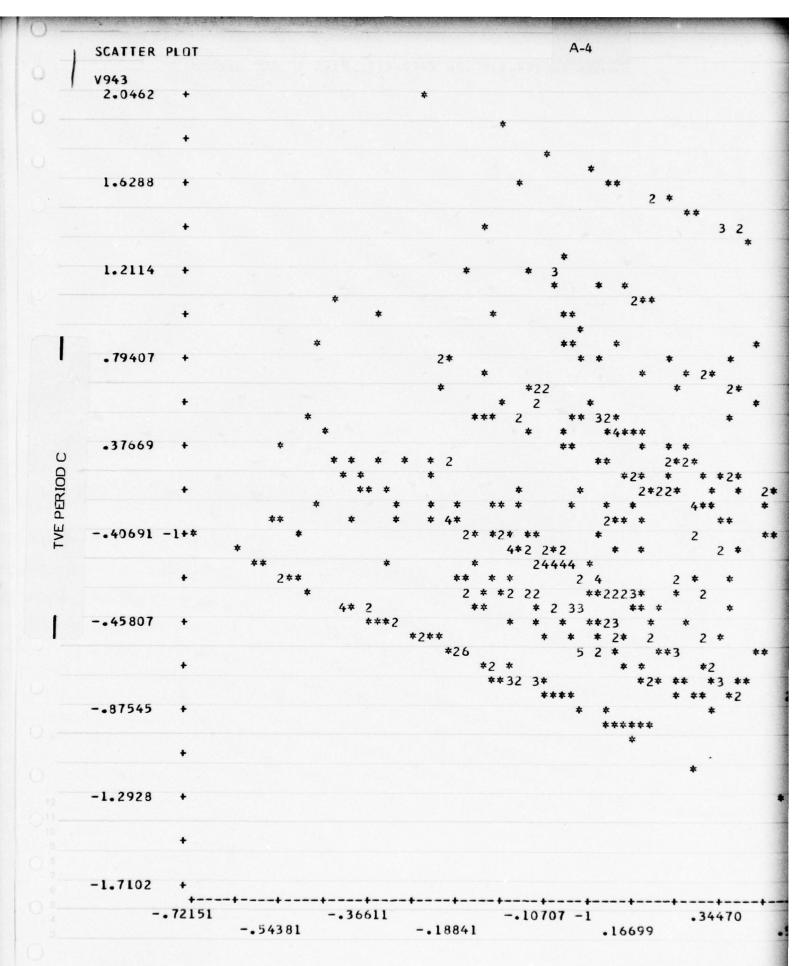
SCATTER DIAGRAMS OF RESIDUAL VS. PREDICTED

VALUES FOR TVE PERIODS A-I AND ABS

PERIODS A-J.



A-3 * 2 .49753 V912 0535 -1 .23350 .10148 .36552



10707 -1 .34470 .70010 V913 .87780

```
A-5
                                  22
*32*2 2
    *4 32**
*22322 * *334*2*
       2 22 ** 2322 ** 2*2
*2**6***
 **2322**4 3

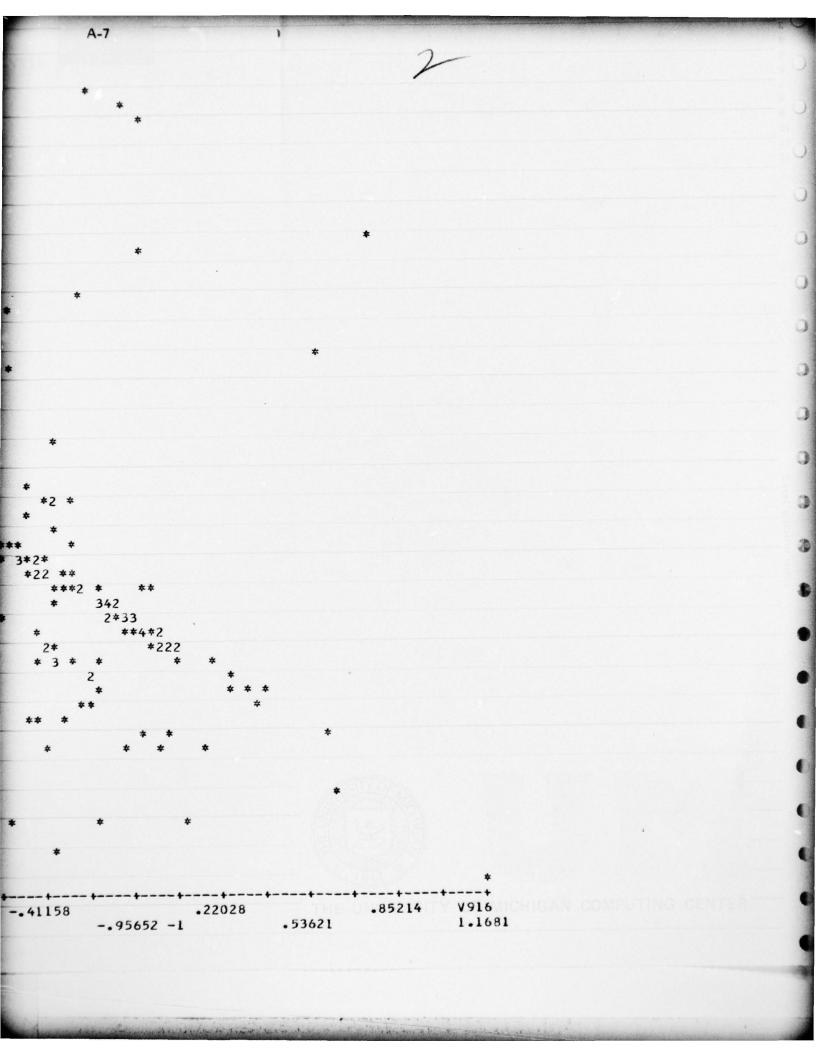
4* * 222*42* *

22 2*2* *23 23**2

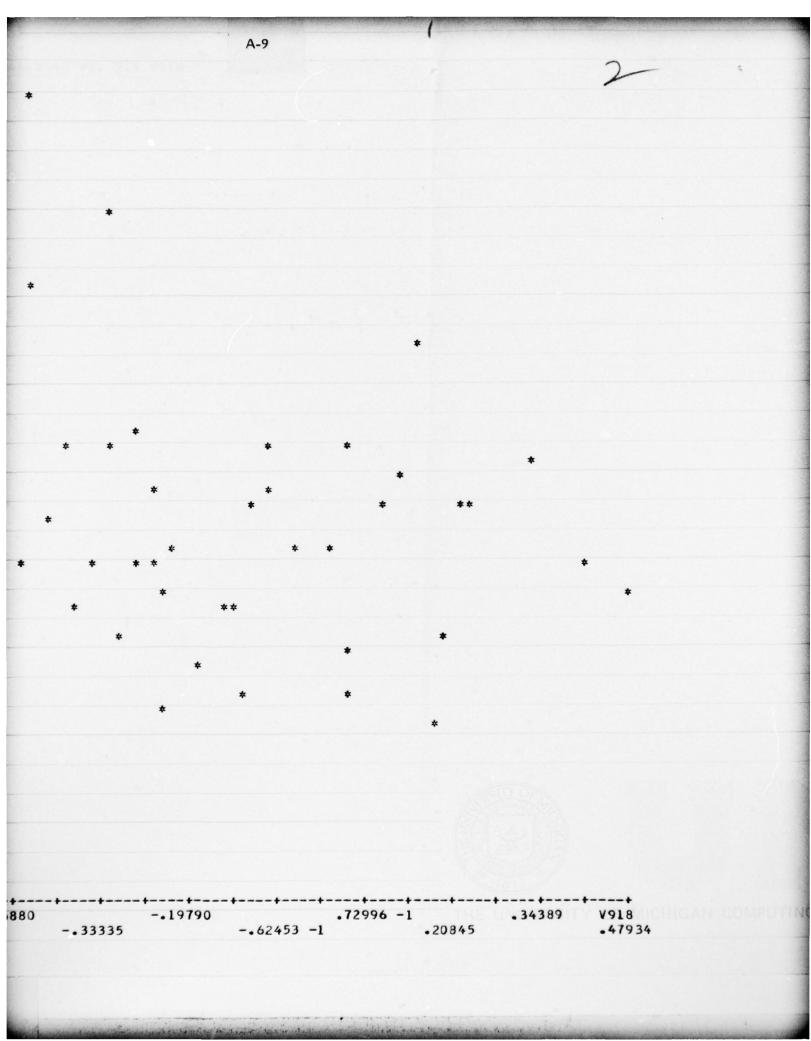
* * *23 3 ***
           * *23 3
                                                                  V914
    -.47039 -1
                             .36819
                                                     .78341
                                        .57580
                                                                  .99103
               .16057
```

-. 73861

·



-.20263 -.85976 -1 .14733 .38063



```
442
                     2
                             2
                                             *
2*
     4*4* 2
     2 ***522* *
            2
  * 3*3*
       *62*5
**23 *
                 2**
                                        *
                               .26966
                                         V919
           -.27594 -1
                                            .41829
                       .12103
 -.17622
```

0

.

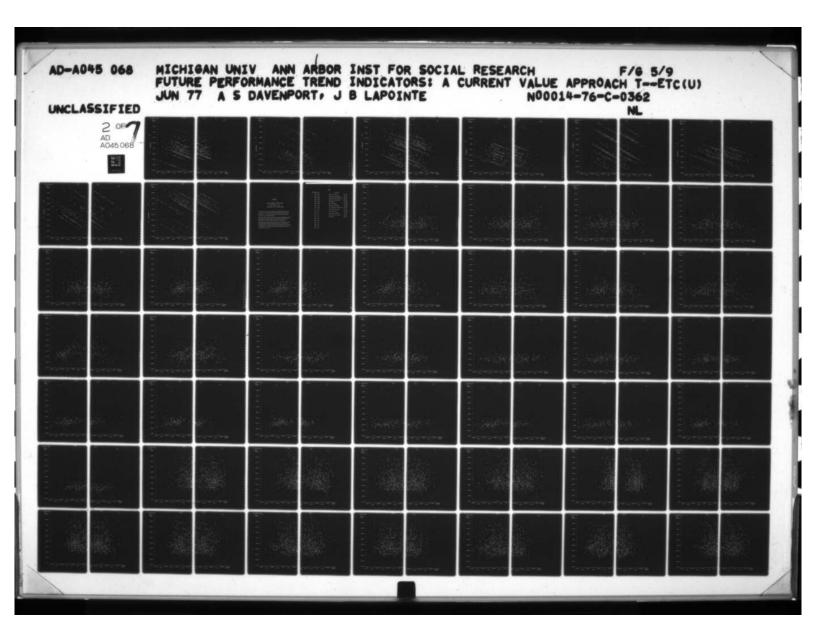
3

- -

-.63267 -.11428

.14492 -.37348

v971 .66331 .40412

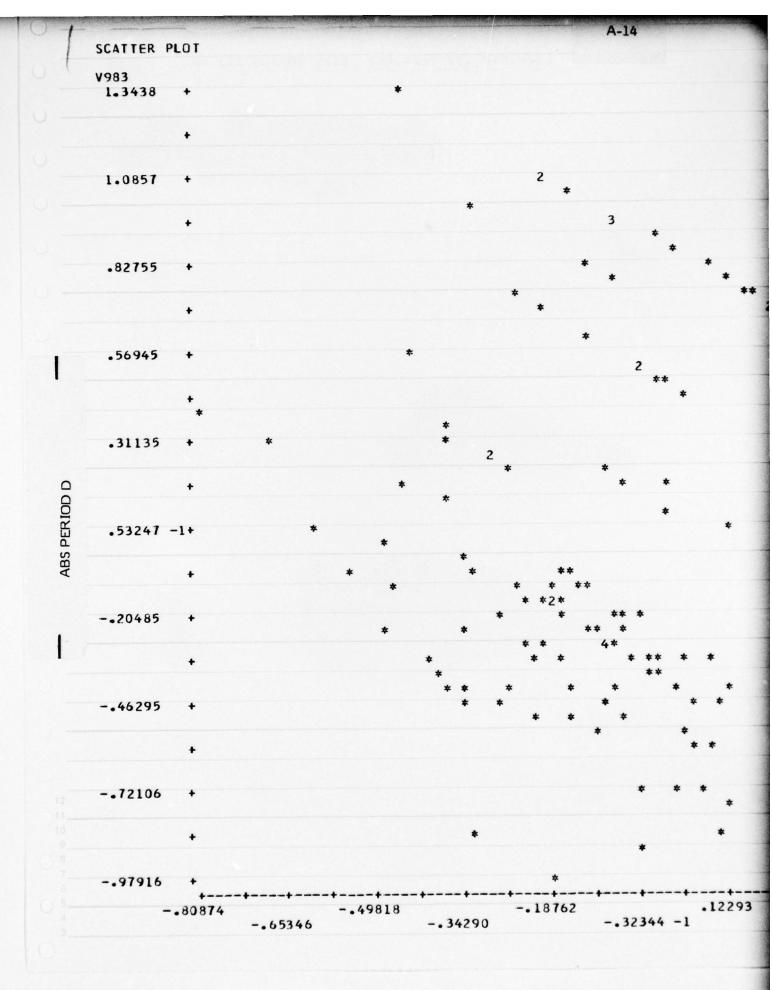


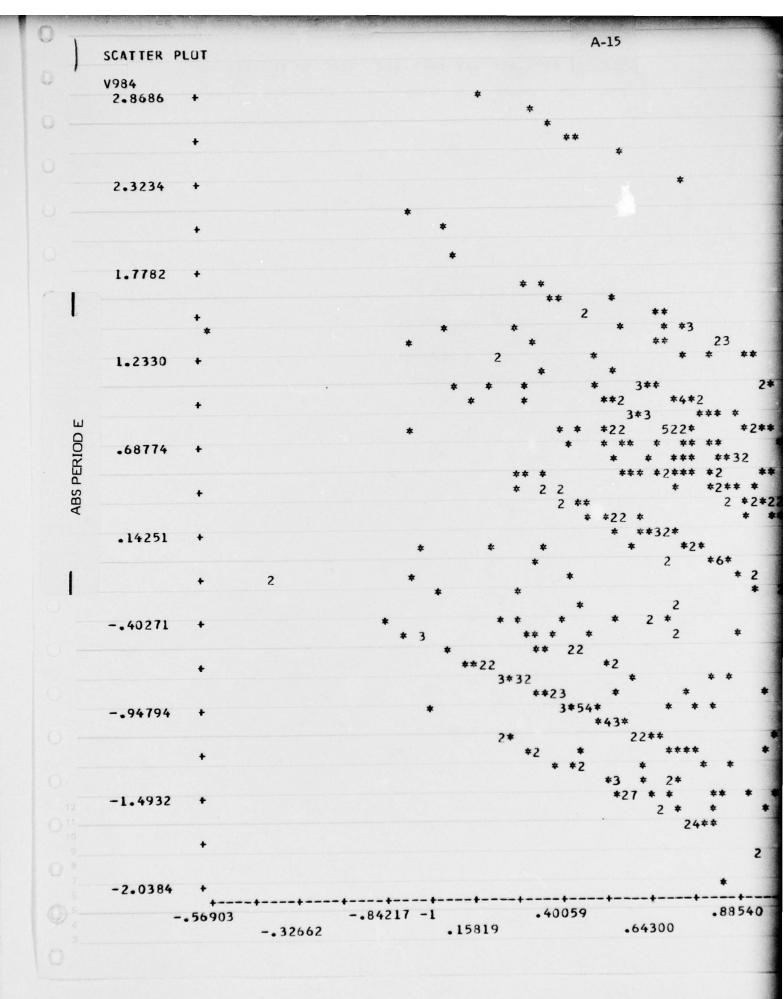
2 OF AD A045068



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-F

```
A-13
 * *
23*
* 2*
       2 22
* **2 * ** *3*
      3 + 2 +
                 242
      **2**3**
3*2
2*54*
*3 *28422*
*42742
      *4274252
            244 222*
                232****
                     **222**
                          .17231
                                                           V972
                                               .59252
 -.24789
                                                             .80262
             -.37789 -1
                                      .38241
```





```
2 2
2 **
*23
3*54*
                               2
                                                             V974
1.6126
                                                 1.3702
                        .88540
40059
                                     1.1278
            .64300
```

0

0

)

0

9

•

•

•

•

•

				A-16					
ABS PERIOD F	SCATTER	PLOT							
	V985								
	2.6545					* *			
							*		
		+						*	
	2.1781							* *	
	2.1101								
		+							
	1.7017	+							
		+				J-			
				*					
	1.2254	+							
						*			
		*	*	*					
		*	*		* 2		*		
	.74898	+	*	*	**	3**			
					* *	4	*322 *2422*		
		+	*	*	**	* 2 **	2*2		
	272/1			42	2 *	**	* 2 2*	*2 *	
	.27261	•		*2	**	5*45	2*	*	
		+		**	* *	2*4	2 *	*	
					**	24*	2 * 2*2*3 2*22*	* **	
	20376	+		**	* 2	* **22	* *	*	
		*	* * *		3	2 2 2	* * ***	*	
		+	* *			**2	*2	*	
				* *	* *	* 2**	2 * ***	*	
	68014	+	* *	*3 *		*	* *	**	
				* *	** *2 * ***2		* 2	***	
		+				* * *2*	**		
						* *	** *	*	
	-1.1565	+					* ** *	** *	
		•						*	
	1 (222						*		
	-1.6329	+	-+	+	+	++	+	-++-	
	-	.52009	32708	13408	.58921 -	• 25192	.44493	.63793	
			32108		. 72451 -		. 44493		

1.2544

1.0359

V976

1.4728

. 38073

* * 2

* * * *

* * *

* * *

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* * *

* * *

APPENDIX B

FOR TVE PERIODS A-I AND

ABS PERIODS A-J VS. SOO INDEX SCORES

This appendix contains the regression residuals $(Y-\hat{Y})$ from each of the TVE and ABS performance periods plotted against the scores on each S00 index. Thus there are 13 plots (one for each S00 index) for each of 19 performance periods.

The codes below identify the performance period and SOO index plotted on each graph and are located at the extremes of the horizontal (SOO code) and vertical (period code) axis of the graphs.

The graphs are arranged by SOO index within each performance period. Thus the graphs of the TVE period A residuals vs. each of the 13 SOO indices appear together and precede the graphs for the TVE period B residuals, etc. The order of periods and indices within periods is as given in the codes.

CODES

RESIDUALS FROM:	SOO INDEX:	
TVEA - V941	Supervisory Support	- 176 SUP
TVEB - V942	Supervisory Goal Emphasis	- 178 SUP
TVEC - V943	Supervisory Work Facilitation	- 180 SUP
TVED - V944	Supervisory Team Building	- 182 SUP
TVEE - V945	Peer Support	- 184 PEER
TVEF - V946	Peer Goal Emphasis	- 186 PEER
TVEG - V947	Peer Work Facilitation	- 188 PEER
TVEH - V948	Peer Interaction Facilitation	- 190 PEER
TVEI - V949	Human Resources Primacy	- 196 HUM
ABSA - 980	Communication Flow	- 197 COMM
ABSB - 981	Motivational Conditions	- 198 MOTI
ABSC - 982	Decision Making Practices	- 199 DEC
ABSD - 983	Satisfaction	- 200 SATI
ABSE - 984		
ABSF - 985		
ABSG - 986		

ABSH - 987

ABSI - 988

ABSJ - 989

1			B-4
1	SCATTER	PLOT	
'	V941 2.8248		
	2.0240		
		+	*
	2.3730	+	
		+	
	1.9212	+	
		+	
	1.4695	+	
		+	
	1.0177	+	
		+*	* *
			*
	•56590	+	* *
			* * *
		•	*
	.11412	+	* * * * * * * * * * * * * * * * * * * *
			* * * * * * * * * * * * * * * * * * * *
		+	** * * * * * * 2
	33765		* * * *** ** ** *
	55765		* ** * 3 **
		+	* * * *
			* * *
	78943	+	* * *
		+	
	-1.2412	+	*
		1.780	2.4956 3.2111 3.9267
			2.1378 2.8533 3.5689

3.2111 3.9267 4.6422 178 SUP 3.5689 4.2844 5.0000

2

3.0133 3.7400 4.4667 180 SUP 0 3.3767 4.1033 4.8300

	the state of the s		Statement of the Control of the Cont				-		Court Debugger Land	THE REAL PROPERTY.	The second second					STREET, STREET
1	SCATTER	PLOT N=	188 0	JT OF	2319	941.	V941	vs.	137.	.182	SUP					
'	V941 2.8248							*								
		+				*		*	*							
	2.3730	+														
		+					*									
	1.9212	+														
		+														
	1.4695	•				*										
															*	
		+														
	1.0177	+												*		
												*				
		+			*						*		*			
												*	*			
	.56590	+						*	k		*	*	*		2	*
					*		*					*	2 *			
		+			*				2	* *	* *	*	*		2	•
									*	* *	2* *	*		*		
	.11412	+					*	* *		*	* *	*	* *	**	*	
				*			•		*2	2	2 *	* :	**	2*	* *	2
		+		*	2	**	*:	*	*	* 2	* *	*	*	,	* *	2
		•			* * *			*		*	*	*	2			**
	33765	+				*		**	* 2 *	*	*	*	*2*	*		*
		*			*				2 .	2						
		+		*		*				*				*		
										2			*			
	78943	+					*			*		•	k			*
		+			*			*	*							
	-1.2412	++-	+	* +	-+	-+	-+	+-	+		+	+	+	+	+	-+-
		1.450			2.	2389					278			3.8	167	

1.8444

* 2 *

182 SUP 5.0000 3.8167 3.0278 4.2111 3.4222

4.7044 184 PEER 5.0000 3.5222 4.1133

3.8178 4.4089

1				B-8
SCATTER	PLOT			
1				
V941				
2.8248	•			
	+			**
2.3730	+			
	+			*
1.9212	+			
	+			
1.4695	+			*
	•			
1.0177	+			*
				*
				*
	+			2 *
				*
.56590	+	*		* * *
	*			* * * * * *
				2 * * *
	+			** 2 *
				* * * * * * *
-11412	+		*	* ** ** * 2
				* * * * * * *
				* 222**2 2 2 * **2 2
	+			* * ** ***2 ** * * *
				*2 * * 22 *2 * ** * *** * ** * *2 *
33765	+			* * * * ** ** **
				* 2 *2 * ** * *
			*	* * * 2 *
	+			* *
			*	* * 3
78943	+			* * * *
,				
	+			* *
				*
-1.2412	+		*	
-1.2412		++		.++++++++-
	1.5000		2.2778	3.0556 3.8333
		1.8889		2.6667 3.4444

1.8889

4.6300 188 PEER 5.0000 1.1500 3.8900

4.2600 3.5200

3.7933 4.1956 5.0000

SCATTER	PLOT			B-12	
V941 2.8248	٠			*	
	٠		* *		
2.3730					
				*	
1.9212					
1.4695				•	
1.4693					* *
	٠				
1.0177	•		*	*	
	+		* *	*	
•56590	•		*	* * * 3 *	* *
	+*	* *	* * 2	*	
-11412	•		* * *	** * * * 2 * ** * *3	*
	٠	* * *	* * 2 2 * *** 2 ** *	* * 2 * 2	* * * * * * * * * * * * * * * * * * * *
33765	•	* *	* 2 * ***** * * 2 **:	2 * * * * *	* * *
	•	* *	*	*	
78943		*	*	* *	* * *
			* *		
-1 2/12		*			
-1.2412	1.5000	2.20 1.8522	2.5567	2.9089	3.6133
		3722	2.,,,,,,	7.0	

3.2611

3.6133

2

3.9656

197 COMM 4.6700

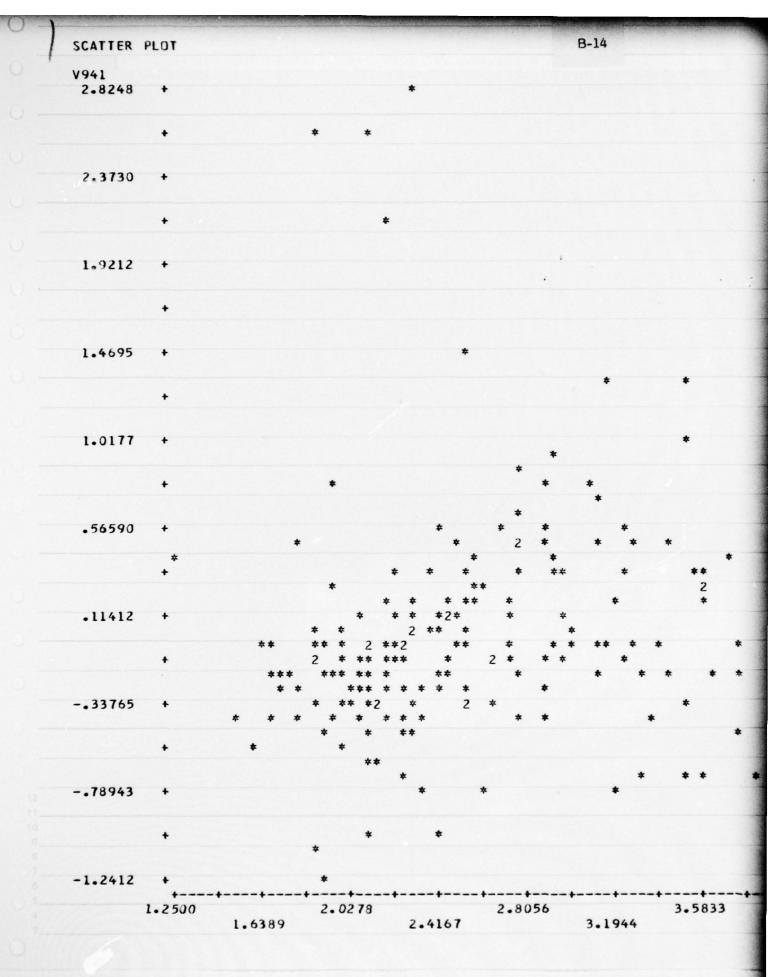
1.8400

2.1544

3.0978

3.7267

3.0978 3.7267 4.0411 4.6700



3.58 3.1944

3.9722

4.3611 199

199 DEC. 4.7500

3.2444 3.9467 4.6489 200 SATI 3.5956 4.2978 5.0000 B-17

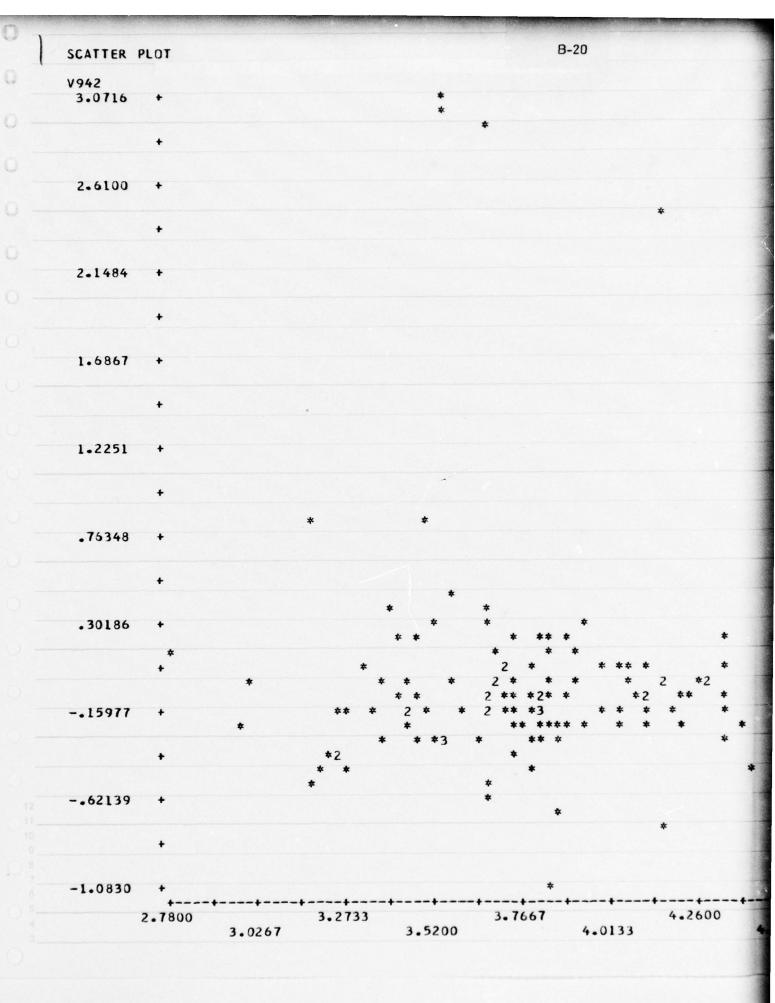
4.6422 178 SUP 5.0000 11 3.9267 4.2844 3.5689

```
SCATTER PLOT
V942
3.0716
2.6100
2.1484
 1.6867
 1.2251
 .76348
 .30186
                                2
-.15977
-.62139
-1.0830
                                            2.7911
                         2.1756
                                                              3.4067
       1.5600
                                  2.4833
```

4.0222 180 SUP 4.3300 2.7911 3.4067

3.0989

3.0278 3.8167 4.6056 182 SUP 5.0000



2

3.7667 4.2600 4.0133

4.5067

4.7533 184 PEER 5.0000

10%

3.4611 4.0767 4.6922 186 PEER 5.0000

3.1500 3.8900 4.6300 188 PEER 5.0000

4.6300 190 PEER 5.0000 3.8900

3.1500 3.5200

196 HUM. 5.0000 4.5978 3.7933 2.9889

3.3911 4.1956

```
SCATTER PLOT
V942
3.0716 +
2.6100 +
2.1484 +
1.6867 +
1.2251 +
 .76348
 .30186
-.15977
-.62139 +
-1.0830
             2.3367 3.0033
2.0033 2.6700 3.3367
                                                        3.6700
```

4.3367 197 COMM 4.6700 3.6700 3.0033

4.0033 3.3367

```
SCATTER PLOT
V942
 3.0716 +
 2.6100 +
 2.1484
 1.6867
 1.2251
 .76348
 .30186
-.15977
-.62139
-1.0830
             2.1889
                            3.0556
       1.9000
                                                     3.6333
```

198 MOTI 64.5000 3.6333 4.2111 3.0556 3.3444 3.9222

2.4500 2.7500

3.0500

-1.0830

1.2500

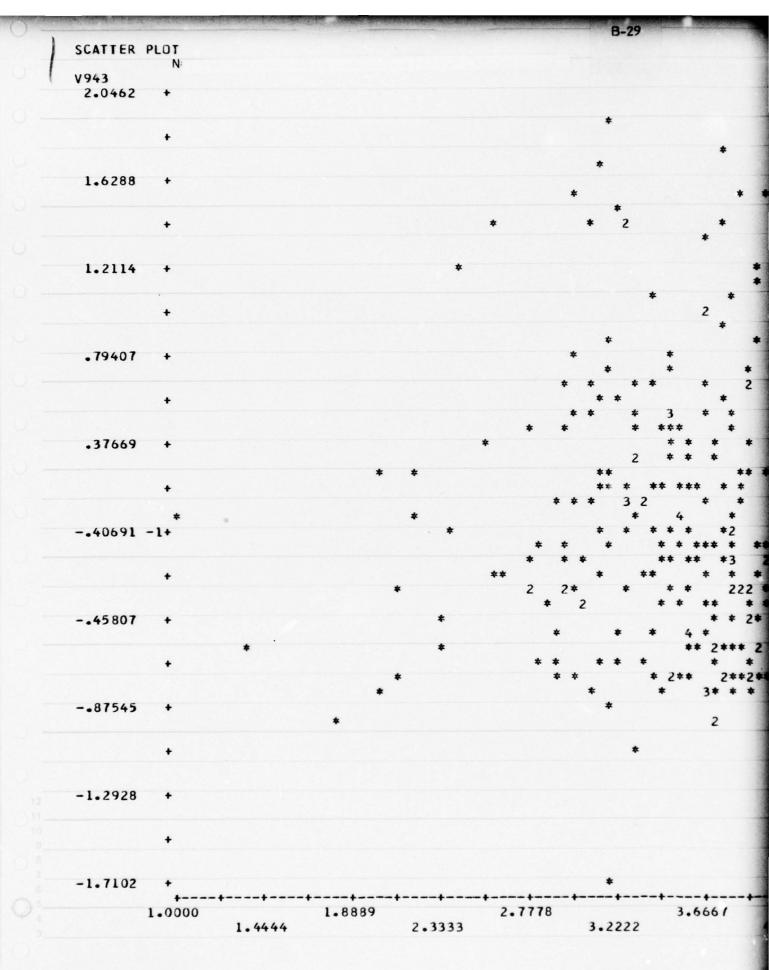
* * *

3.0500 3.6500 199 DEC. 2.7500 3.3500 3.9500

3.4844

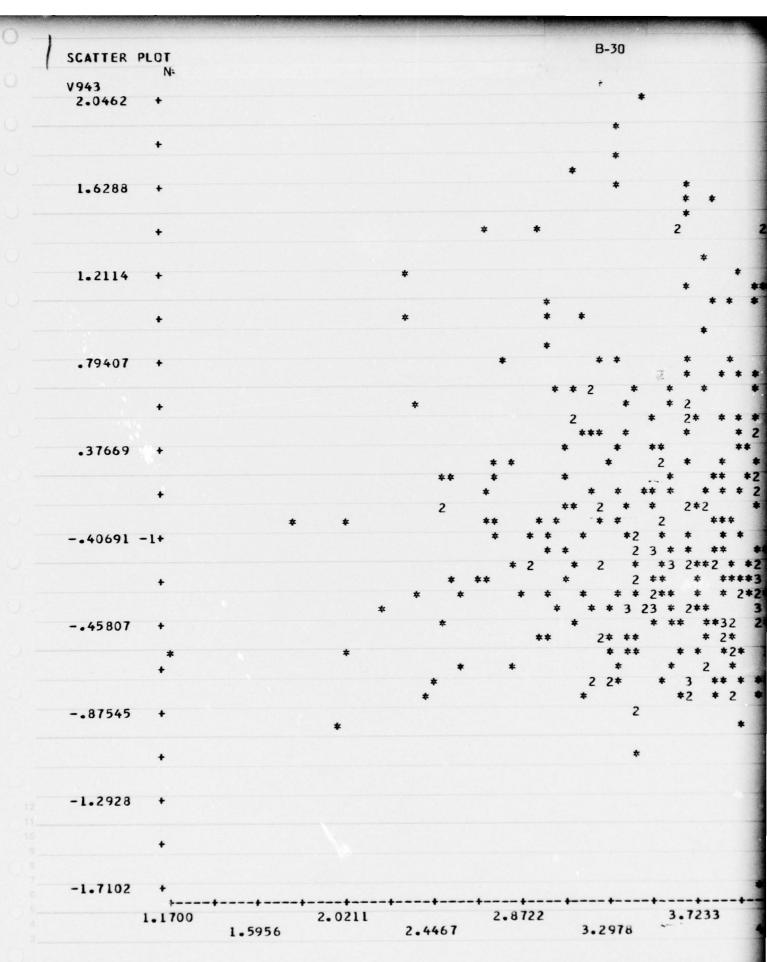
3.8133 4.1422

4.4711 200 SATI 4.8000



4.1111 3.2222

176 SUP 5.0000



3.2978

4.1489

2.8722

67

SCATTER	PLOT							B-3	31	
V943										
2.0462							*			
2.0										
						*				
			*							
1.6288						* *	*			
1.0200						*		*	*	
	+			*	*	**		*	*	*
1.2114	+						*		*	*
							**		* *	*
				*		*		*	* *	
								*		
704.07			*				*	*	*	**
.79407			*	*	*	*		2 *	*	
					*	* *	* *	*	*	
	+			2 *	2	**	**	*		* 2 *
				2 2	** *	2	* *	*	**	**
.37669	•					*	* **	*		*
			* *	* *		*	* *	*	* 2 · ***	2 * *
	+		*			**	* *	2 *	* **	
			*	**	* *	* *	* * *	*	2 **	* **
40691	* -1+	*	*	* * *	*	**	-	** *		* **
					* * *	*	*2*2	* *	*	* ***
	+		*	* * *	*	2*2*		*4	*** *	* * 3
			*	2 * 1	* 2	2 *	*	* *3	*2	* **2
			* * **		* *	* *	****	* 2	**3	**
45807	+		*	*	*** *	* *2		****	**	****
	*		*			*	2		* *22	
	+			,	* *	* 2	*	* * 3 * *	***	
			*		* **	2*	**2	*3**	*	* *
87545	+					*			*	*
		*					*	*	* *	
	+					*				*
-1.2928										
2										
1 7102								*		
-1.7102	+	-++	-+	++-	+	+	+	+	-+	++
	1.0000		1.8889			2.7778	8		3.6	667
		1.4444		2.33	33		3.	2222		
										19.00

2

4.5556 180 SUP 5.0000 2.7778 3.6667

3.2222 4.1111

1	SCATTER	PLOT					B-32	
1		PLUI						
	V943 2.0462	٠			•			
		٠			*			
	1.6288	+		*		*	*	
							*	* *
		+			* *		* *	2
	1 2114				*		*	*
	1.2114	•					*	* **
		٠				*	2*	
							* *	
	.79407	•		*	*	*	*	** *
		+				* **	* *	*
					*	* * *		* * * *
	•37669	•			* * *	* * *	* * *2	* **
		+	*	2*	*	* *	* * * *2	2 * ***
				*	2	* ** *	**** * *2 *	* * *
	40691	* -1+		*		* *	222 *	*
					2* *	* * ** * * 2*2* * *	*2***	* *
		+	*	*		* * * *	2 * ***	*2 *** ***
	45807	+	**		*		22 ****	2 2 * * * * * * * * * * * * * * * * * *
	• 15001		* *			* * 2	2 * *	
		•			*		* *	2 * *2
				*	*	**	*3 * *3	
	87545			*			*	2 *
		+					*	
	-1.2928	•						
		+						
	-1.7102	+	++	+	-++	-++	* -++	
		1.0000	1.4444	1.8889	2.3333	2.7778	3.2222	3.6667

2 * * 2 * 2 * 2 2 2

182 SUP 5.0000 4.5556 3.6667 2.7778 4.1111 3.2222

0

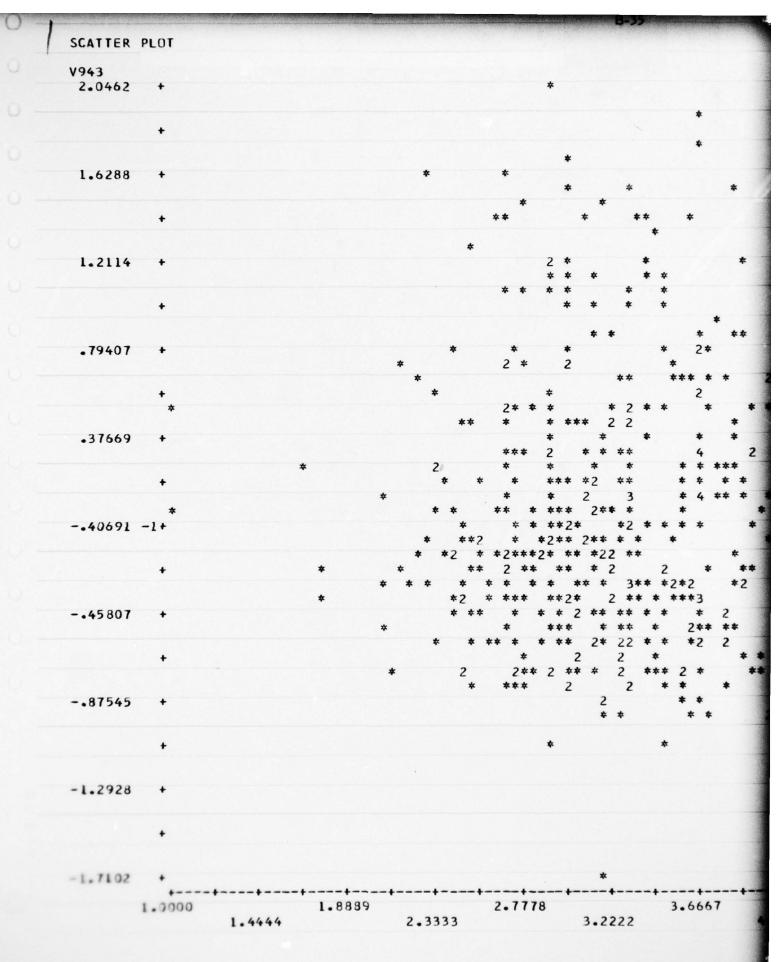
SCATTER	PLOT					B-:	33	
V943 2.0462	+							
						*		
	+		r					
							*	
1.6288	+					*	*	
						* *	*	*
	+					*	* 4	* *
						*	*	
1.2114	+						* 2	
						*	* 2	
	+						*	* *
						*	* * *	*
.79407	+					* *	**	2
					*	*	* 2 * **	
	+					*	* ** .	
	*					2 *		* * 3
.37669	+					* * *	2 * * 2	** *
•3.007							** 2 2	
	+					*	* 2 2 * ** *22 2*	*
						* *	* 2*2	2 * 24
40691	-1+	*			*	* *	* * ** * * ** 2 *	* 3
******							** *2*3	
	+			*		****		22* ** 21
	•					* 2*	** **242	2* *
45807	+					* 2 * 2	* * 2° 2° 2° 2° 2° 2° 2° 2° 2° 2° 2° 2° 2°	3** *
•45001						*	* * *;	23*
	+				*	* **	2** * 2*	2**
						2 * * **	* ****2 **	* 2 3
87545	+					***	*2 * 2	* *
					*			* **
	+						* :	*
-1.2928	+							
-1.2920								
	+							
1 7102				*				
-1.7102		++		·		-++		-+
	1.0000	1 4444	1.8889	2 2222	2.7778	3.2222	3.6667	4
		1.4444		2.3333		3.2222		

2.7778 3.6667 4.5556 184 PEER 3.2222 4.1111 5.0000

333

1		
SCATTER	PLOT	B-34
V043		
V943 2.0462	+	
		•
		*
1.6288	+	* * * *
		* *
	+	* * * * *
		*
1.2114	+	* * 2
		* * * * * *
	+	* * *
		*
.79407	+	* * * * * * *
•17401	*	* * **
		2 * *4 *
	+	* * * 2 * * 4 * * *
		* * *****2 * *
.37669	+	* * * *
		* * * * * * * * * * * * * * * * * * * *
	+	* * * * * * * * * * *
		*
40691	-1+	2 ** 3* * * * * 2 * 2 * * 2 2* 3 * * * *
		* * * * 2 ** * * 2 * 2 * * * *
	+	* * 2 24 *23***
		* * ** 2 *** * 2* * * * 22 * * 2
45003		* * * * 2 **2* 2* * 3 2 **2 *
45807	+	* * 2 2*2 ** * *22 * * * * *** * * 2 *** * *
		* * 5 2** ***** * * ***
	+	* 2 *2 * * * * * * 2 22**2 **2* 42 *
		* 2 22**2 **2* 42 * * 2 * * * 3 * * *
87545	+	* * *
		2 2 * *
	+	* *
		*
-1.2928	+	*
	+	
-1.7102	+ +	*
	1.5000	2.2778 3.0556 3.8333
		1.8889 2.6667 3.4444

3.4444



```
B-35
            * * ** 2* 22

* 2 2

2** 2 ** * 2

*** 2 2
    2
                                                                             188 PEER
5.0000
                                                                  4.5556
                                      3.6667
         2.7778
                                                  4.1111
                      3.2222
333
```

SCATTER	PLOT					B-36	
V943 2.0462					*		
						*	
	+						
					*	*	
1.6288	+			*	*		
					*	* *	
	+			*	*	* *	
				*			
1.2114	*			* *	* *	*	*
					**	** *	* *
	+						*
.79407	+			*	* *	*	* * *
.,,,,,,,				3	* *		* *
	+			*	*	* * *	*** *
		*		* *		2 * * 2	* * * *
.37669	+				*	* ** *	*
		*		*	** *	2 * * * *	2 2 *
	+				-	* * * *	* ** *
	*			*	3 **	2 * * * * 2*	* 22
40691	-1+		*	* * ***	*2 *	3 * * * * * * * * * * * * * * * * * * *	2 2
			*	* *2	* 222 2**	2** * *	*
	+		2	* * *		3* *** **** 2 2	*
45007			2		** *23	**2 3 *	** *
45807	•				*	** 2 2 3 2* 2 2*	
	+			* **		2 **** ** * **	* * * 2
				* ***	* * * *	2 ** *2* *	2 3*
87545	+			* *2	**	* *	* * *
						* *	*** 2
	+					*	*
-1.2928	+						
	+						
-1.7102	++	+	++	++		*	
	1.0000		.8889	2 2222	2.7778	2 2222	3.6667
		1.4444		2.3333		3.2222	4.

2

2

3.6667 4.5556 2.7778

4.1111 3.2222

333

190 PEER 5.0000

2

SCATTER						
V943	N= 44					
2.0462	+					*
	+					*
						*
				*		
1.6288	•		*		* *	* *
					* *	
	•			*	*	2 * *
					*	
1.2114	+			*		2 * 2
				* .	* * *	*
				*	* * *	* * *
						*
						* * 2
.79407	•		*	* *	* *	* * * * 2 *
				*	* * 2*	* *
	+			*	* * *	*
	*		*	24	2 * * *	* 2 * * ** 2 *
.37669	+			_	2 **	
				* **	* * **	
	+	*	*	* ***	* 2 * ** *22**	* * * *
		The state of the s		*	2 *	2 * 2** * *
		*	*		* * * *2	* 2** 2 *
40691	-1+	* *	*	*	* 3** 2** * * *	* ** ** 2
		* *	* ** *		** * 2 32 *	
	+		*	** * * *	* * *	* * 2 * ** 2
		*	* *	*2*	** ** ** *	** ** * * * *3 2 ** **4 * 2* 2
45807	+		** *	* * *	* ****	
			2*	* *	*	* * **** *
		* *	*	* *	* * * *	* * *2* 22**** * ***
	•				* * * * *	2 2** 2 *
		*	* *		** * *	* ** **
87545	+			*	* **	* * * *
				•		** * *
	+			* *		
-1.2928						
-102720						
	•					
-1.7102	•				*	
	1.0000	+	.8889	++-	2.7778	3.6667
	1.0000					3.0001

3.2222

```
B-37
                                 2
                                                              196 HUM.
5.0000
                              3.6667
                                                    4.5556
       2.7778
                  3.2222
                                        4.1111
333
```

```
SCATTER PLOT
V943
2.0462 +
 1.6288
 1.2114
 .79407
.37669
-.40691 -1+
-.45807 +*
-.87545
-1.2928
-1.7102
                         2.2044
                                           2.9089
       1.5000
                                                              3.6133
```

1.8522

2

3.6133

2.9089 3.2611

3.9656

197 COMM 4.6700 4.3178

1.8400

2 *2 * 2 3 2 * 198 MOTI 5.0000 4.2978 3.5956

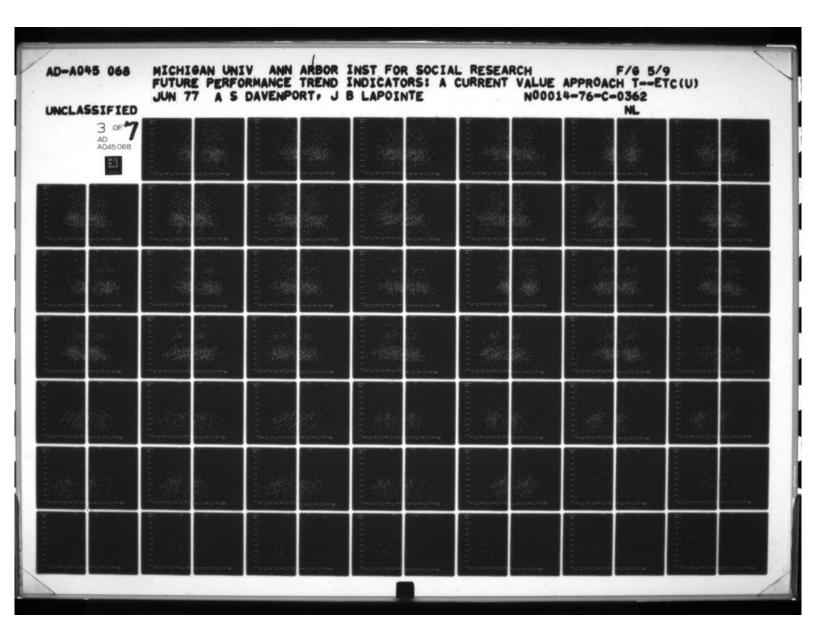
B-39

3.2222

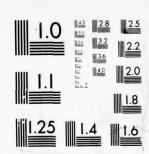
```
B-40
```

2.7778 3.6667 4.5556 199 DEC. 3.2222 4.1111 5.0000

3.0944 3.8567 4.6189 200 SATI 3.4756 4.2378 5.0000



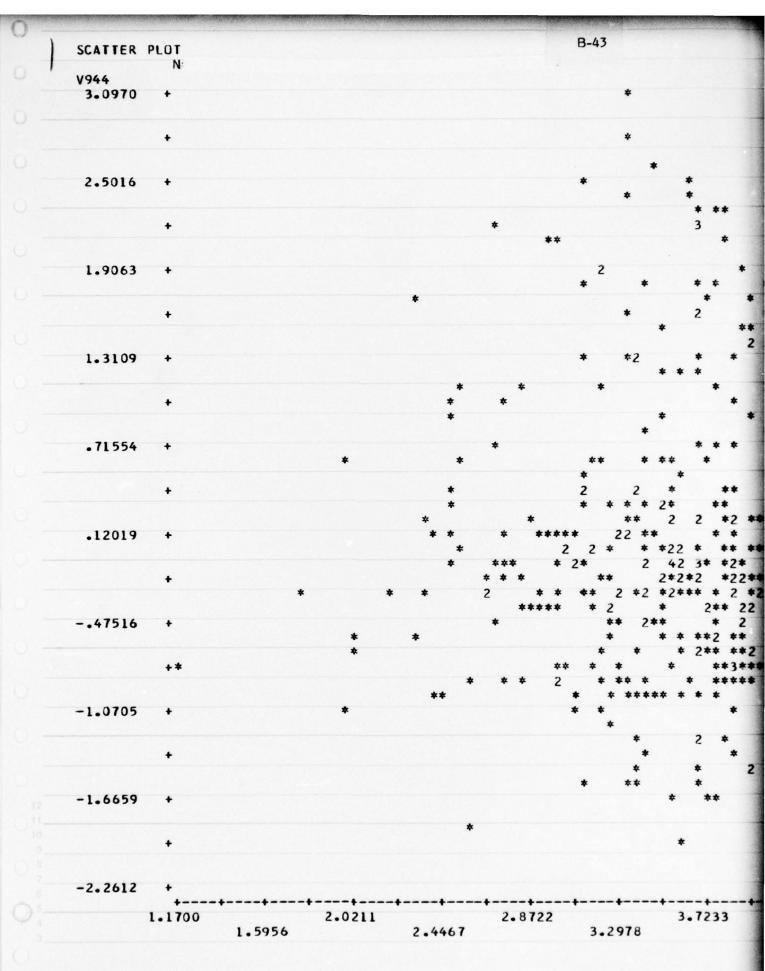
3 OF AD A045068



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-7

4.5556 176 SUP 5.0000 3.6667 2.7778

3333 3.2222

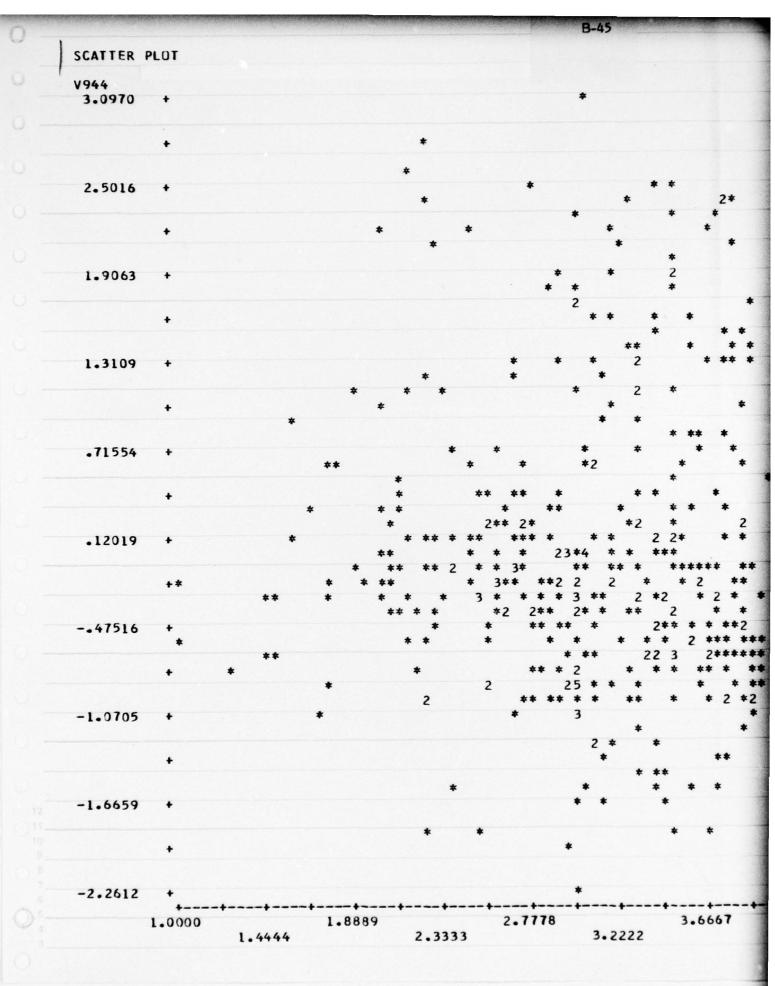


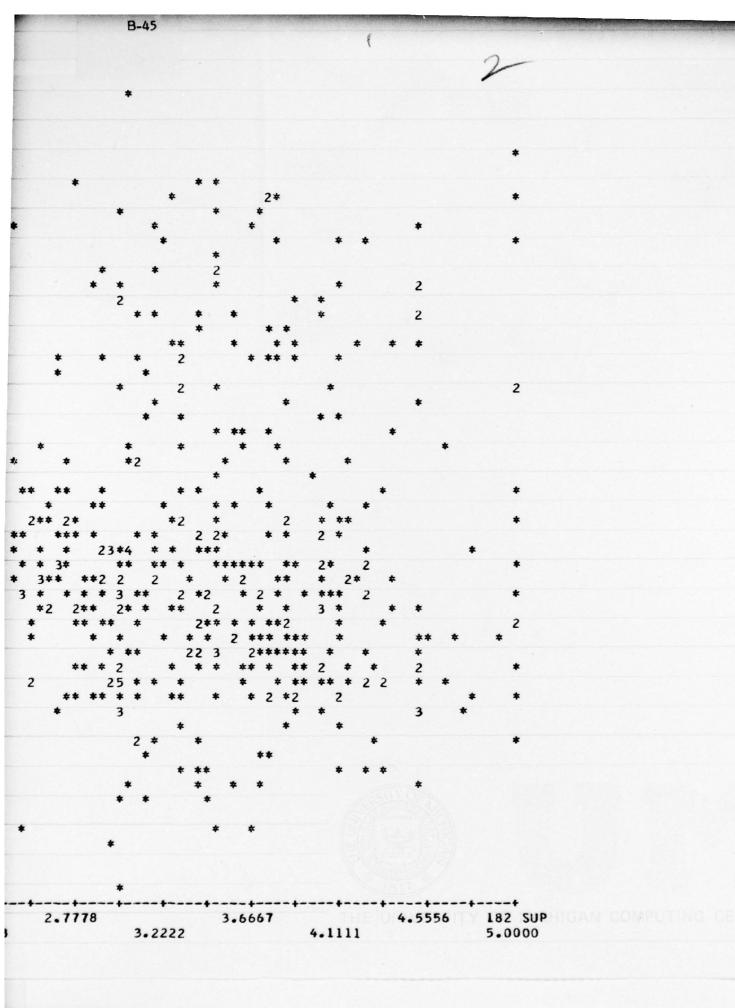
1.4444

3.6667

2 2

2.7778 3.6667 4.5556 180 SUP 3.2222 4.1111 5.0000





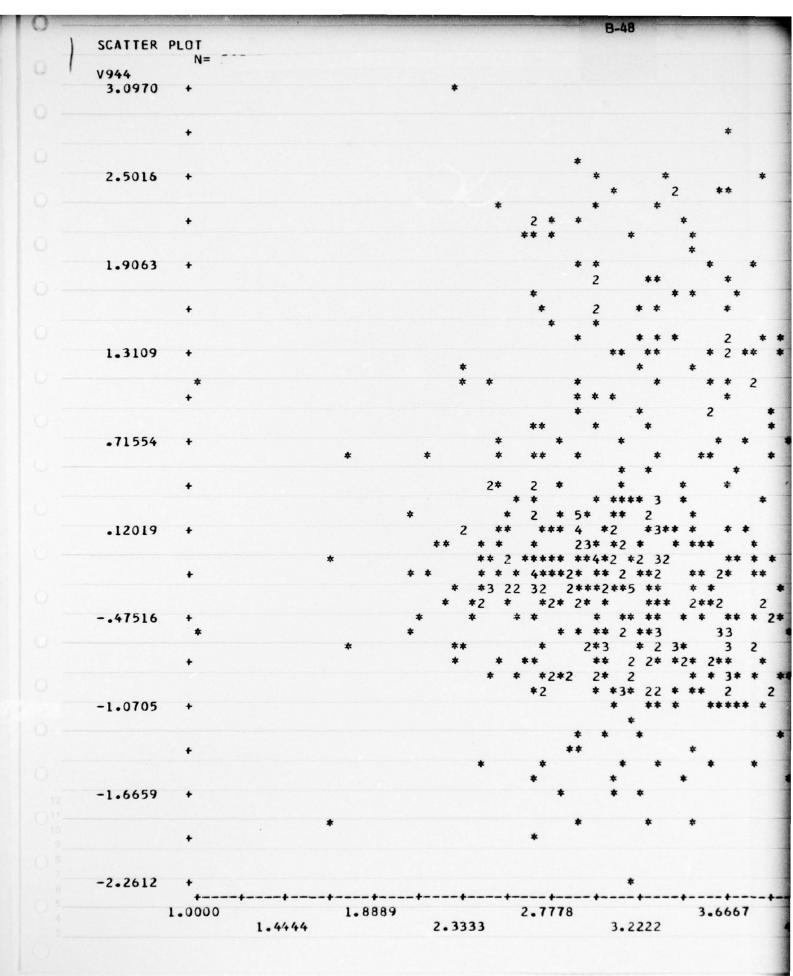
** ** 3*** 53* 2 23 *33 222 2*3 23* 2*253*3 22 * 2**3 *5

2 **3* 2 *2 * 2 * 2* ** 3* 33* * * *22 * *2* **2** * 2 5*2*

.7778 3.6667 4.5556 184 PEER 5.0000 3.2222 4.1111

SCATTER PLOT	
V944 3.0970 + *	
*	*
2•5016 + ** * * * * *	*
* * * * * * * 2 2 *	
** * **	
1.9063 +	. *
* *** * * *** *	* *
1.3109 + 2 * *	* ** 2 * 2 * 2
* * * * 2 *	* * *
* **	* * *
* ** * •71554 + * * * * 2 * * * *	* * * *
* * * * + 2* ** * *	* *
* * ** *2 ** * 2* *	
	2 *** 2 **** ** *2* * 3
+	22* *
* * * 2* 22* ** * * * 2 * * -•47516 +	* 2 2 2 * **
2 * * 2* * 2 2* * * * * 2 2 * 22* + * * 2 3 3 ** 2 ***	***2 * 2 232 ** * **
* * ** 22 ** * 5 5 *** *** 6	22* 2 2 21 *2*
* 2	* *
2 * * * * * * * *	
** * *	* *
* 2 *	
9	
-2.2612 + *	

3.4444

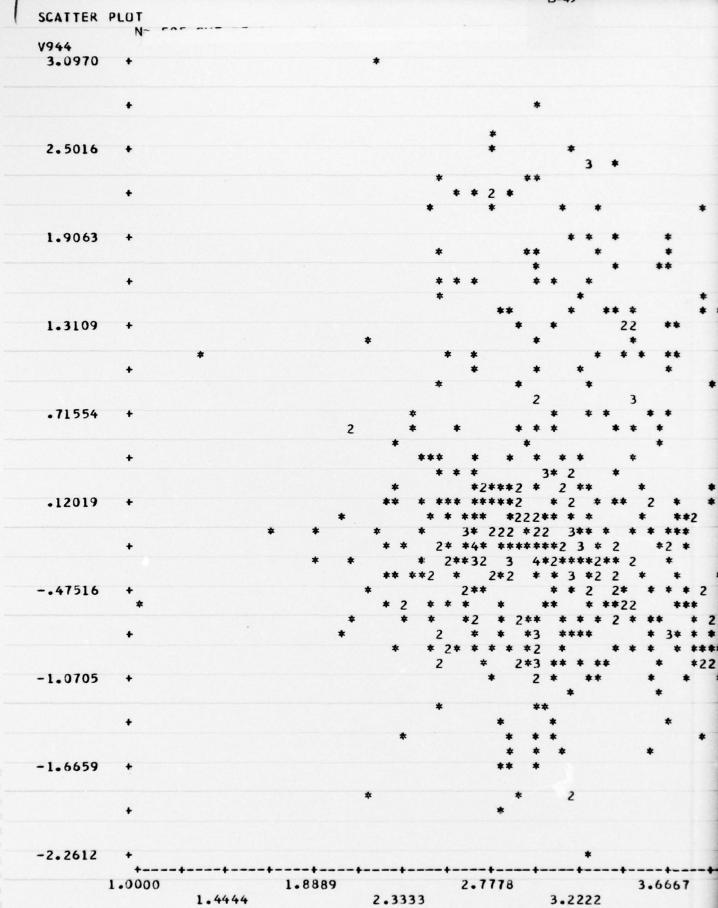


3.6667 2.7778

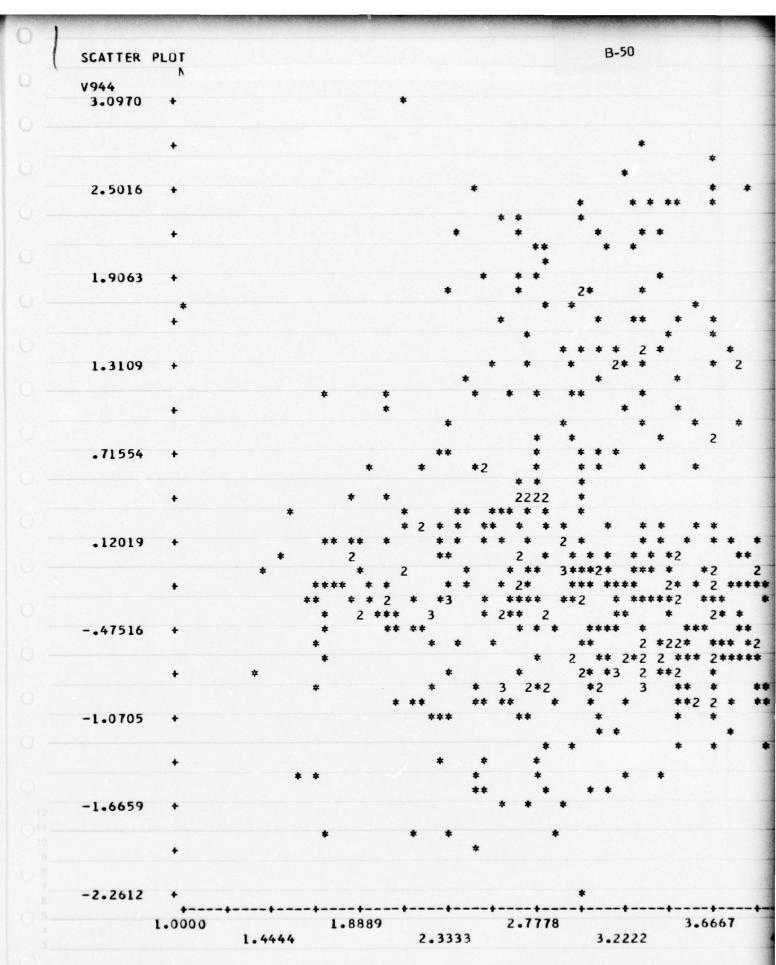
4.1111

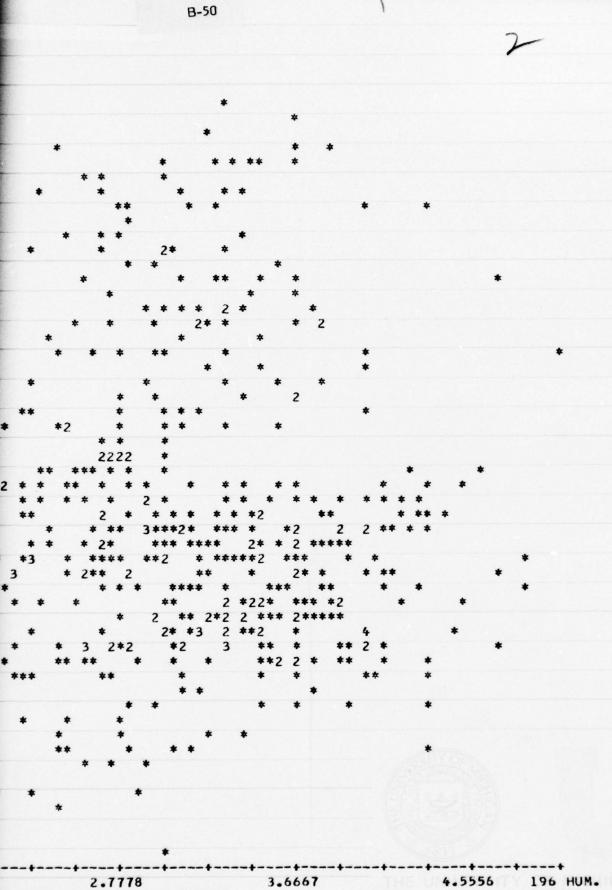
3.2222

4.5556 188 PEER 5.0000

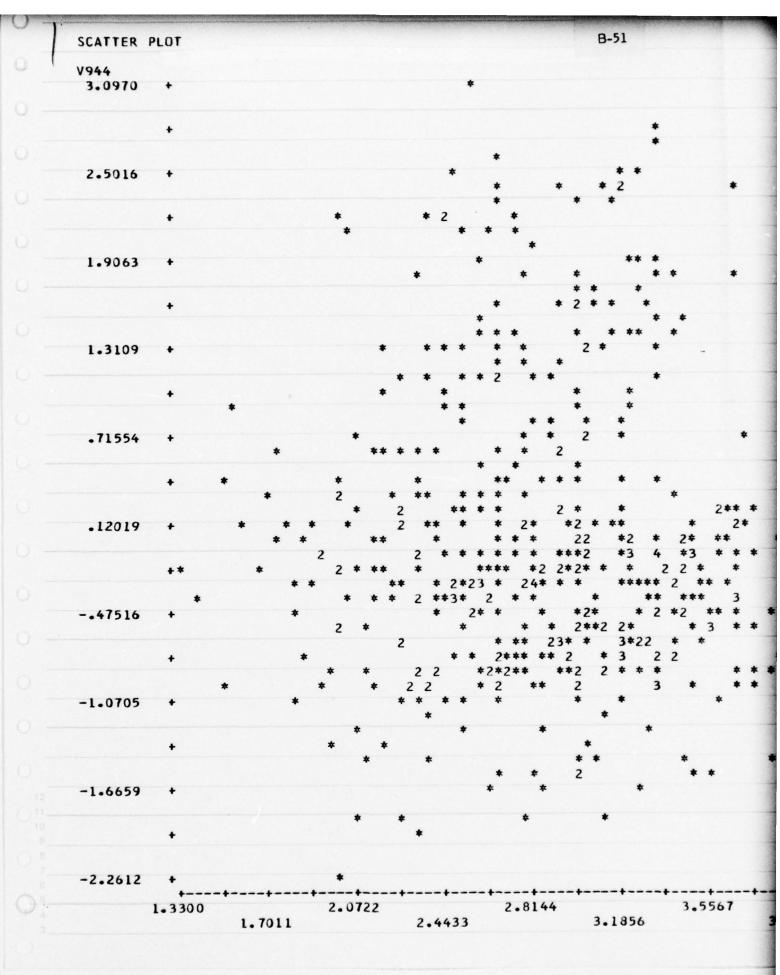


B-49





4.5556 196 HUM. 5.0000 3.2222 2.3333 4.1111



2.8144 3.5567 4.2989 197 COMM 3.1856 3.9278 4.6700

2 4.6456 TY 198 MOTI GAN CON 5.0000

3.9367

3.5822

4.2911

3.2278

```
4.5556 199 DEC.
5.0000
2.7778
                     3.6667
          3.2222
                               4.1111
```

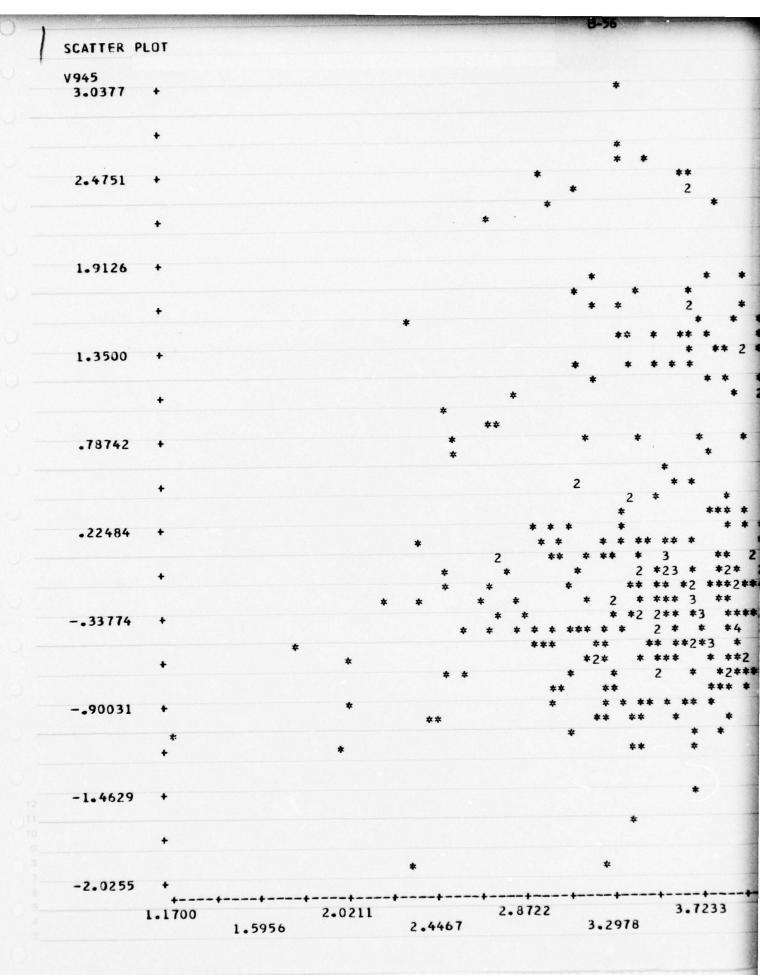
SCATTER	PLOT					В	-54			
V944 3.0970	+					•	*			
	•								*	
								*		
2.5016	+						*	* *		*
	•				*	* *	*	*	3	
									,	*
1.9063	•					* 1	* *		**	
	•				* *	*		*		* *
						*		2	*	* 1
1.3109	•					*		*	***	* *
	+				*	**	*	*	**	**
						*	2		**	
.71554	•			*	*	* * *	*	***	*	
	+			*	*	*2				2
				*	*	**		2** ** *	2 **	* **
.12019	+			* * **	*	* * **		** * 32	*	2* 2
	+*			**	** 7	_	**3 ** 22		* 3	2*
	**			* **	2 *	*** *	** *2	2 23	* 3*	22
47516	+			**	* * *	** 3	**	**2 *	32 *	
		*		*	*	*		* **	*23	2 *
	+			*		*	* *	* **	*2* *	* *2**
				*	*	2		*** *		
-1.0705	•					*			2 2	
								* *		* **
	•					**	**		2	*
-1.6659	+							**	-	*
						*	*	*	* *	
	•									
-2.2612	٠.							*	4	
	1.2900	+	2.1144		2.93	89		3	3.763	3
		1.7022		2.5267		3	.3511			

					B-55
SCATTER	PLOT				
V945					
3.0377	•				
	•				*
2.4751	•				* 2 *
	+				*
1.9126	•				
					* *
	+				**
					* * *
1.3500	+				* ** *
					* ** *
	+				* * *
				*	*
.78742	+		*		* 2
					*
	+				* 2
					* *
.22484	+				* * **
					* * * **
	+				** * * * *
					* * * 2 **
33774				*	*
					* 2* *** 2* 2
	+ .			*	** * * *3*3* * * ** * 2*
				*	** * * * * *
90031	+*				** * * * * 2 2**
•,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			*	*	* * ** *
	+	*	*		* * *
-1.4629	+				
	+				
				*	
-2.0255	+		+	+	*
	1.0000		1.8889		2.7778 3.666
		1.4444		2.3333	3.2222

3.2222

4.1111

4.5556 176 SUP 5.0000



2.8722 3.7233 4.5744 178 SUP 3.2978 4.1489 5.0000

3.2222

1.4444

3.6667

3.2222

1.8889

1.4444

2.3333

2.7778

SCATTER PLOT

3.0377 +

2.4751 +

1.9126 +

-2.0255

1.0000

V945

```
B-58
2
2.7778
                     3.6667
                                           4.5556
```

182 SUP 5.0000 3.2222 4.1111

							B-59	
SCATTER	PLOT						. 6-77	
	N=							
V945							*	
3.0377	+							
	+							
						*	*	
2.4751	+					* 1	*	* * *
						*	*	*
							*	*
	+						*	•
1.9126	+						*	
1.7120								* *
							*	
	+					*	* *	* *
							*	* *
						*	* *	
1.3500	•							2 * * 2
						*		
	*				*	*		* *
	+							
							*	
.78742	+			*			*	2 *
• • • • • • • • • • • • • • • • • • • •						*		
								* *
	+							**
						2		* *
						*	* 2*	
•22484						•	* *	* 2 *
							*	* 3* 4
	+					*	*2* *	* 4** 2
								** 2**33*
							* ****	
33774	+						* *	22*3**4* *
								** 22*23 **
					2		**	2 * 6*2*
	+							2 *** 2 * *
					*	2	*3 **	** 23 * 2 * *
00031		*				•	*	*2*2 ** 3
90031	+					*		22* 2
						*		* *
	+						**	* **
-1.4629	+							*
								*
	•							
								* *
-2.0255	+							
2.0233	+	-++	++	+		-+	++-	+
	1.0000		1.8889		2.7778			3.6667
		1.4444		2.3333		3.2	222	4

2 * * 2 * * * * * 2 * * * * * * * * * * * *

* 2 * * * * * * * *

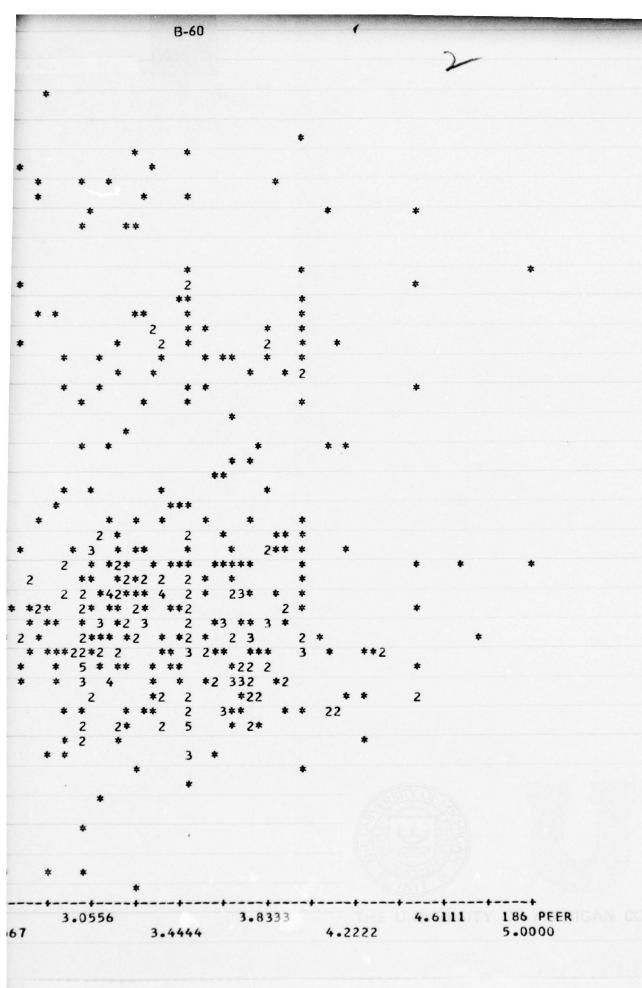
**2*2 ** 3 * * * 2 * * * 22* 2 22 * * * * * *

*

• •

2.7778 3.6667 4.5556 184 PEER GAN COM 3.2222 4.1111 5.0000

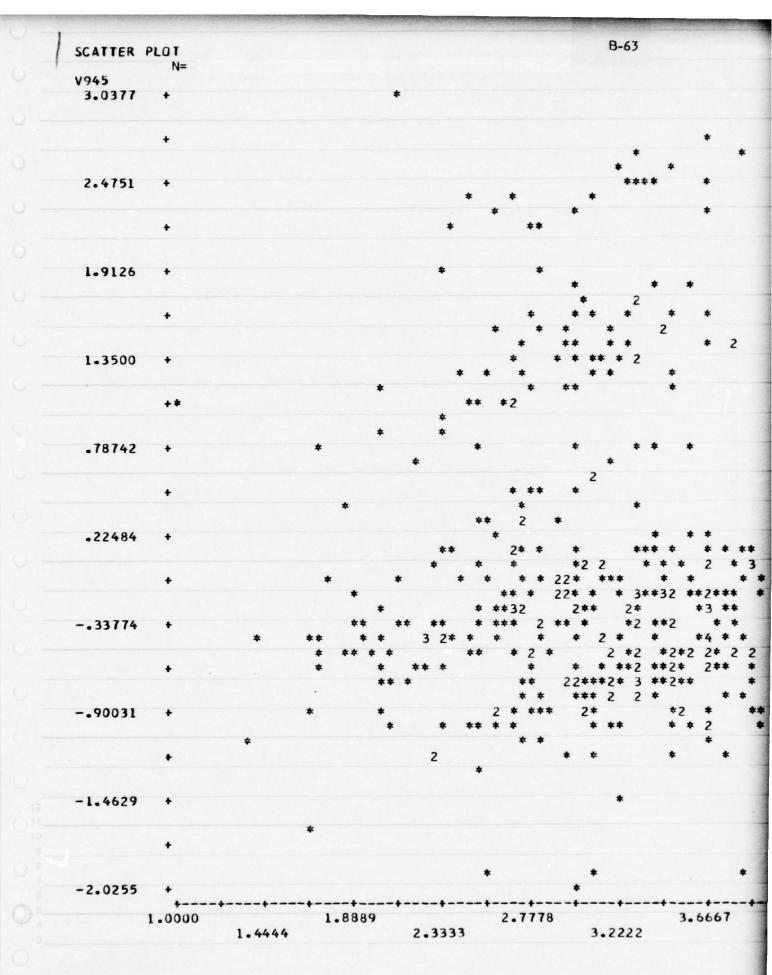
SCATTER	PLOT			B-60
V945 3.0377	+			*
360311				
	+			•
				* *
2.4751	+			* * * * *
2.4731				* * *
				* * **
	+			
1 0126				* *
1.9126	•			* 2
				**
	+			* * ** * * * * *
				* * 2 * 2 *
1.3500	•			* * * * * * * * * * * * * * * * * * * *
		*		* * * *
	+*			* * * * *
			*	*
.78742	+		*	* * * *
				**
	+		*	* * * *
				* * * * * * *
-22484	+			* 2 * 2 * ** * * * * * * * * * * * * *
				* 2 * *2* * *** **** *
	•		* *	* * 2
			*	2* *2* 2* ** 2* **2 2 *
33774	+		* *	
			*	2** * 2 * 2*** *2 * *2 * 2 3 2 * * ***22*2 2 ** 3 2** *** 3
	+	*		* * * 5 * ** * ** *22 2
				* * * 3 4 * * *2 332 *2 2 *2 2 *22
90031	+			* * * * * 2 3** * *
				2 2* 2 5 * 2*
	+			* * 3 *
-1.4629	+			
				*
	+			,
				* * *
-2.0255		či. e		*
	+	++	2.2778	3.0556 3.8333
	1.5000	1.8889	2.2118	2.6667 3.4444



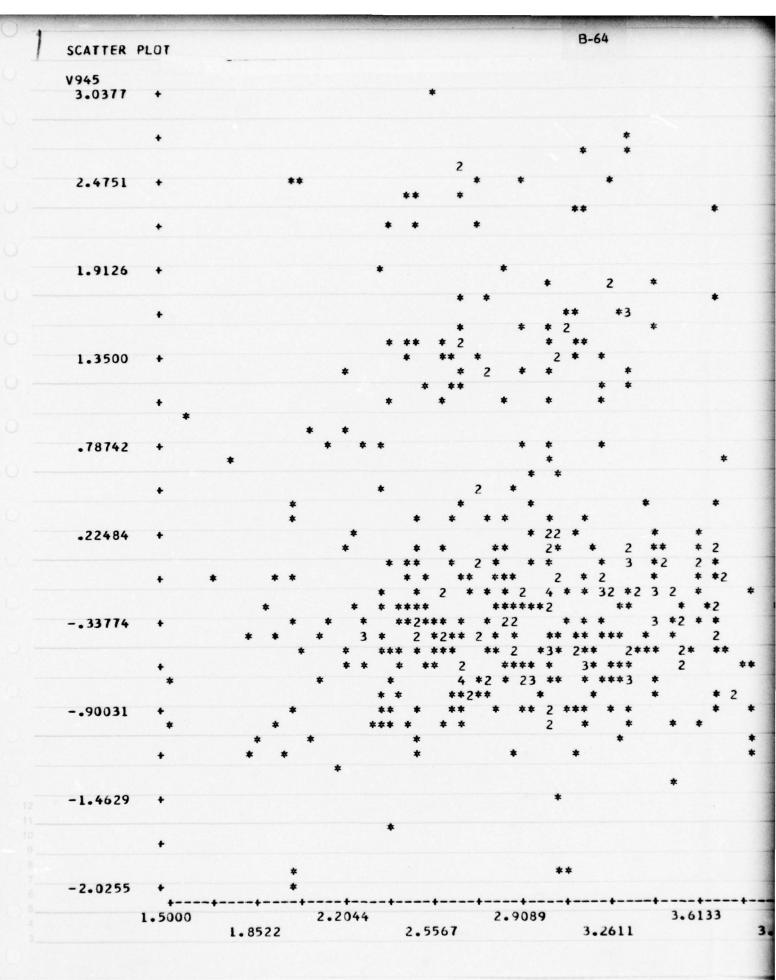
3.2222

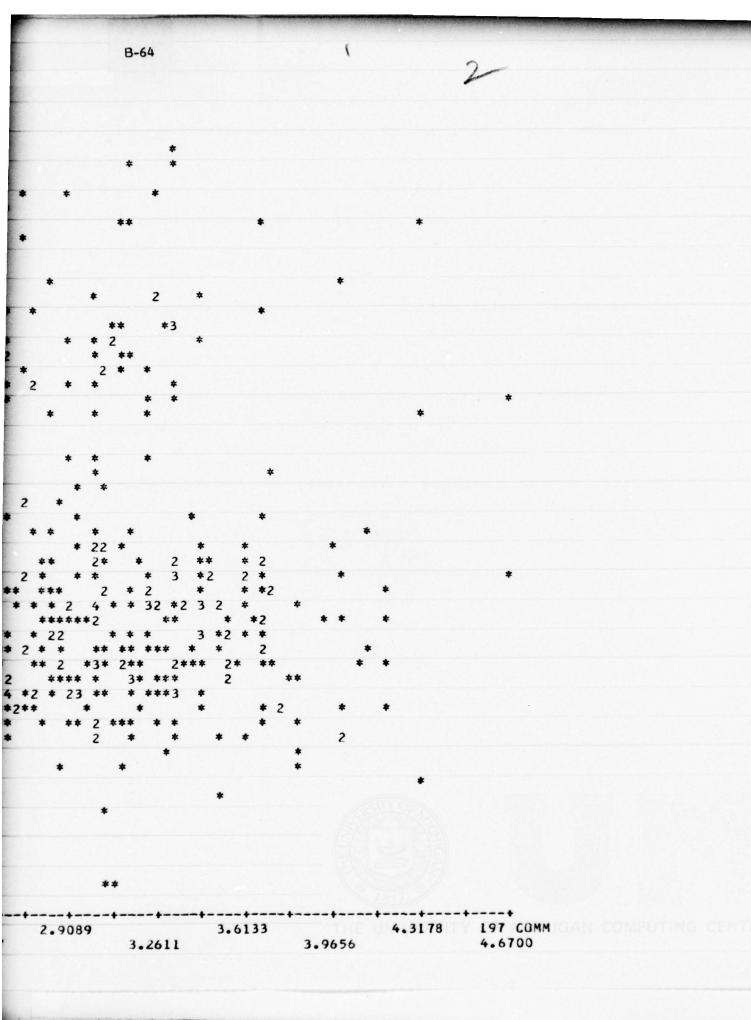
2.7778 3.6667 4.5556 188 PEER 5.0000

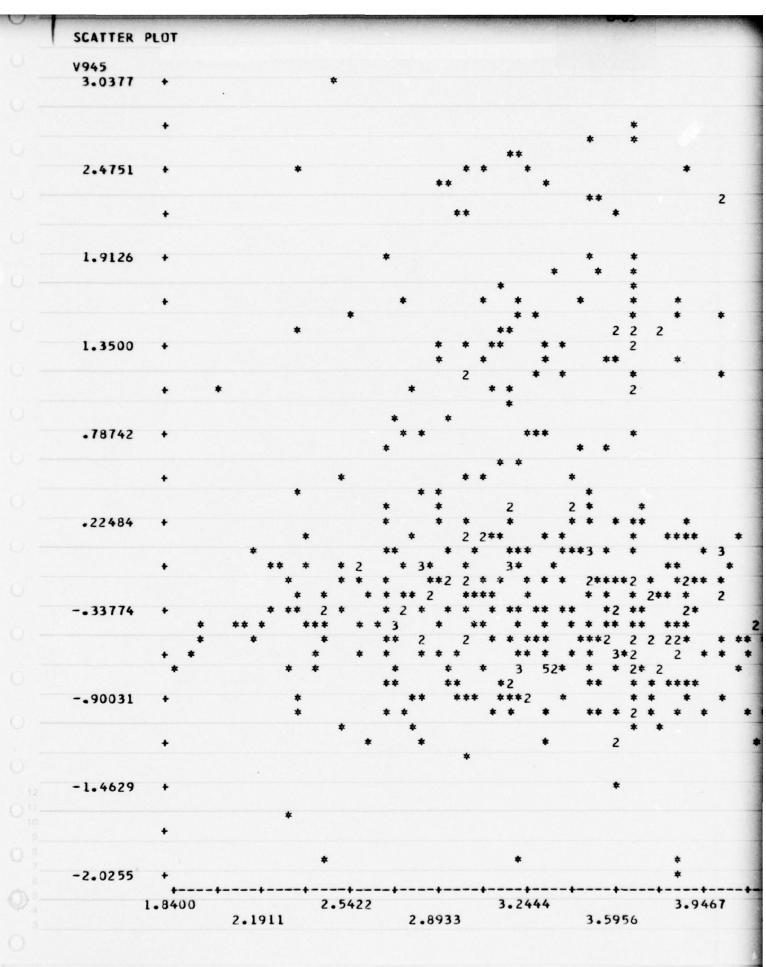
*
2.7778 3.6667 4.5556 190 PEER
3.2222 4.1111 5.0000

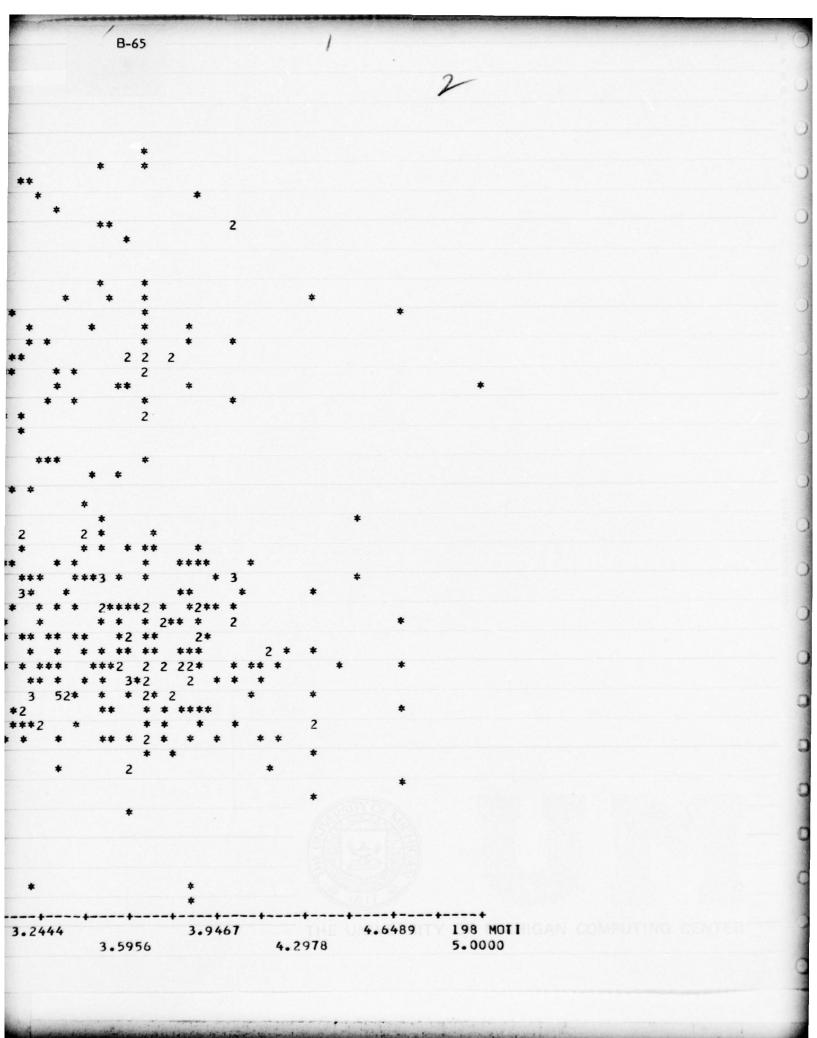


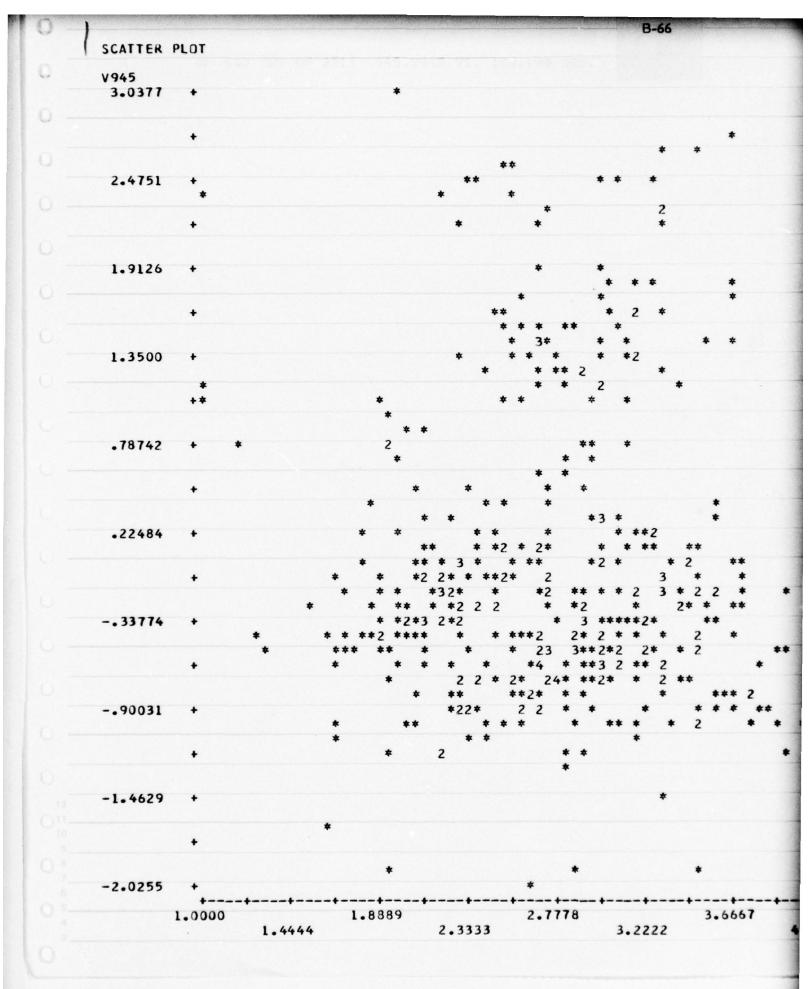
2.7778 3.6667 4.5556 196 HUM. 3.2222 4.1111 5.0000







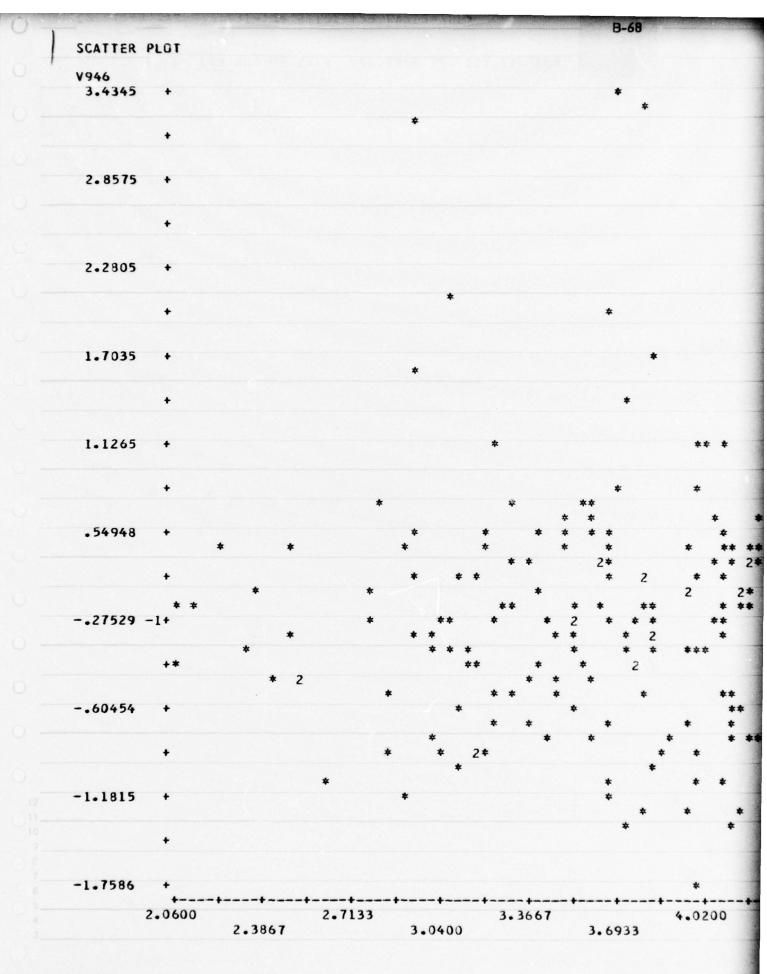


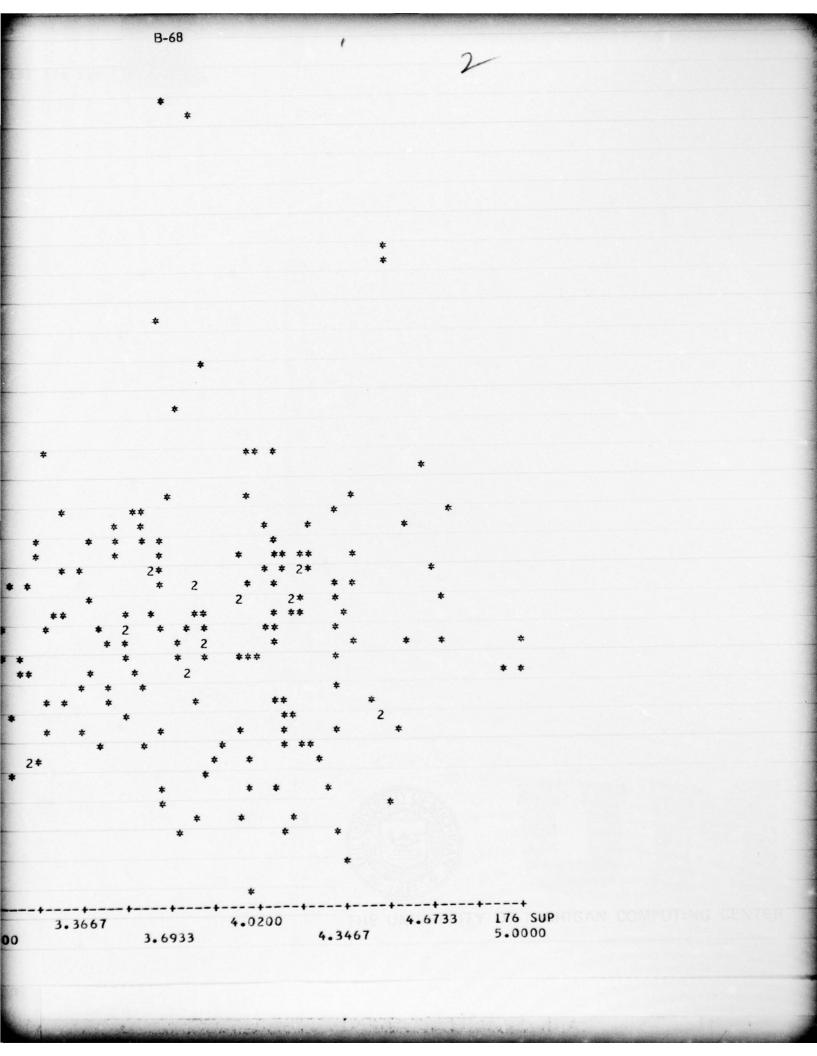


3.0944 3.8567 4.6189

3.4756 4.2378

200 SATI 5.0000





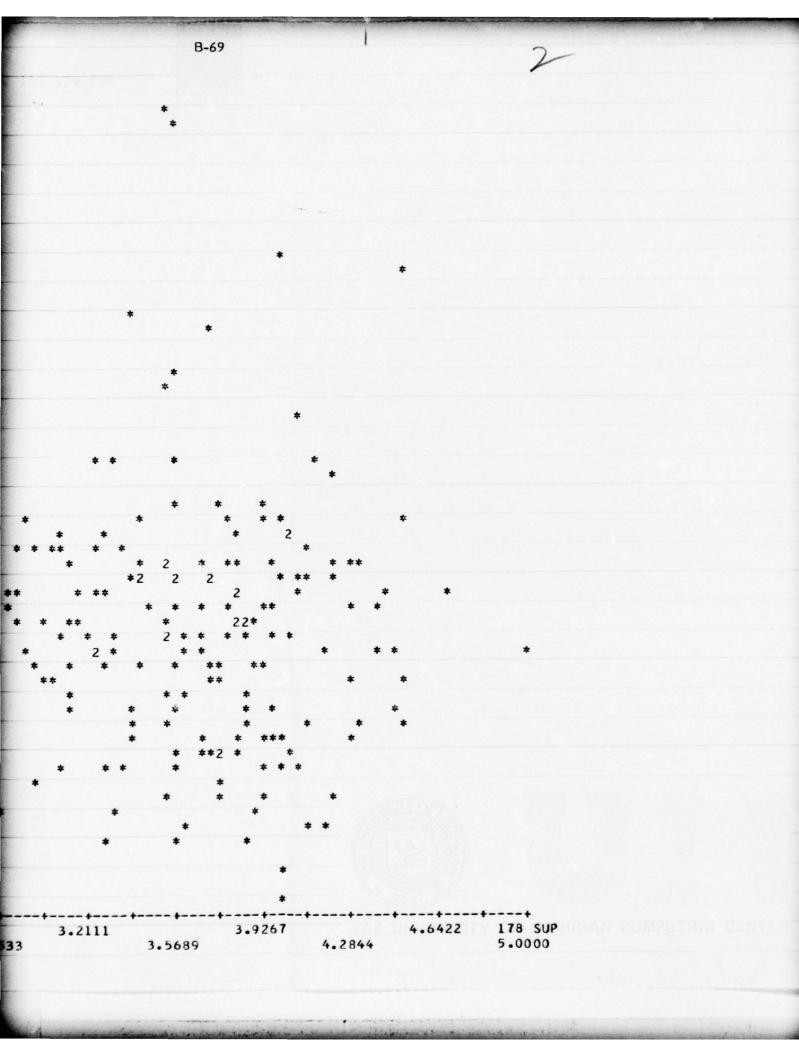
3.2111

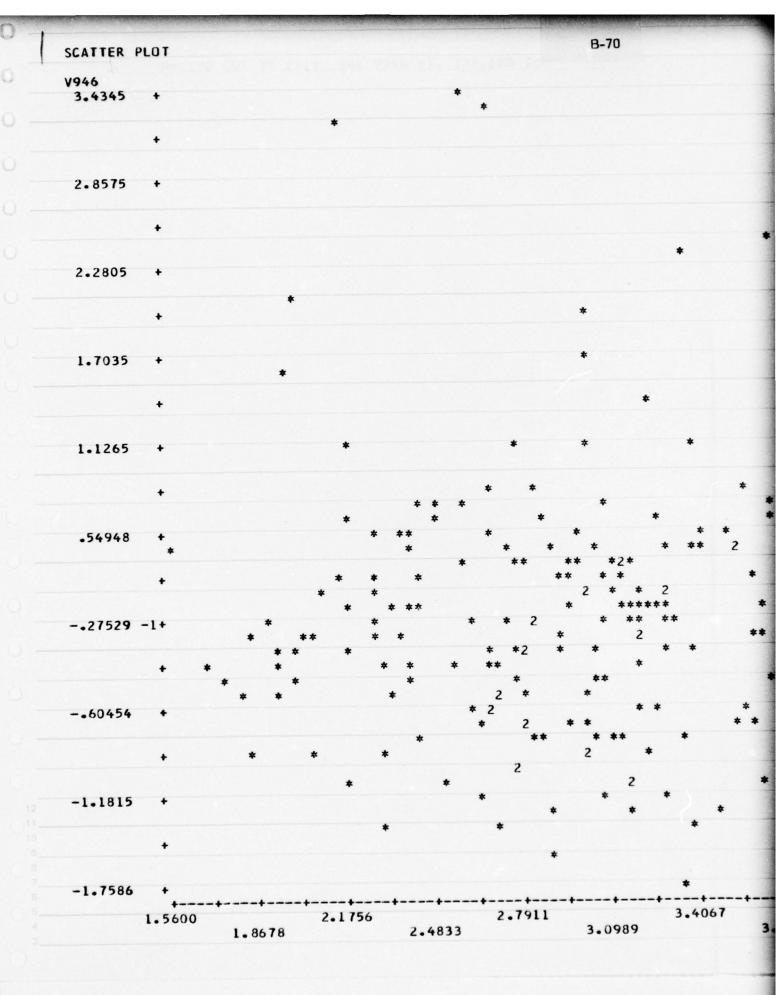
2.4956

1.7800

2.1378

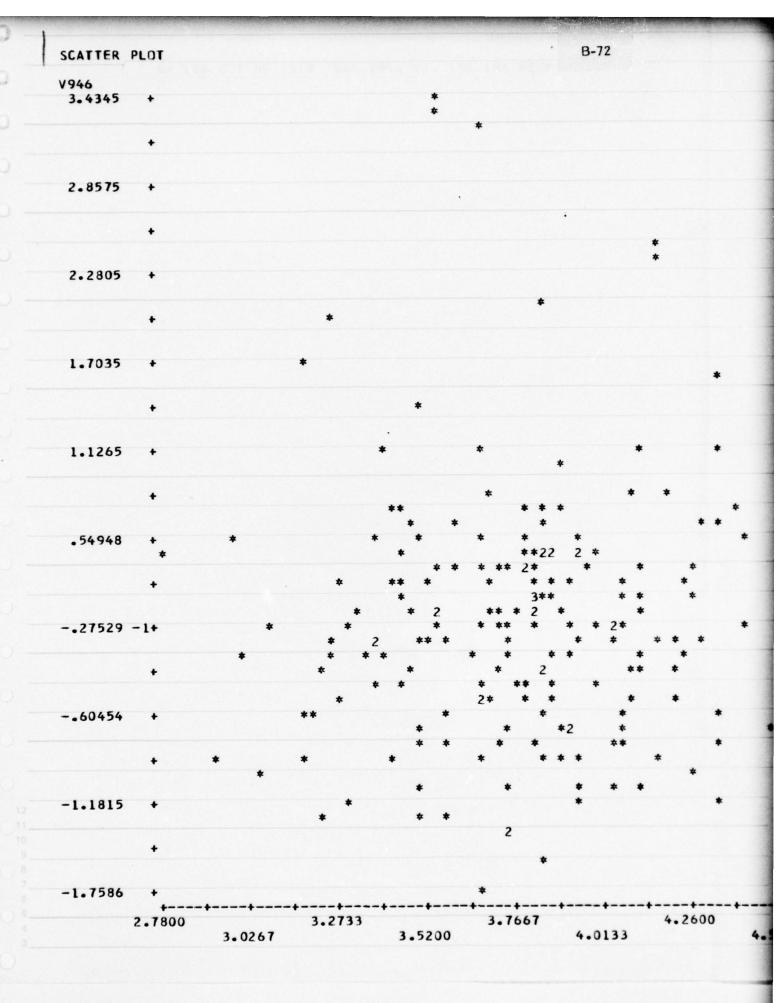
3.9267





V946 3.4345	SCATTER	PLOT					B-71	
2.8575 2.2805 + 1.7035 +	V946							
2.8575	3.4345							
2.2805 * <td></td> <td>٠</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		٠						
2.2805 +	2.8575	₹						
2.2805 + 1.7035 + 1.1265		•			*			
. 1.7035 +	2.2805	•					*	
1.1265 +		٠		•			*	
1.1265 +	1.7035	٠		*		*		
* * * * * * * * * * * * * * * * * * *		٠					*	
2 * * * * * * * * * * * * * * * * * * *	1.1265	٠			•		* *	•
* * * * * * * * * * * * * * * * * * *						*		
* 2 * * * 2 * * * * * * * * * * * * * *						2		* **
+	.54948	•				2 *	*	
27529 -1+ * * * * * * * * * * * * * * * * * * *		٠		*		*3 *		*
60454 + * * * * * * * * * * * * * * * * * *	27529	-1+	*	**	*	*2* *		***
60454 +				* :	* * *	3*		* *
60454 +					2 *			:
+	60454	+		*	•	*	*	* *
-1.1815 + * * *		٠		* *	* **		* *	***
* * *	-1.1815						**	
•					*	*	•	* *
		•						
-1.7586 + *	-1.7586	+	-++	+	+	+	*	+
1.0000 1.8889 2.7778 3.6667 1.4444 2.3333 3.2222		1.0000	1.4444	1.8889	2.3333	2.7778	3.2222	3.6667

2.7778 3.6667 4.5556 182 SUP 3.2222 4.1111 5.0000



3.7667 4.2600 4.7533 184 PEER 5.0000

3.8900 3.1500 4.6300 4.2600

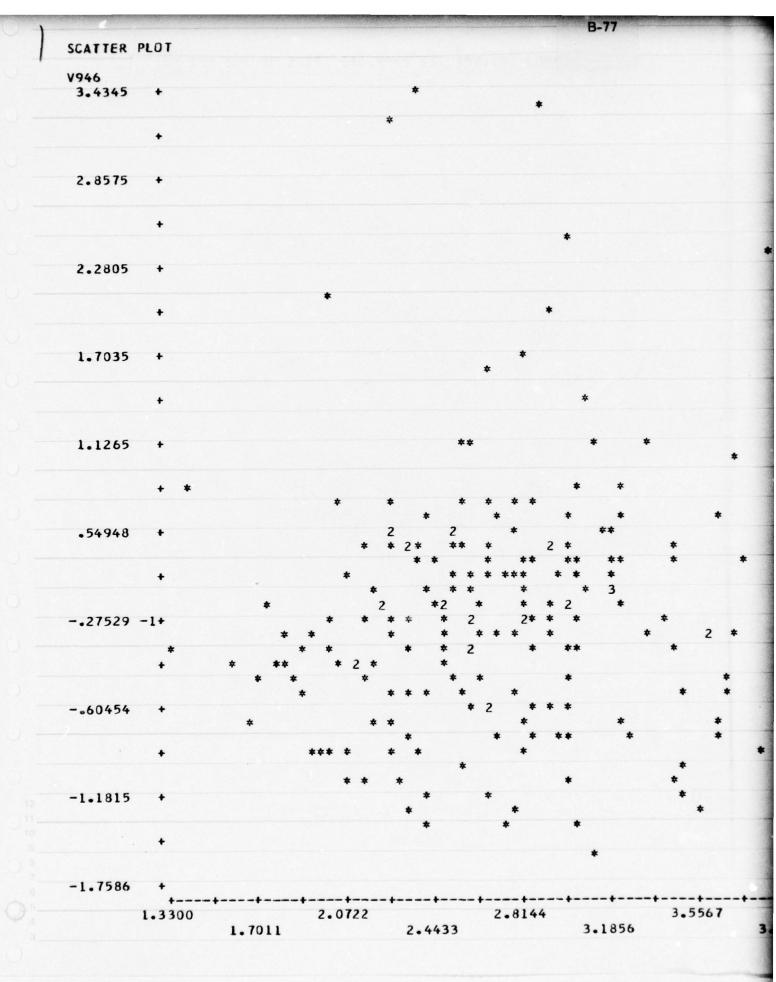
3.5200

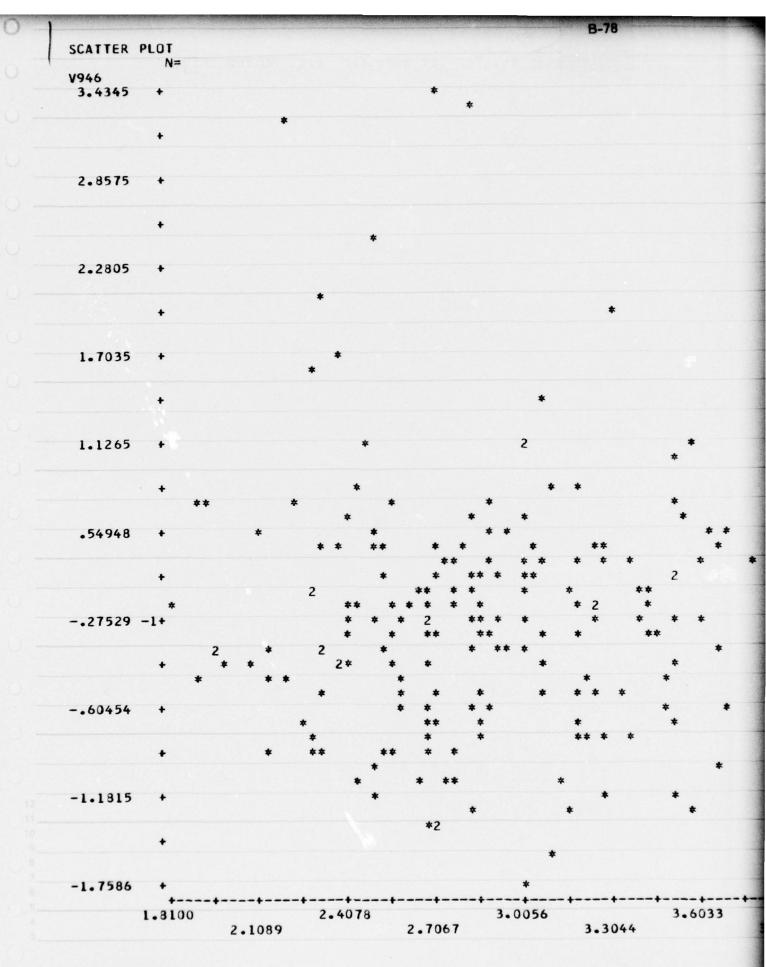
2

188 PEER 5.0000

1.3800 2.1844 2.9889 3.7933 1.7822 2.5867 3.3911

2.9889 3.7933 4.5978 196 HUM. 5867 3.3911 4.1956 5.0000





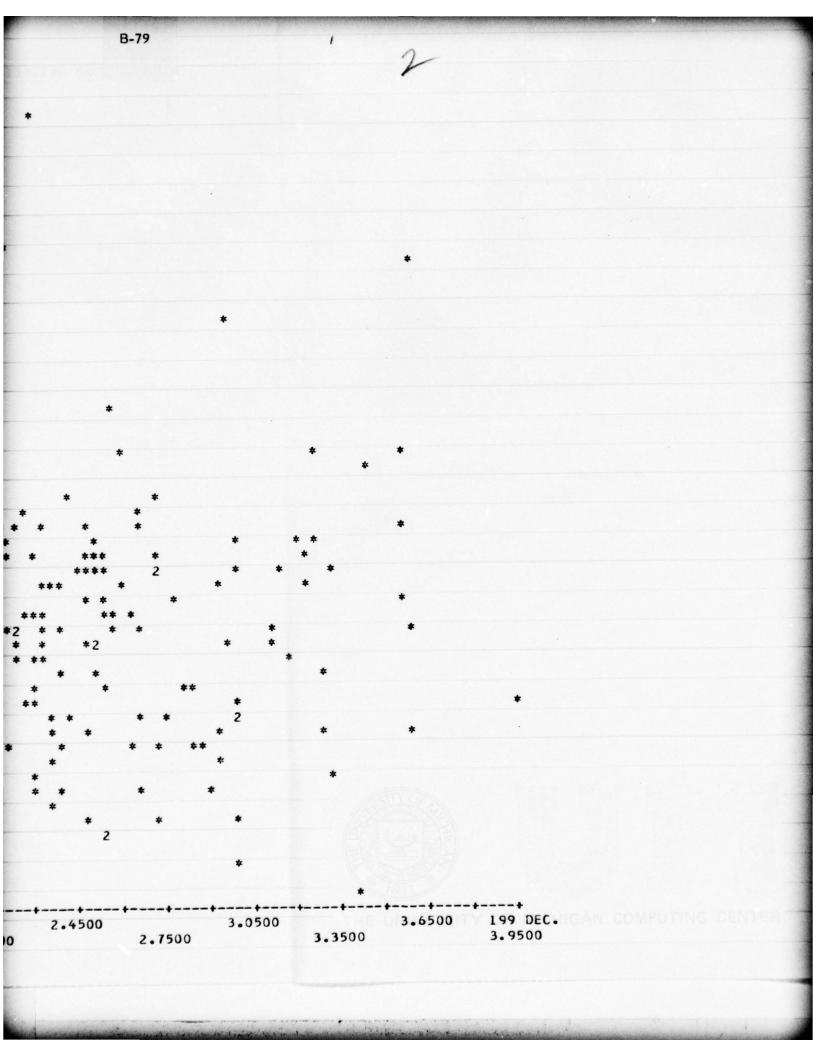
3.0056 3.6033 4.2011 198 MOT I .7067 3.3044 3.9022 4.5000

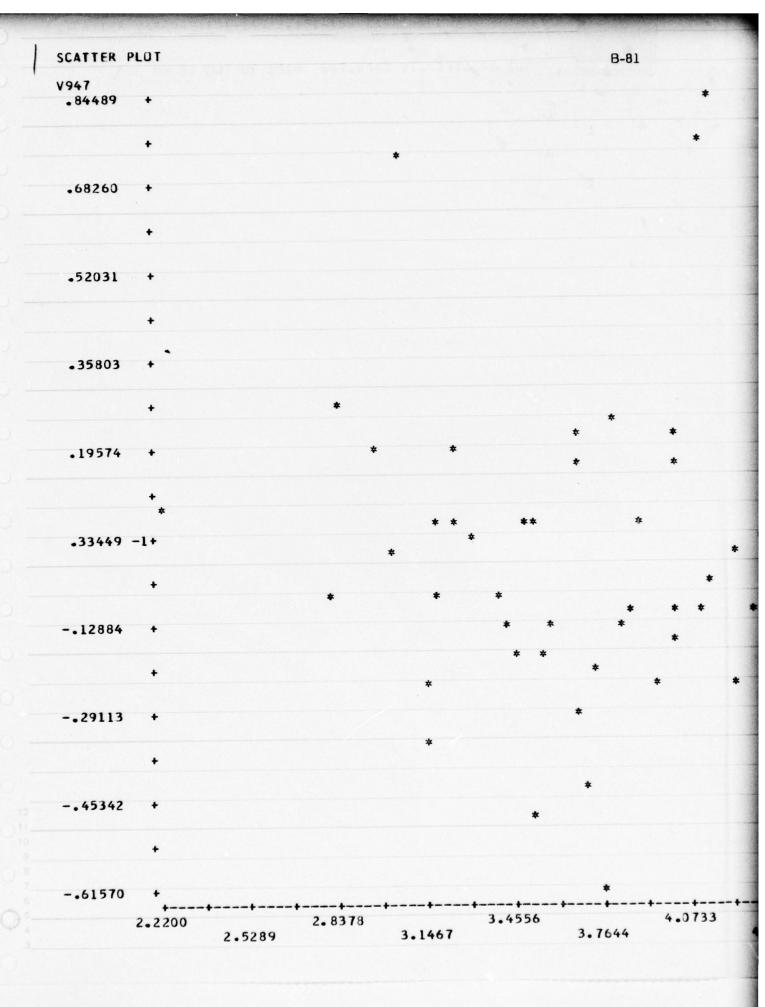
1.8500

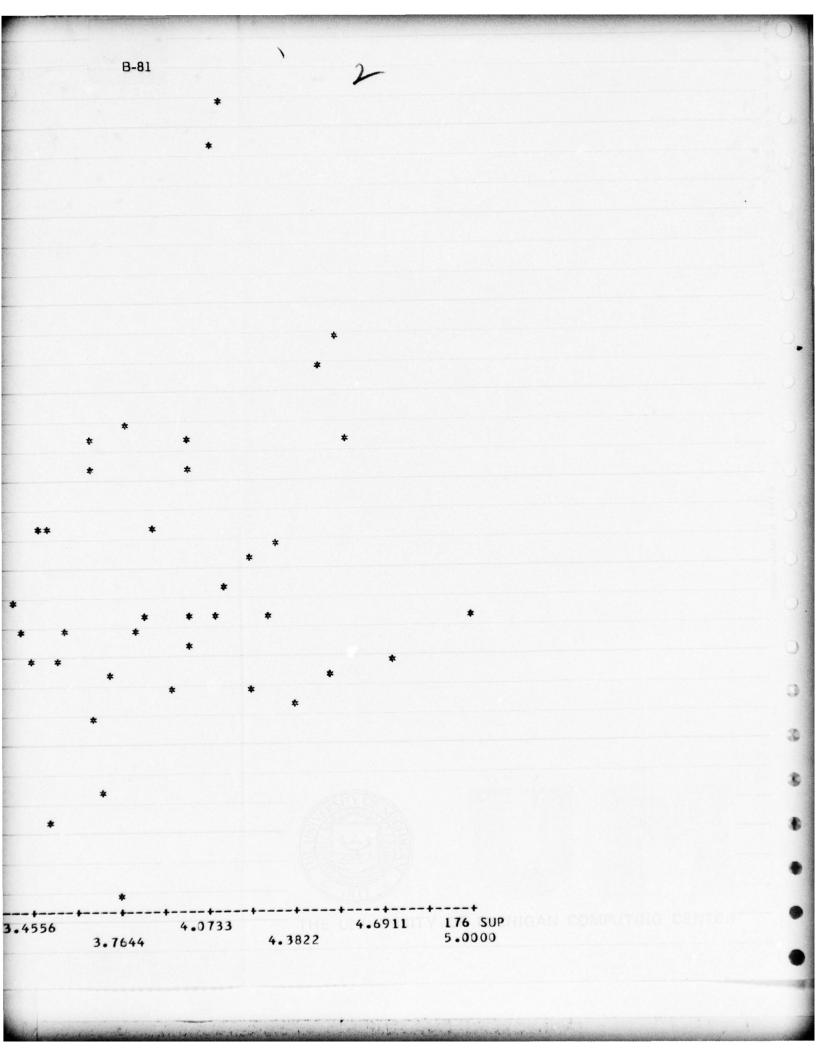
1.2500

1.5500

3.0500



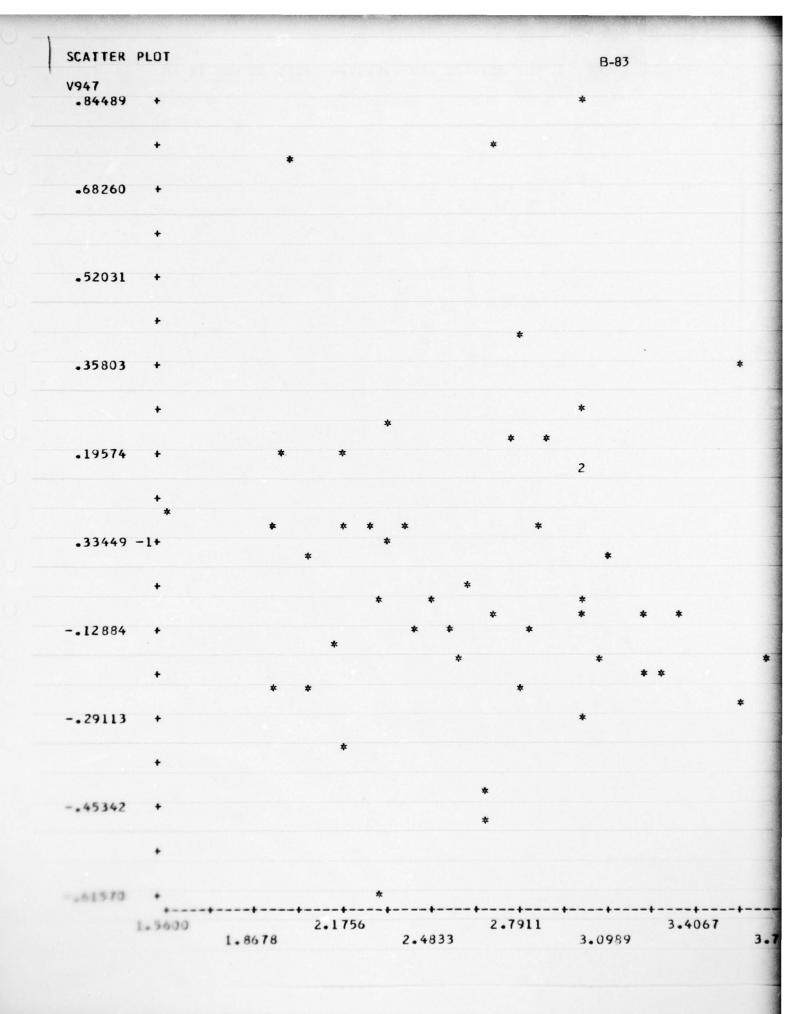




SCATTER	PLOT					B-82	
V947						*	
.84489	•					*	
					*		
					*		
.68260	+						
.52031	+						
	+						*
.35803	+						
	+				*		
10574					*	*	
•19574						* *	
	•						
	*		*		***	*	
.33449	-1+			*			*
					*		
					* *	*	**
12884	•				* * *	*	
				* *			. * .
	•			*	*		* *
29113	+					*	
				*			
	•						
45342						*	
. +9342							*
61570	+	++	*	+	++-	+	
	1.7800	2.1378	2.4956	2.8533	3.2111	3.5689	3.9267

3.9267 3.2111 3.5689

178 SUP 5.0000



2

4.0222 180 SUP 4.3300 3.4067 2.7911

3.0989

SCATTER PLOT B-84 V947 .84489 + .68260 + .52031 + .35803 + 2 .19574 + .33449 -1+ -.12884 + -.29113 +* -.45342 + -.61570 + 2.4722 3.1944 2.1111 2.8333 3.5556 3.9167 1.7500

B-84 2

3.1944 3.9167 4.6389 182 SUP 2.8333 3.5556 4.2778 5.0000

2.7800 3.2733 3.7667 3.0267 3.5200

4.2600

V947

-.61570

2 *

3.7667 4.0133 4.2600

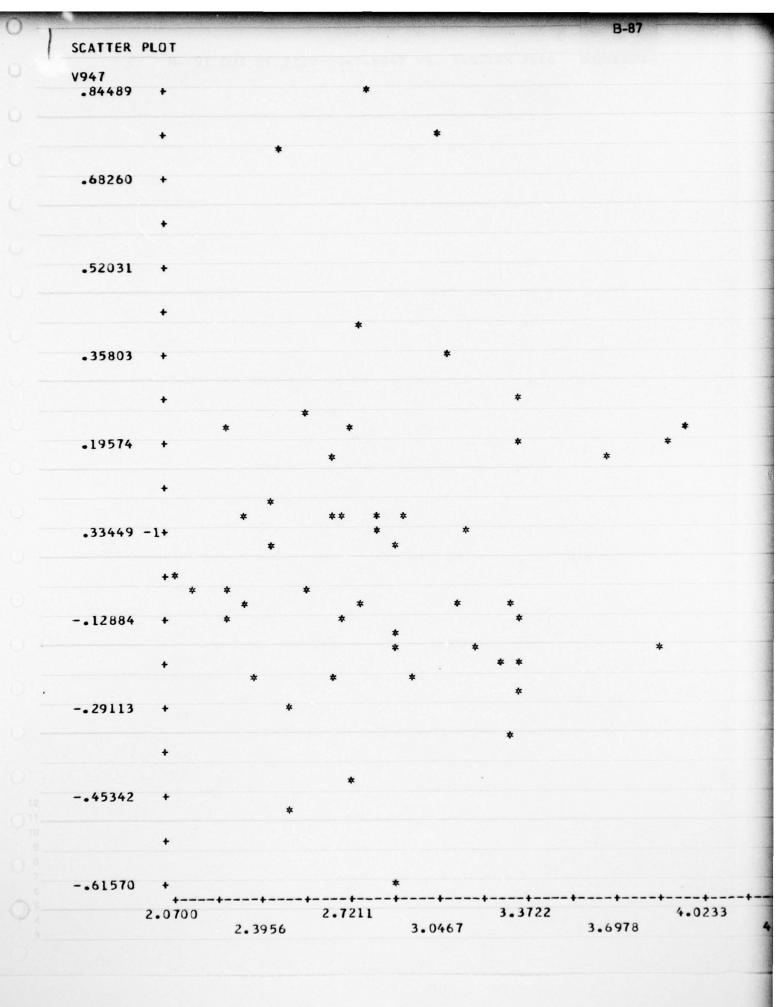
4.5067

4.7533

184 PEER 5.0000

1						B-86	
SCATTER	PLOT						
V947 .84489		•		*			
.04407							
	+			*			
			*				
.68260	+						
	٠						
.52031	+						
	+						
				*			
.35803	+						*
	+						*
			*			*	
.19574	+			*	*	*	
	+			*			
.33449	-14	*	* *	* *			
•33447		*		*			
	+	*					
		*	* *	*	* *	*	
12884	+		*	*			
		*		*			
	+		*		*	*	
					*		
29113	+*						
	+			*			
45342	+			*			
					*		
	+						
61570	+			++		++	
	2.250	0	2.8611		3.4722		4.0833
		2.5556		3.1667		3.7778	

3.4722 4.0833 4.3889 4.6944 186 PEFR 5.0000



3.3722 3.6978

4.0233

4.3489

4.6744 188 PEER 5.0000

3.4500

2.8300

4.0700

3.7600

-.61570

2.2100

2.5200

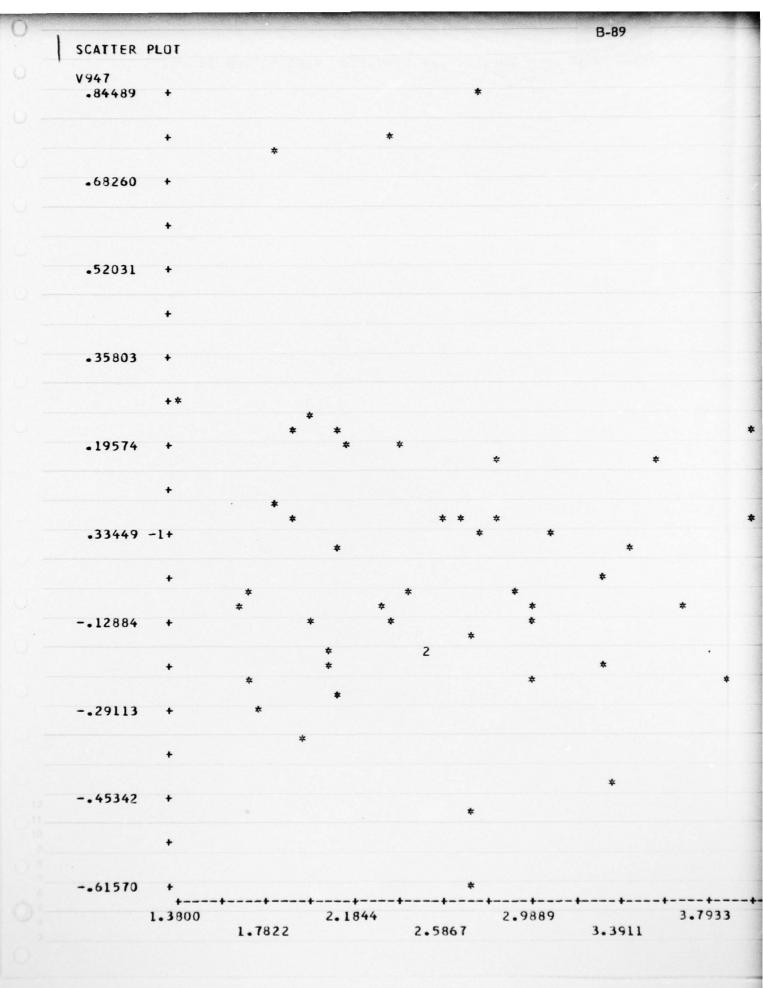
*

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3.4500 4.0700 4.6900 190 PEER 3.7600 4.3800 5.0000



2.9889 2.5867

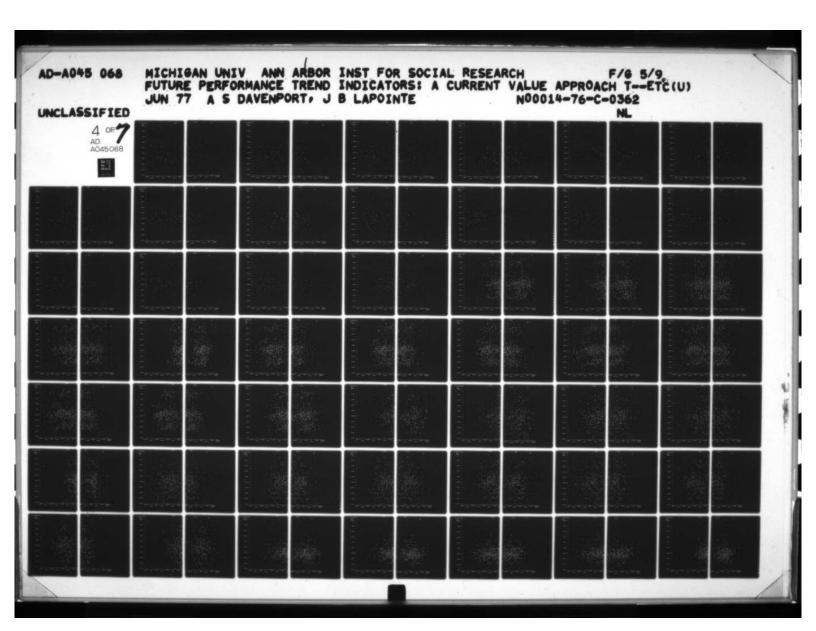
3.3911

3.7933

*

4.1956

4.5978 196 HUM. 956 5.0000





SCATTER	PLOT					B-90	
V947							
.84489	•				*		
							1
	. +	*		*			
.68260	+						
	+						
.52031	+						
	+						
							*
25022							
.35803	+				*		
	+	*					
		*					
10574		*		* *			*
-19574	+			* *	*	*	
	+						
				*			
.33449			* 2	*	*		*
•33447		*			*		
	+				*		
		*	*	*			*
12884	+		*	*	*		
				*			
		*		*			
	+	*			*	*	*
					•	*	
29113	+*						
	+	*					
					*		
45342	+						
				*			
	+						
7							
61570	٠.						
	1.6700	· · · · · · · · · · · · · · · · · · ·	2.3367	+	3.0033		3.6700
		2.0033	2.0001	2.6700	3.0033	3.3367	3.3100

B-90 *

•

* *

* * * *

* * * *

3.0033 3.6700 4.3367 197 CDMM 4.6700

*

* * *

* *

•

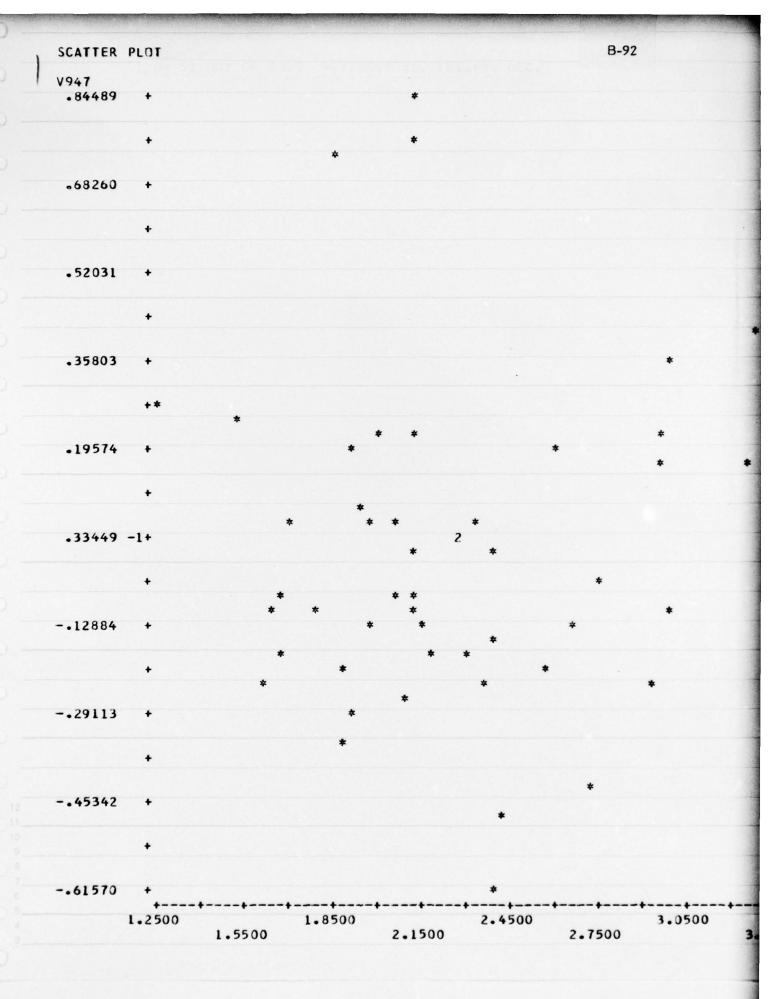
*

3.0556 .7667 3.3444

3.6333

3.9222

4.2111 198 MOTI 4.5000



2.4500 3.0500 3.6500 199 DEC. 1500 2.7500 3.3500 3.9500

SCATTER	DIOT					B-9	77
SCALLER	N=					D-1	"
V947	N-						
.84489	•						•
	+						*
					*		
.68260	+						
	+						
.52031	+						
	+						
							*
.35803	+						*
	+		*				
					*		
					*	*	
.19574	+				*		*
******						*	*
	+						
			*				
					*2		* *
.33449	-14				+2	*	*
. 33449	-14			*		•	*
				•			•
							*
	*.						•
					*	#	
					* *		
12884	•					*	*
				*	*		*
	+						*
				*		*	*
							*
29113	+			*			
					*		
	+						
							*
45342	+						
					*		
	+						
61570	•						
	+	++		+	-+	-++	-++
	1.8400		2.4978		3.1556		3.8133
		2.1689		2.8267		3.4844	

B-93 *2

3.1556 3.8133 4.4711 200 SATI 3.4844 4.1422 4.8000 2

* * *

*

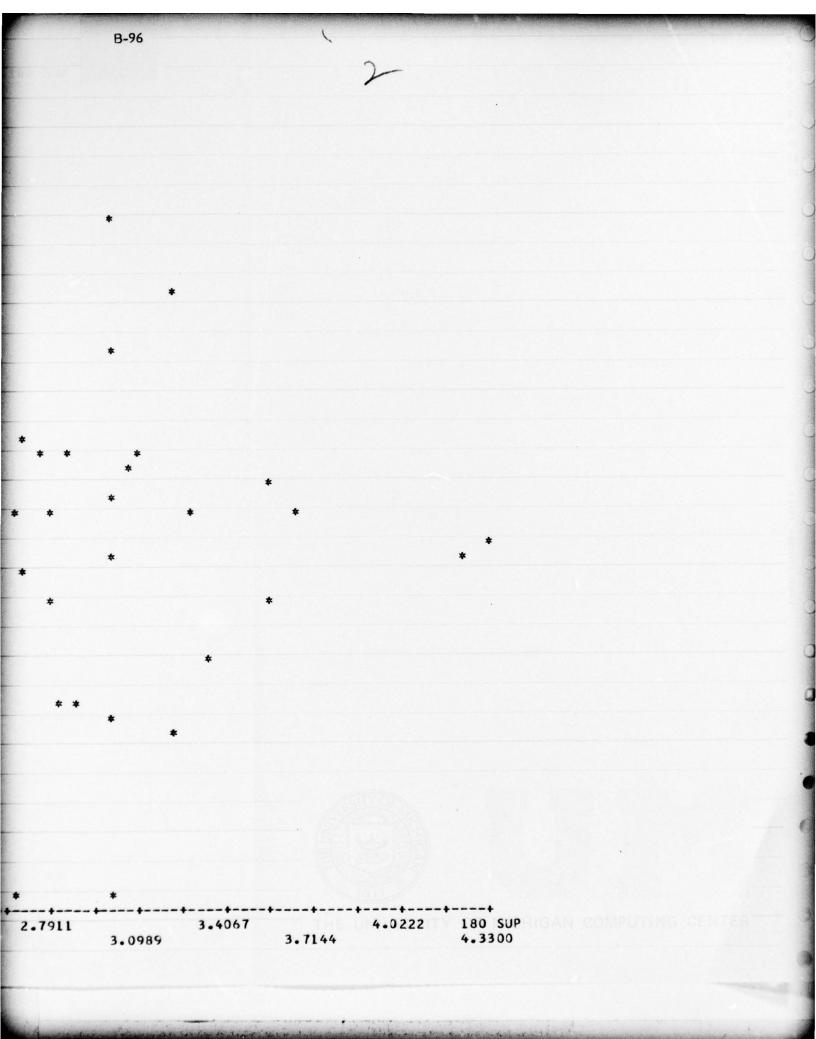
3.4556

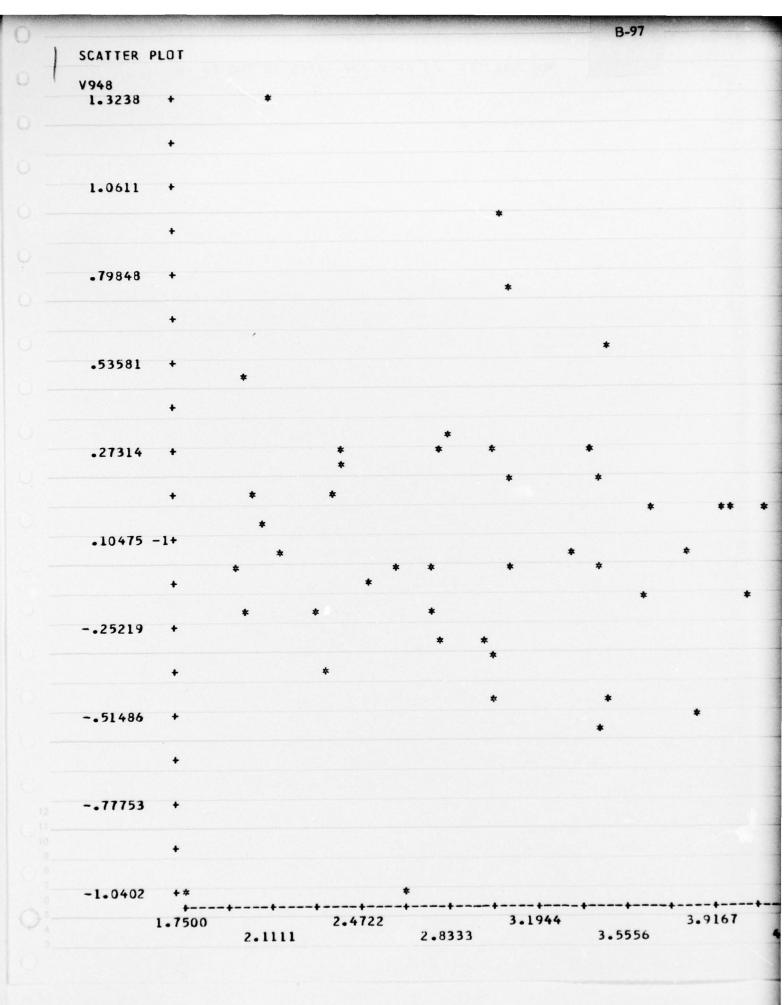
4.3822

4.0733

4.6911 176 SUP 5.0000

3.2111 3.9267 4.6422 178 SUP 3.5689 4.2844 5.0000





182 SUP 5.0000 .1944 4.6389 4.2778 3.5556

3.7667

4.2600

4.7533 184 PEER 5.0000

4.0133

4.5067

SCATTER	R PLOT			•		В	-99
V948							
1.3238	3 +		*				
	+						
1.0611							
	+			*			
70949							
.79848	3 +				*		
	+						
				*			
-53581	+						
			*				
	+						
-27314	. +	*	*	*	*		
		*					
		*			*		*
				** :	•		*
10/75					*		
-10475	-1+			*		* *	
	*	*		* *	*		
	+			*			
			*	* *	* *		
25219	+						
			*		*		*
	+		*				
51486			*	*		*	
				*			
77757							
77753	•						
	•						
-1.0402	+*						
	2.2500	-+	2.8611	++		++	++
	2.2.700	2.5556	2.0011	3.1667	3.4722	3.7778	4.0833
						341110	

0 0 0

4722

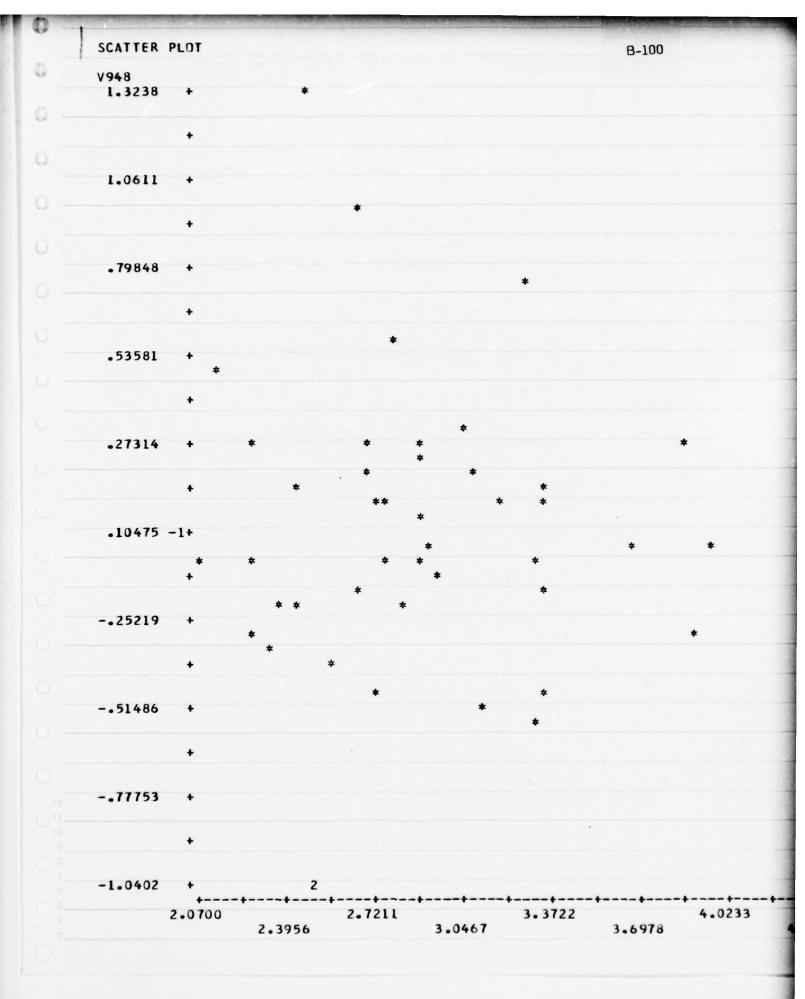
3.7778

4.0833

4.3889

4.6944

186 PEER 5.0000

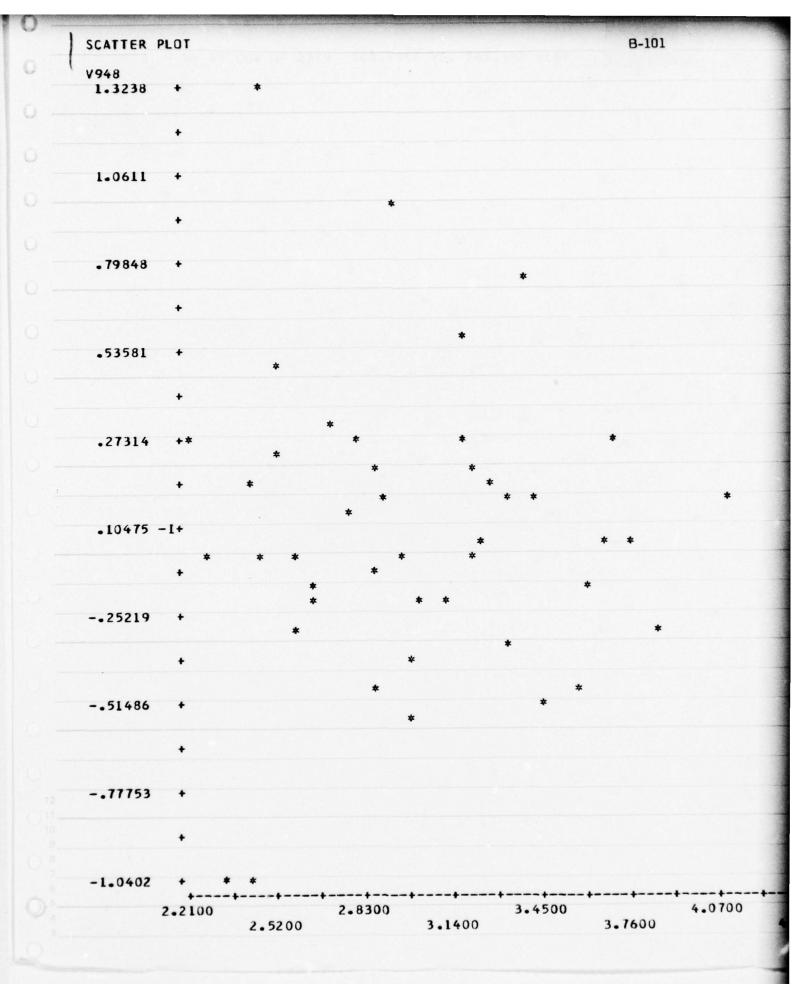


4.0233 . 3722

3.6978

4.3489

4.6744 188 PEER 5.0000



3.4500

3.7600

4.0700

4.3800 190 PEER 5.0000

SCATTER	PLOT					B-102		
V948 1.3238	•							
	٠							
1.0611	•							
	٠					*		
.79848	٠		*					
	•				*			
•53581	•			*				
	•		*					
•27314	+*	*	**	*		*		
.10475				*		**		*
*10415	-14				*			2
	+	* •	*	*	*	*		
25219	٠	* *	* *		*			
	+		*					
51486	٠	*			*		*	
	٠							
-•17153	•							
	٠							
-1.0402	٠.	. *.						
	1.3800	1.7822	2.1844	2.5867	2.9889	3.3911	3.7933	4.

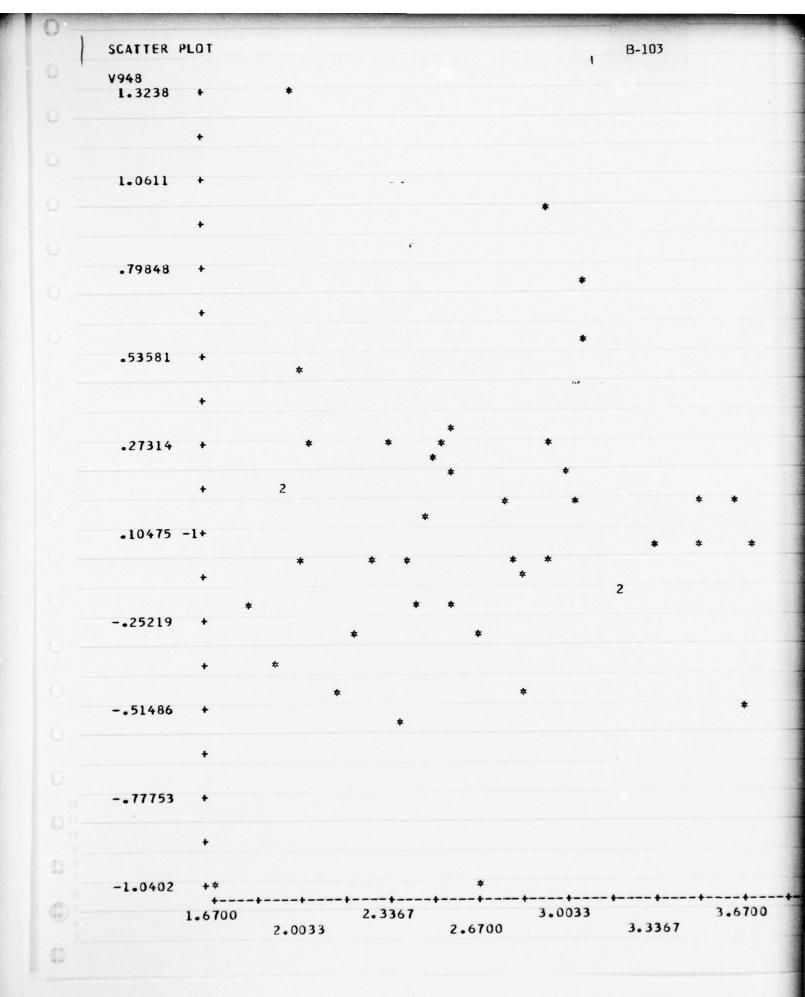
Q

3.7933 2.9889 3.3911

4.1956

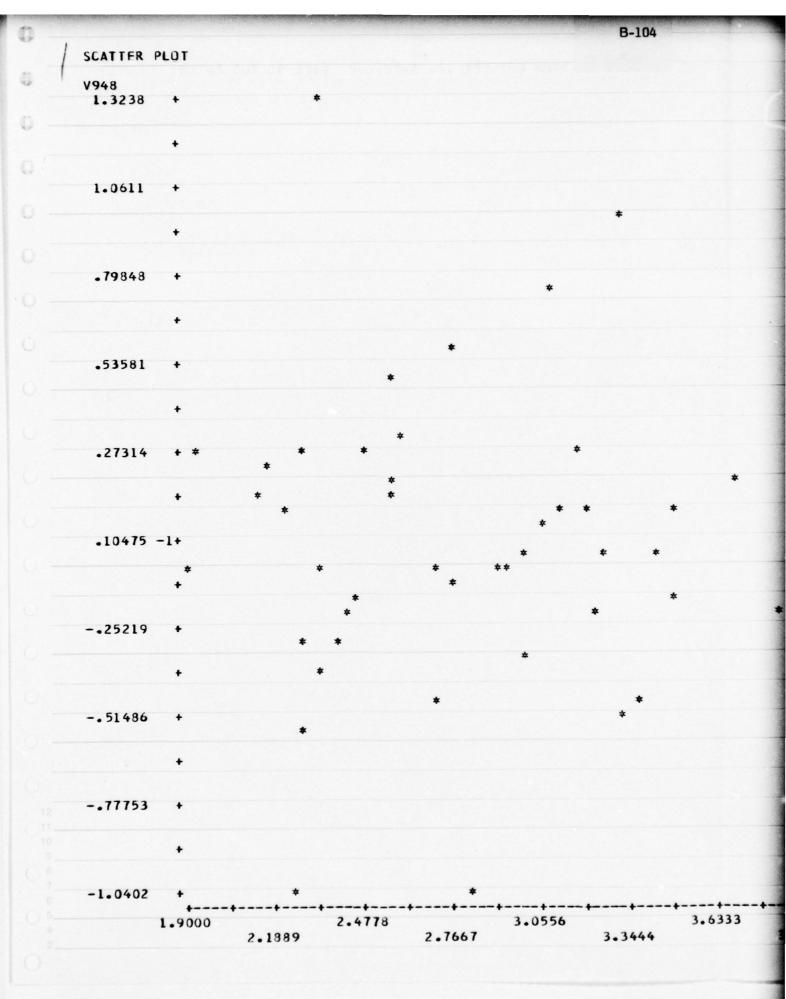
2

4.5978 196 HUM. 5.0000



2

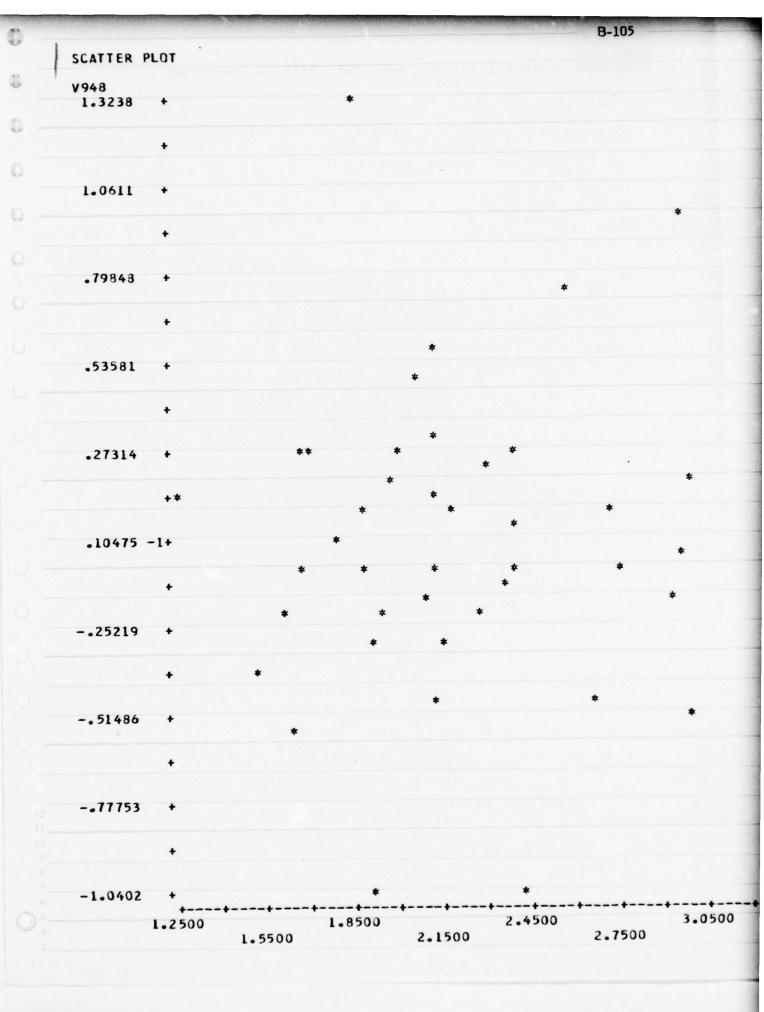
197 COMM 0 3.0033 3.6700 4.0033 3.3367



3.0556 3.3444 3.6333

3.9222

4.2111 198 MOTI 4.5000

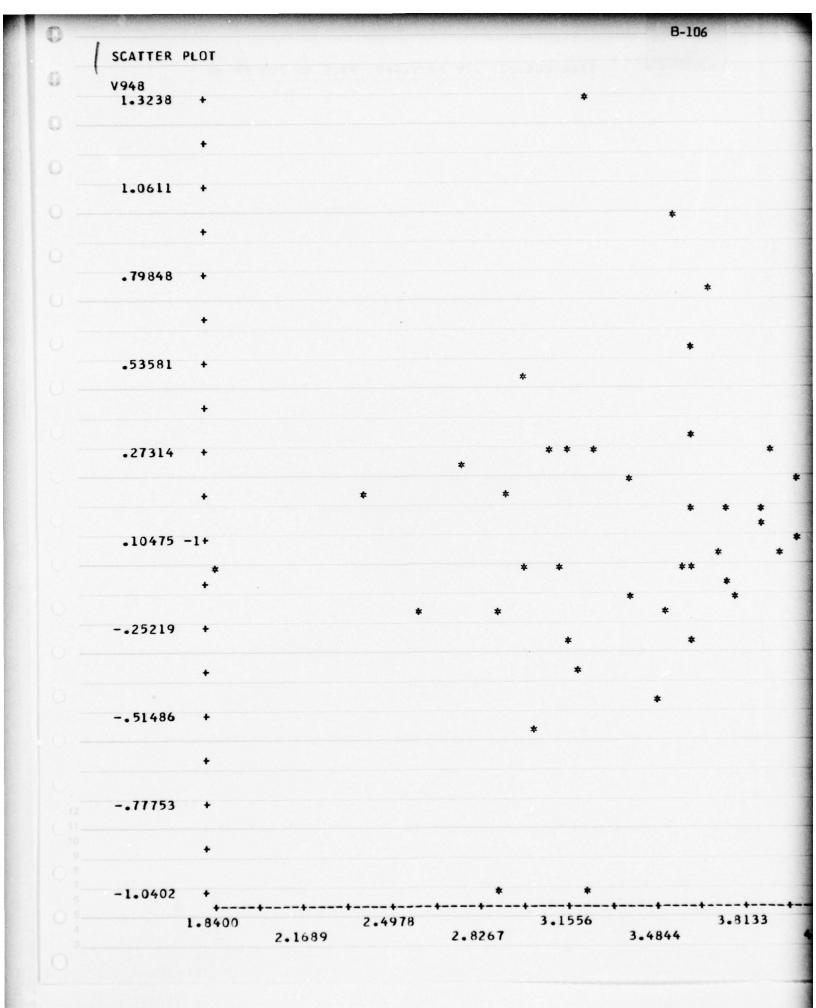


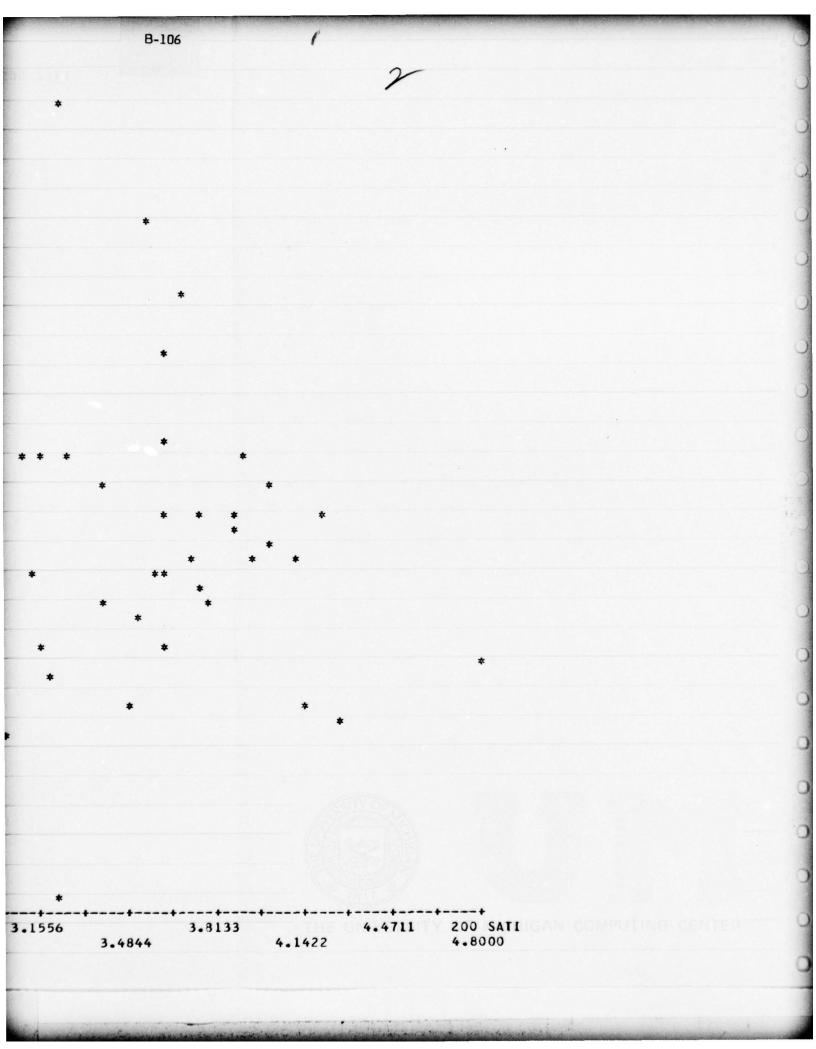
* *

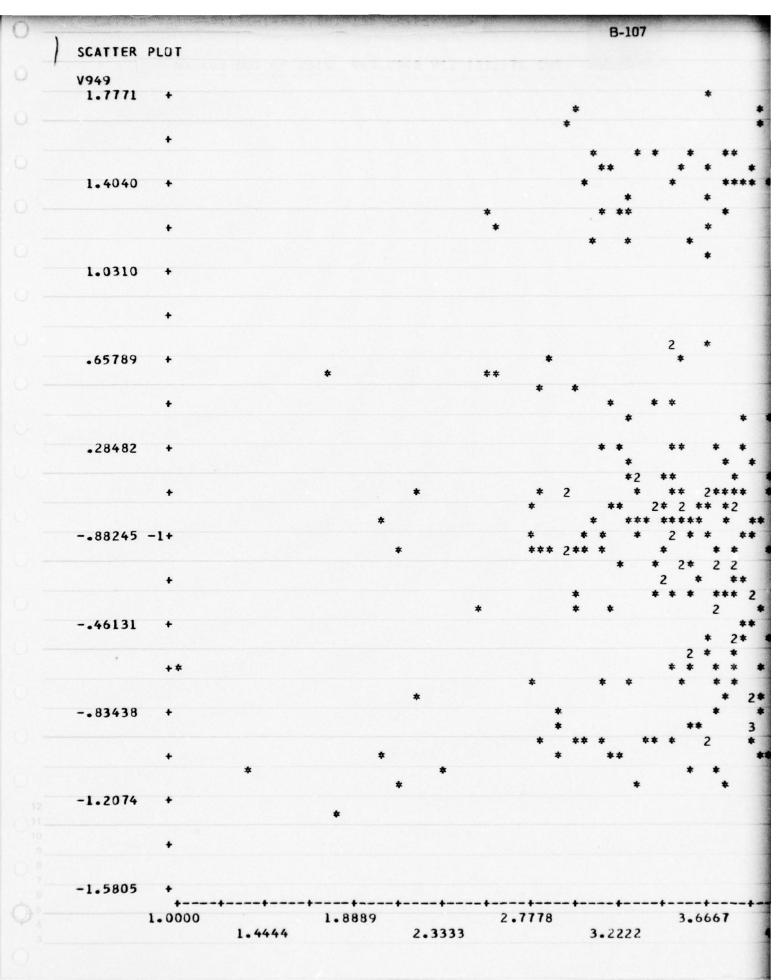
* * * * *

*

*
2.4500 3.0500 3.6500 199 DEC.
2.7500 3.3500 3.9500







B-107

2.7778 3.6667 4.5556 176 SUP 3.2222 4.1111 5.0000

-1.2074 .

1.1700 2.0211 2.8722 3.7233

1.5956 2.4467

2.8722 3.7233 4.5744 178 SUP 3.2978 4.1489 5.0000

3.6667

3.2222

1.4444

-1.5805

180 SUP 5.0000 4.5556 2.7778 3.6667 3.2222 4.1111

1 444

2.7778

3.6667

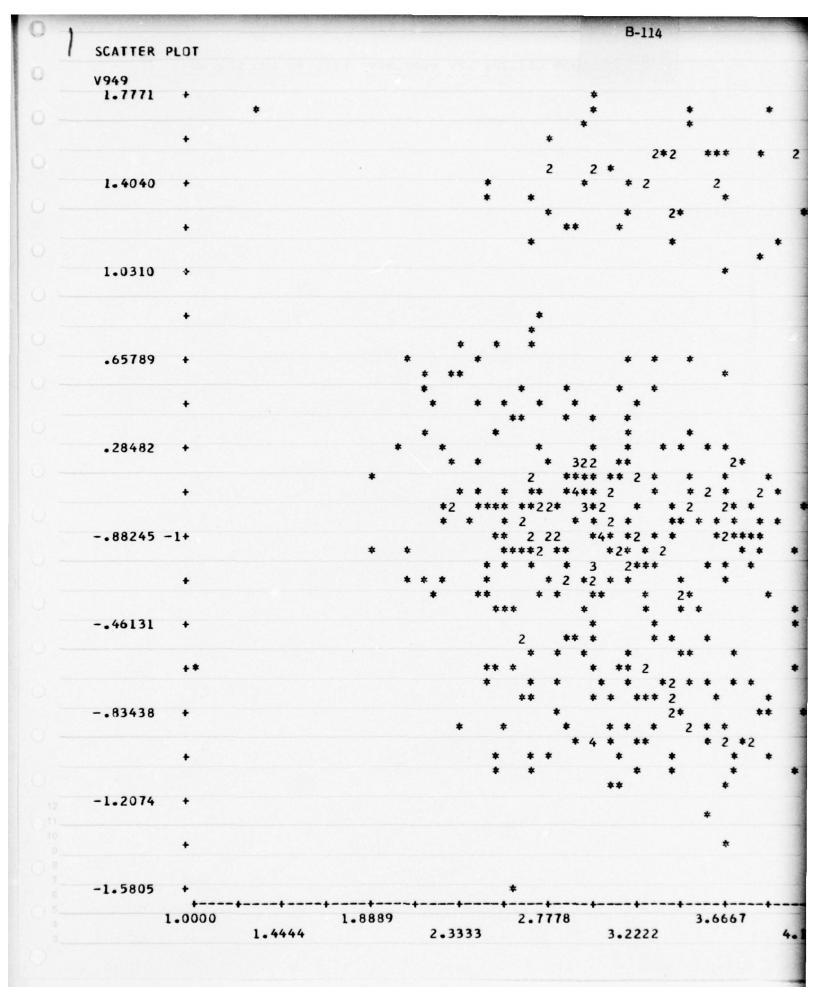
	1.0000	1.4444	1.8889	2.3333	2.1710	3.2222	
-1.5805	+	+	1 0000	+	2.7778	-+	3.6667
	•						
-1.2014							
-1.2074	•					**	* *
						* 2*	* 2*** *2
83438	٠				* *	* *	* **
	+	*	1		**	* **	*
46131						*	* 2*
						* *:	*2* 2 2
						* * * * ** 2	**** 222* * 2 * *22 * 2*2*
88245	-1+					** *	3 **3** **** *22 3
	•						* 2* ** 34 2 ** * *22 2*32
.28482	•					* *	2 ***
	+		,			*	*
•65789						* * *	* *
	•					*	
1.0310				4			
1.0310	•						
	•					* **	* 2
1.4040	•					* * *	** 2
	+					*	* *2 * *
1.7771	*					. *	*
SCATTER V949	PLOT					5-111	
						B-111	

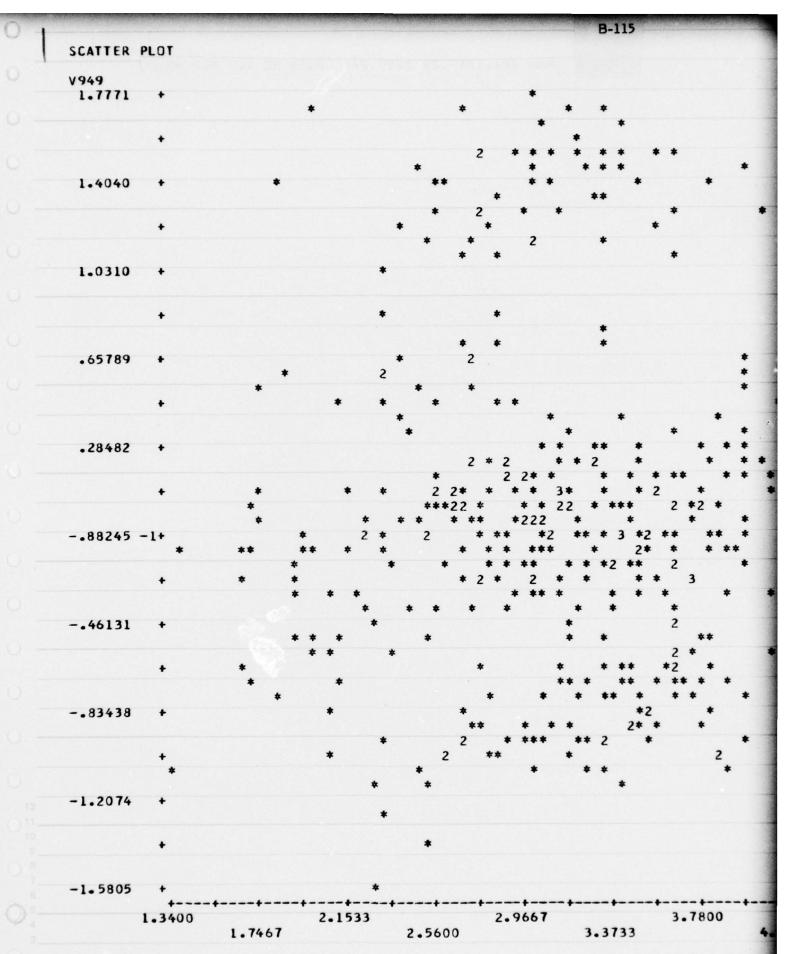
```
*22 3 * 23
222* * 33
```

4.5556 184 PEER 5.0000 2.7778 3.6667

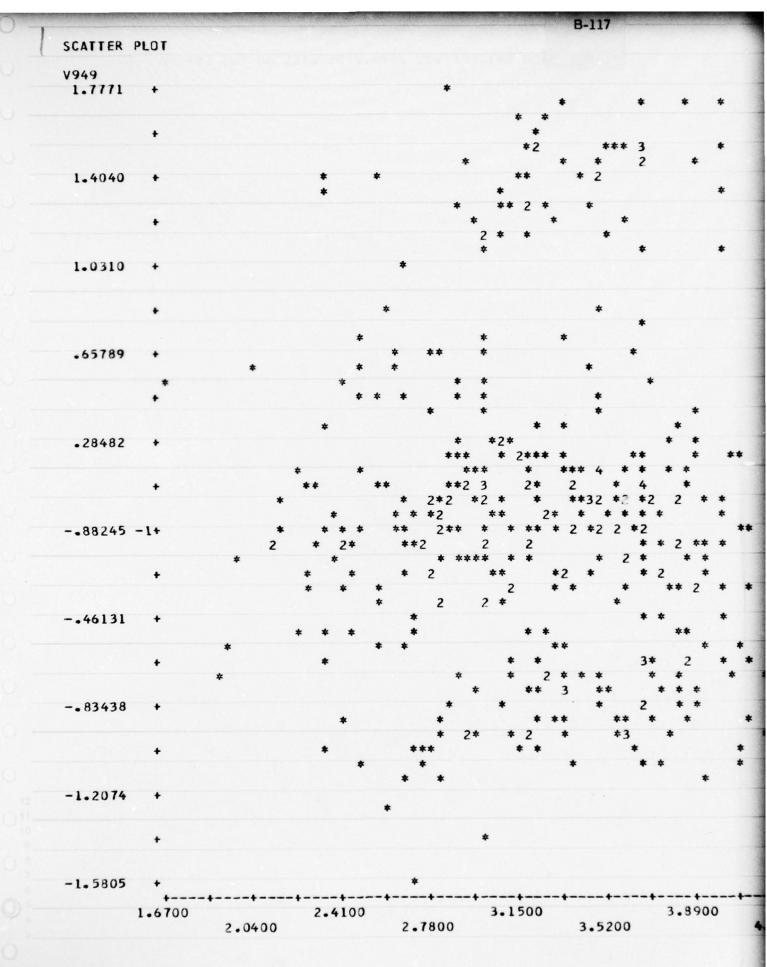
3.2222 4.1111

SCATTER	PLOT						В	-113			
V949											
1.7771	+								*		
	*								*	*	*
									*		*
	+						*			* *	***
						•	2		•	*	•••
1.4040	+				*		2		*	* *	* *
						**				*	
						**		*	**		*
	+					2		*		*	
										*	
1.0310	+						*				
	+						*			*	
						* *			*	•	
-65789	+		*	*	*	*		*			
					* *	*					*
					* *			**	*		
	•			2*	*	**	2		*	*	
						*	2	*			*
.28482	+			* *				*		2 *3	
,				*		* * *	4	** *	*	**	*
					*	*		2*2*	*	* 3	*
	+				***	*	32*	***2	**	* *	**
				*	* * *	24 **	** 32*	* 2	*	* *	*2 *
88245	-1+			*	*	* 2*	*2*3*	* **	* **	***2	*
			*	***	*2	***	**	2 3		2	
				. *	. *	**		* 3	*		* .
	•			*	*	2 **	* **	*	3 2		
				*	*		+ 2.	** **			
46131	+							*		*	*
					*	* *		*	2		*
						**	*	*	*		* *
	+*			*	*		٠.	*	* .	**	٠
				•	*	*	*	* *	3	* 2	
83438	+					*		*		2	
						*	* **		22	* *	
							**	*3	* *	* *	3
	•				*	2 *		•	2	* *	
					_		*	*	2	*	
-1.2074	+										
											*
										*	
	+									*	
-1.5805	+					*					
	+	+	++	-++	+	+-	+-	+-	+	+	
	1.0000		1.8889	2 22		2.777	78	2 222		3.66	67
		1.4444		2.33	33			3.222			



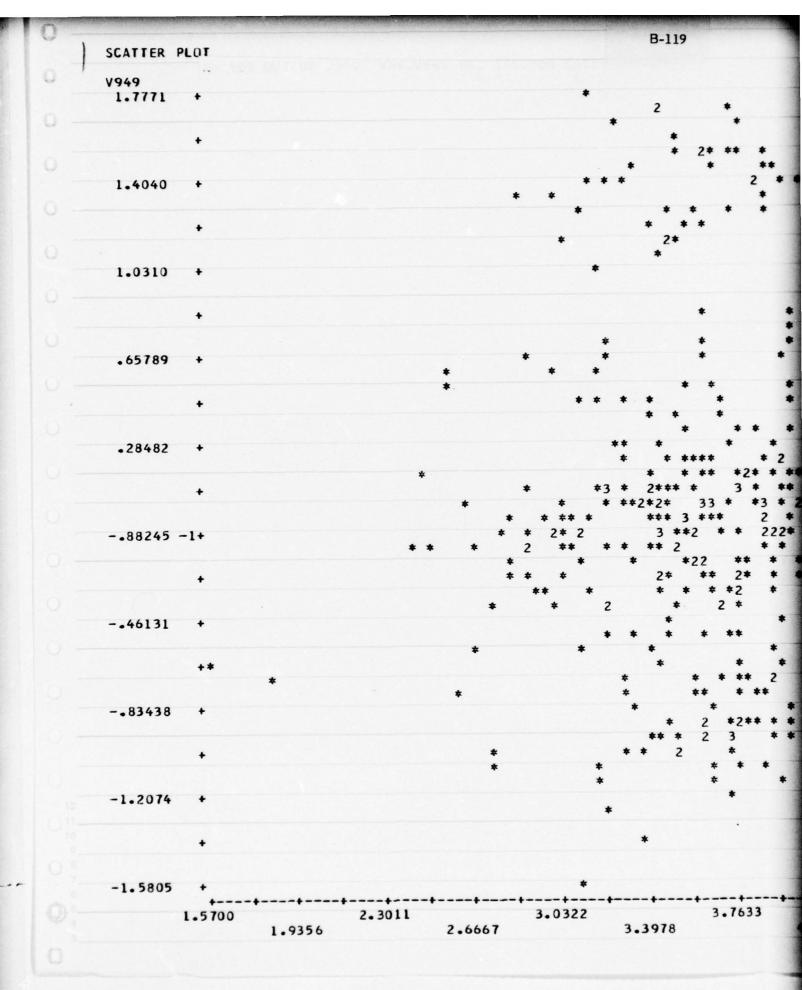


3.2389

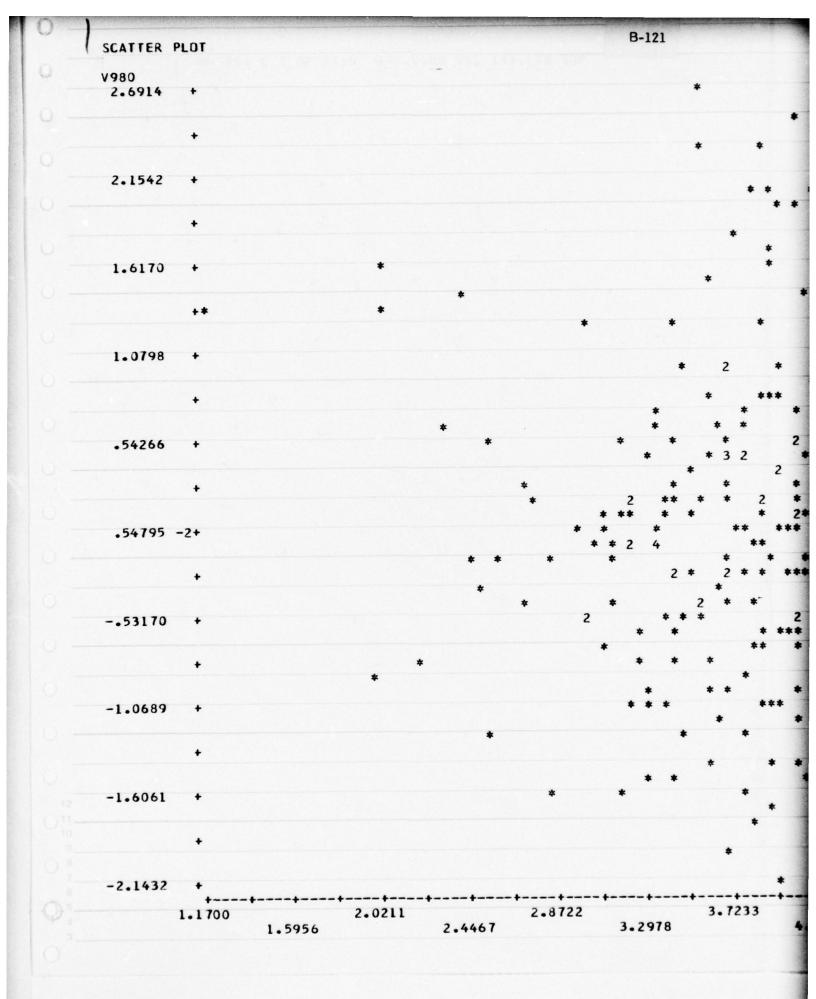


3.2222

333



							B-120	
SCATTER F	PLOT							
V980								
2.6914	•							
	•							
2.1542	+							
	•							
								*
								**
1.6170	•					*	*	
			*					
	+*	*						
1.0798	+							
								•
	+							
					*			* 2
•54266	+						*	*
								*
	•				*		* *	* *
				*		* *	* -	** 2
.54795	-2+					*	2 *	* *
				*	*	* *	* *	* 2
	+					*		**
				*			*	
E2170					*	*	*	* *
53170								**
								*
	+		*			*	*	*
						*		
-1.0689	+							
			*					*
	+							
1 4041								
-1.6061								
								2
	•							
-2.1432	+							
	1 0000	+	1.8889	-+	2.77	78	+	3.666
	1.0000	1.4444	1.000,	2.3333	2	3	.2222	

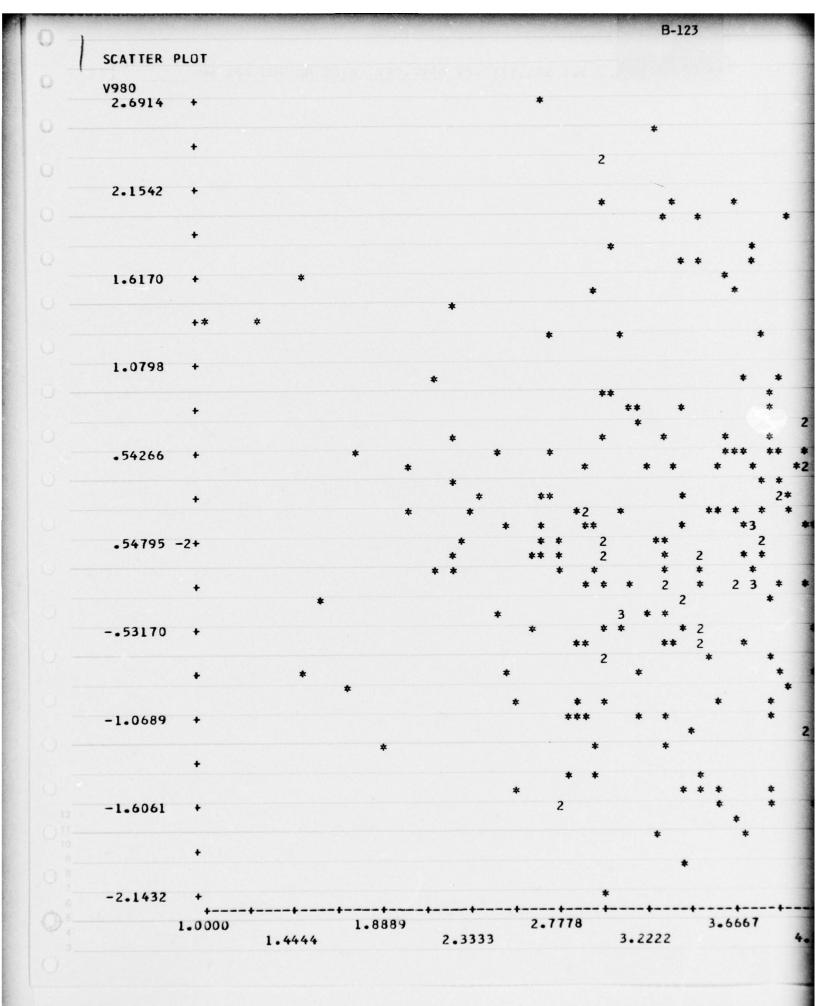


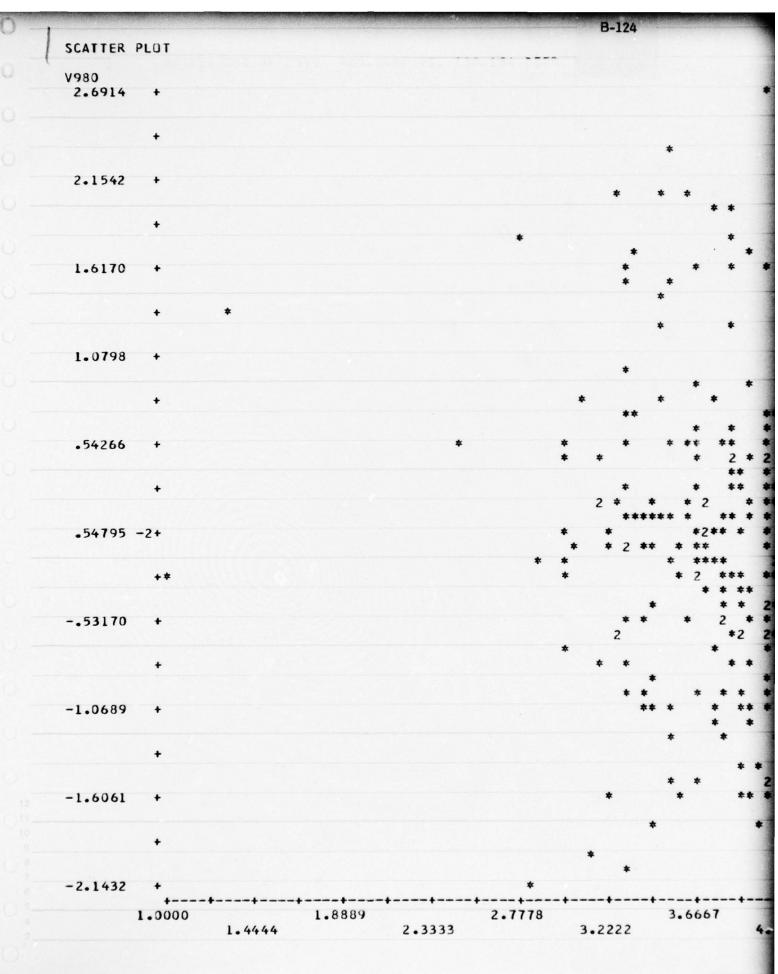
3.7233 2.8722

3.2978 4.1489

178 SUP 5.0000

0	SCATTED DIOT		B-122
0	SCATTER PLOT		
0	V980 2.6914 +		•
0			*
0	2 15/2 4		
0 -	2.1542 +		* **
	•		* 2
0			* * * *
	1.6170 +	*	* *
0	+2		
0			** *
	1.0798 +		* * * *
			* * * *
	•		* * *
	.54266 +	**	* * * * * * * *
			* * 3* * * * *
	•		* * * * * * * * * *
	.54795 -2+		**
			* * 3 * * * * 2 * * * * 2 * * *
	•	*	2 ** ** ** 3* *
	53170 +		* * * * * *
			* * * * * * * *
	•	*	* ** *
		*	* 2 * * *
	-1.0689 +		** *
	•		2
			* * * * * * * * * * * * * * * * * * * *
	-1.6061 +		** * * * *
			* *
	-2.1432 +		*
	1.0000	1.8889	2.7778 3.6667
		1.4444	2.3333 3.2222 4.1

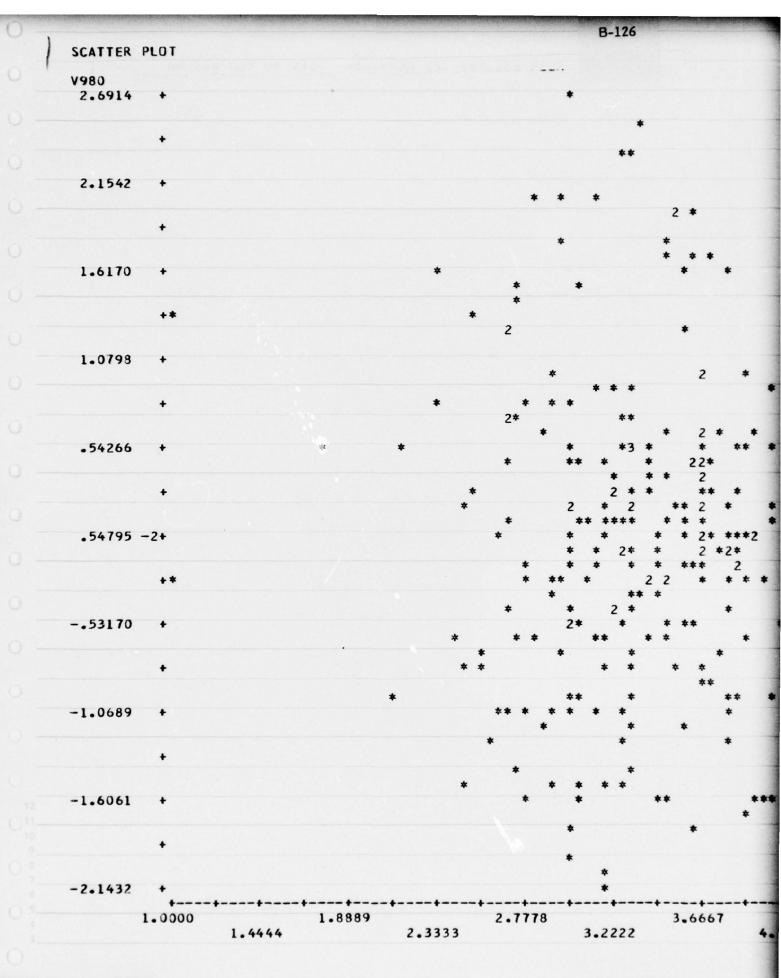


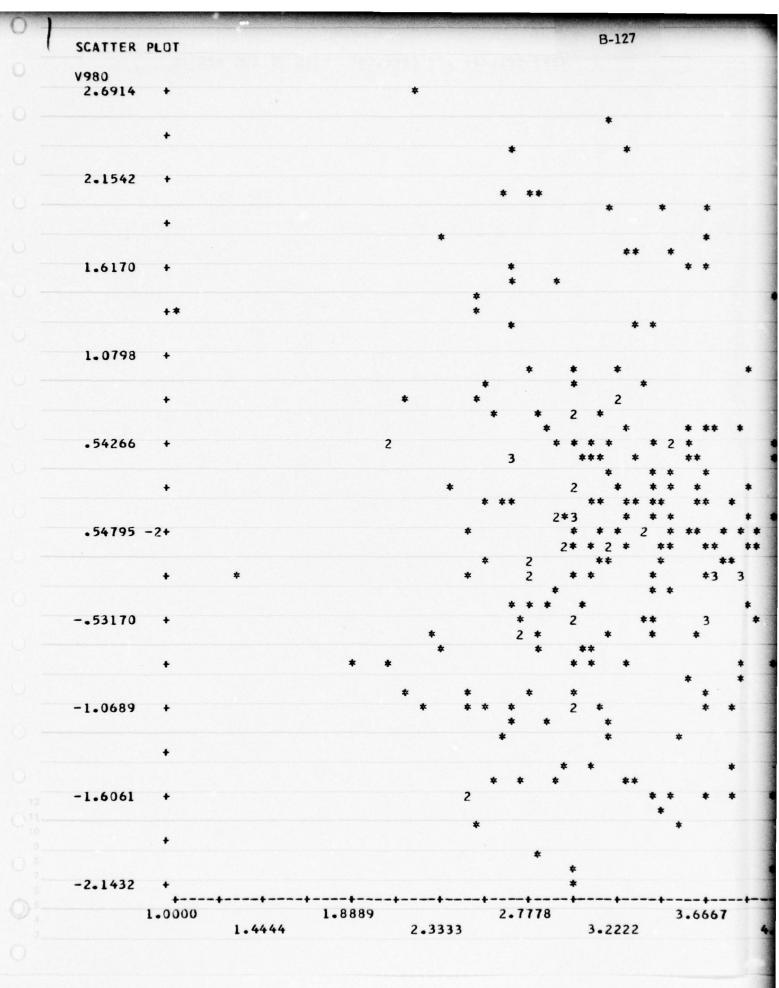


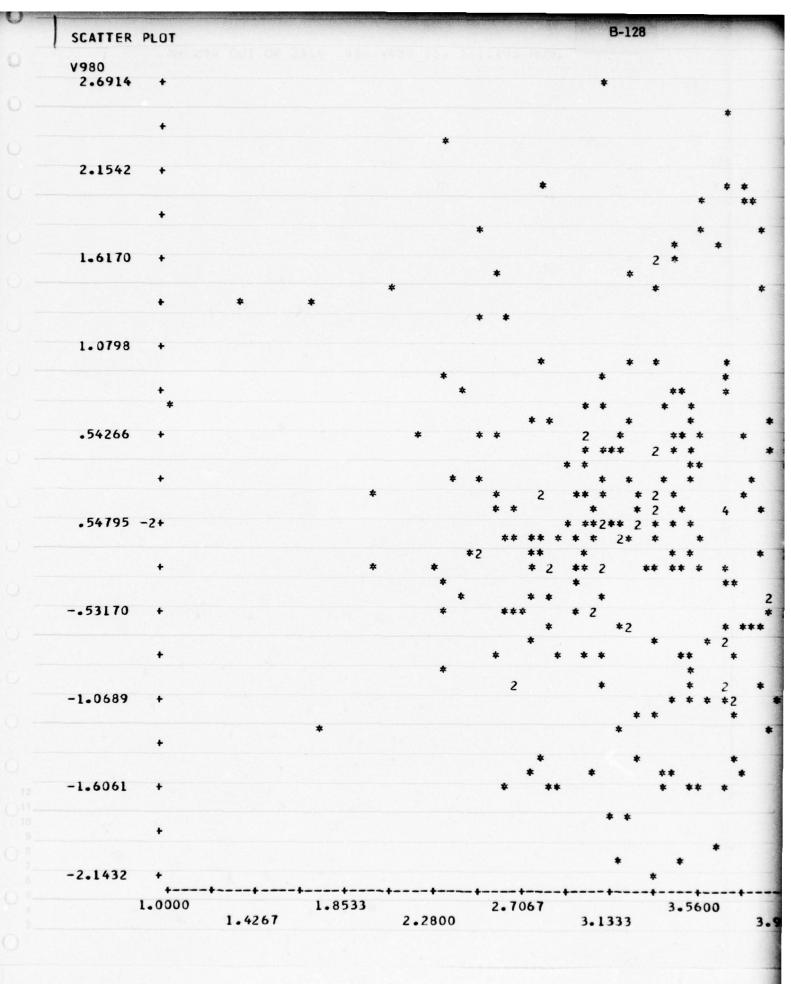
4.1111

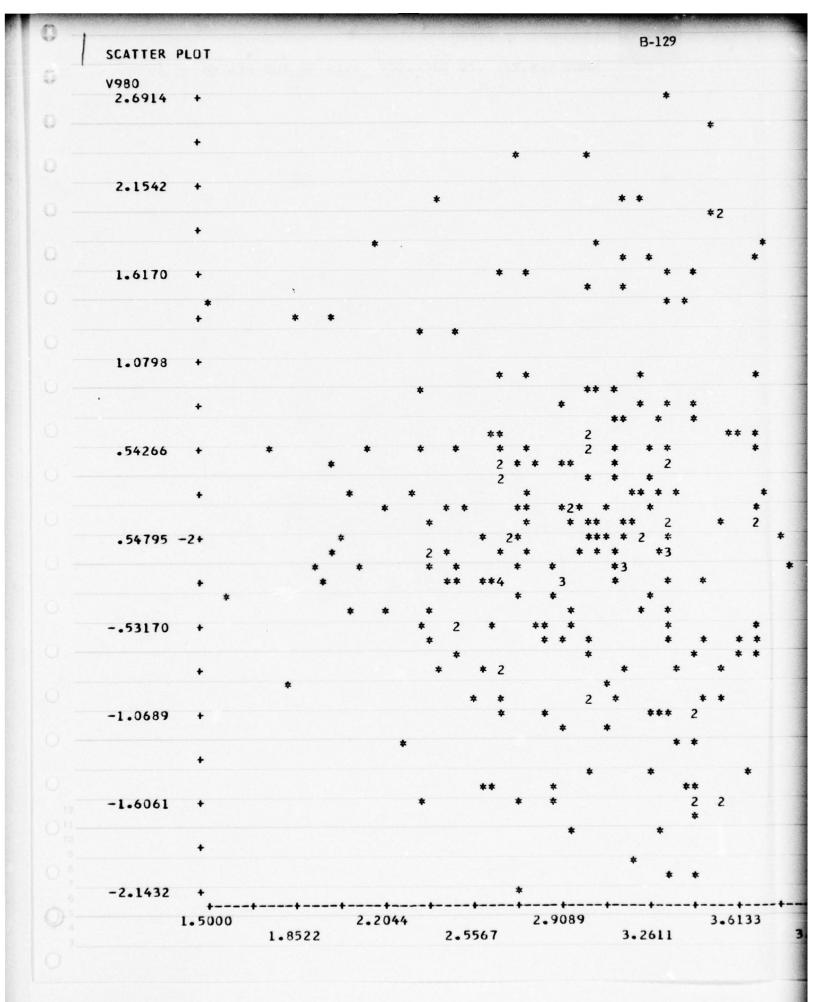
184 PEER 5.0000

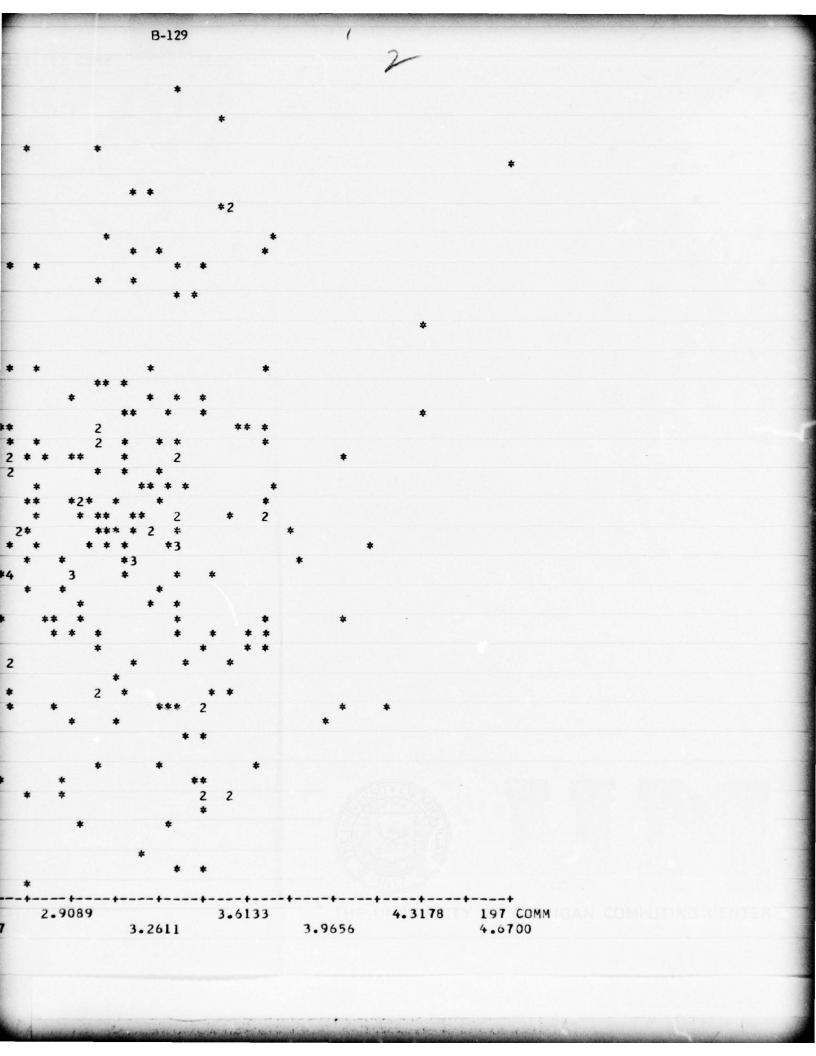
3.6667 4.3333 5.0000











3.0000

3.3333

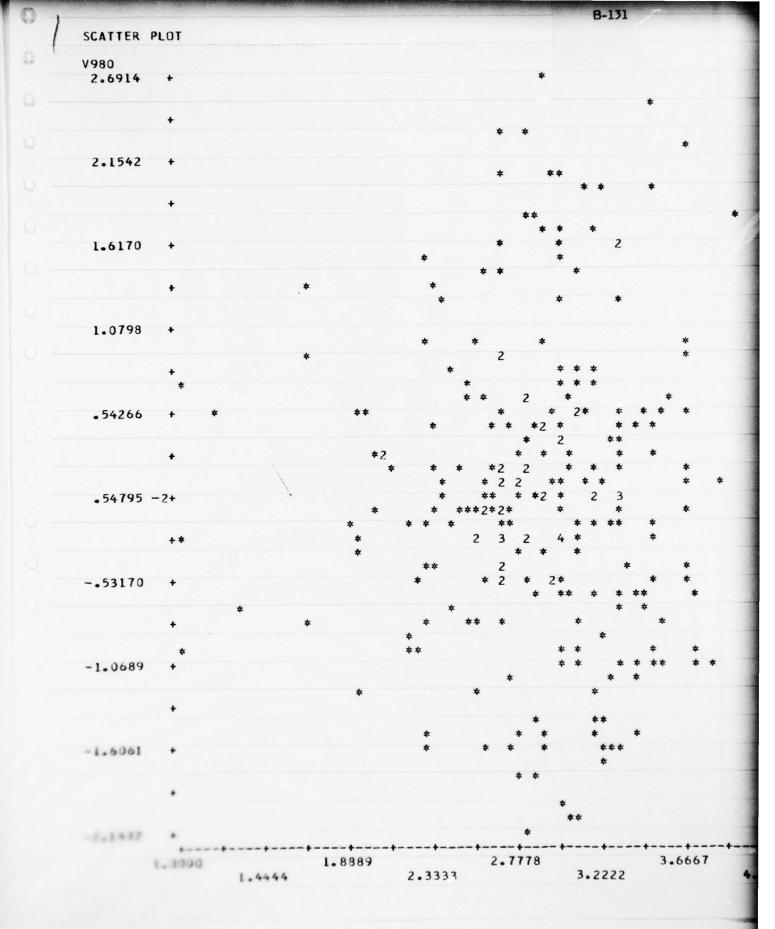
3.6667

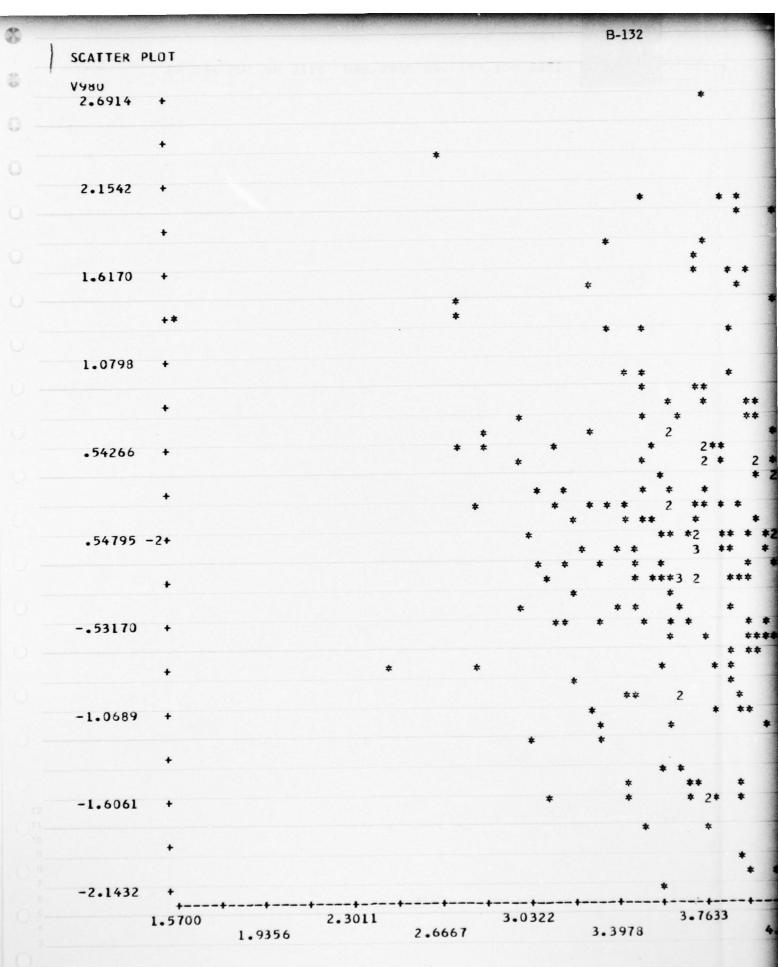
4.0000

\$

-2.1432

2.0000





3.0322 3.7633 4.4944 200 SATI 4.8600

1	SCATTER	PLOT							8-13	,		
1	V981											
	3.2960	٠								*		
		٠					*					
	2.7389											
		+										
	2.1817	+										
											1	
		•								*	*	•
	1.6245	+										
								*		*		*
										*	*	
	1.0674	+										
		+			*	* *		*		*	* *	* ***
	.51022	+							*	*		2* *
	• 51022		•			*	*	* *	* *	2	* **2*	
		+		*			*		*2	* *	***	*** 3
	46940	-1+				* *	*	2	**		22*2	* *2
				*		*	*	*	*		*3* 3	** 334
		٠.		*	*		*	* *	**		* *	* *
	60410	•			*		**	2 * *	* * *	*	*	* *
			*	•				•	* *	*	* *	*
								*			** *	* :
	-1.1613	+										
		+										
	-1.7184											*
	-1.7184	+	+		+	+	-+	+	+	+	-+	-+
		1.0000	1.4444	1.8889	2.3333	2.	7778	3.	.2222	3.	6667	4.1

```
B-133
                                      2
                                                   2
                                           176 SUP
5.0000
         3.6667
```

2.8722 3.7233

4.5744 178 SUP 5.0000 3.2978 4.1489

SCATTER	PLOT							В-	135	
V001										
V981 3.2960	+						*			
302,000										
				*						
	+									
						*				
2.7389	•									
	+									
2.1817	+									
	+				*	*		**		
								*		
1.6245								*		
1.0243										
	+			ŧ		*	2 *		*	
							* *	*	*	*
1.0674	+									
							*			
				* *	*	*	**	*	*	
	•							*		
					*	*		*	**	
•51022	+					* **	*	* *	* *2*2*	***
			*	**	***	* 2 *			** *	
	+		*		* *	*	2 **	* 4	*	**
			* *		**	2*	*			*
46940			* **	*	* *	2 2 **	2 2**	** *	22 *	2
40940	-14		**			3#	*2 *2222	223*2	**23 3*	* 2
						* * 2	22 * 4	* *4 2	2** **	3
	+		* *	_	* *	*** * **22	3 *	* *	2* ** 2* * 2	*
	*	*		* *	*	* *				2 **
60410			*		* 2	* 2	**		** *	*
							**		**	
	*		*		**	**	*		2	*
					* *		*	* *		*
						*	**	*		**
-1.1613	+							*		
								•		
	+									
							*			
-1 7104	+					*				
-1.7184	+	-++	-++	+	-+		+	+	++-	+-
	1.0000		1.8889			2.777	8		3.666	7
		1.4444		2.	3333		3.	2222		

Q

* 4 *4 22** 2* * 2*

2.7778 4.5556

4.1111 3.2222

180 SUP 5.0000

V981 3.2960 + * + * 2.7389 +	
* * *	
*	
•	
2.1817 +	
+ * * * *	
1.6245 + *	
+ * * * *	
* * * * * * * * * * * * * * * * * * *	
1.0674 +	*
2 * * +	
* * * * * * * * * * * * * * * * * * *	
* * * * * * * * * * * * * * * * * * *	, , ,
+	* *
**	**
* ** * * * * * * * 2 * **2** 2 **3 3 * * * 2 * 2 5***** 2 *** * * * * * * * * * * * * * * * *	*2*
** * * 2 * ** **	3
60410 +	2 2
* * * * * * * * * * * *	**
* * 2 * * * * * *	* *
-1.1613 +	
•	
-1.7184 + *	
1.0000 1.8889 2.7778 3.666 1.4444 2.3333 3.2222	57

3.6667 2.7778 3.2222

4.1111

182 SUP 5.0000

* 2

	1.0000	1.4444	1.8889	2.3333	2.7778	3.2222	3.6667
-1.7184	+	-+	•	+	+	++	*
	•						*
-1.1613	٠						
	•				*	* **	2 * *
60410	•					* *2 *	** *** *
	•	*			*	* * * *	*3 *2
46940	-1+*				**	* ** *3 * * *	2 2* * 4 ** *3 224*3 *22 ***5*32
	•				*	*2**	* * 2* 4 * *2 342
•51022	•				2		*2 *** ***2 22
	•			*		* *	* **
1.0074				*		* 2	* *
1.0674						*	* *
						***	* *
1.6245							
	•						* **
2.1817							
2.7389						*	
							*
V981 3.2960							
SCATTER	PLOT					B-137	

**

*2 342 ** ** **

2 2* * 4 3*2 2 *3** *3 224*3 6 2 * *3*

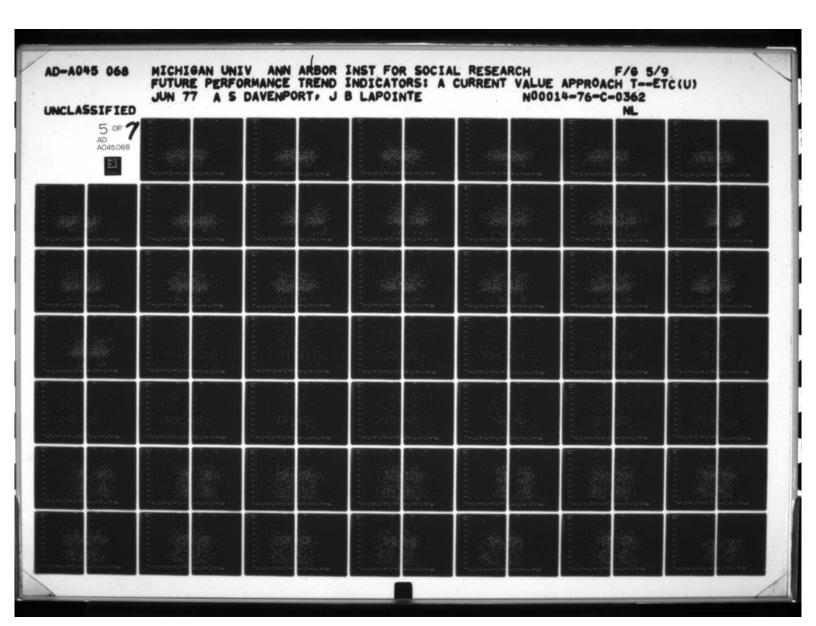
*22 ***5*32 2 323

2* *

3.6667 2.7778

3.2222

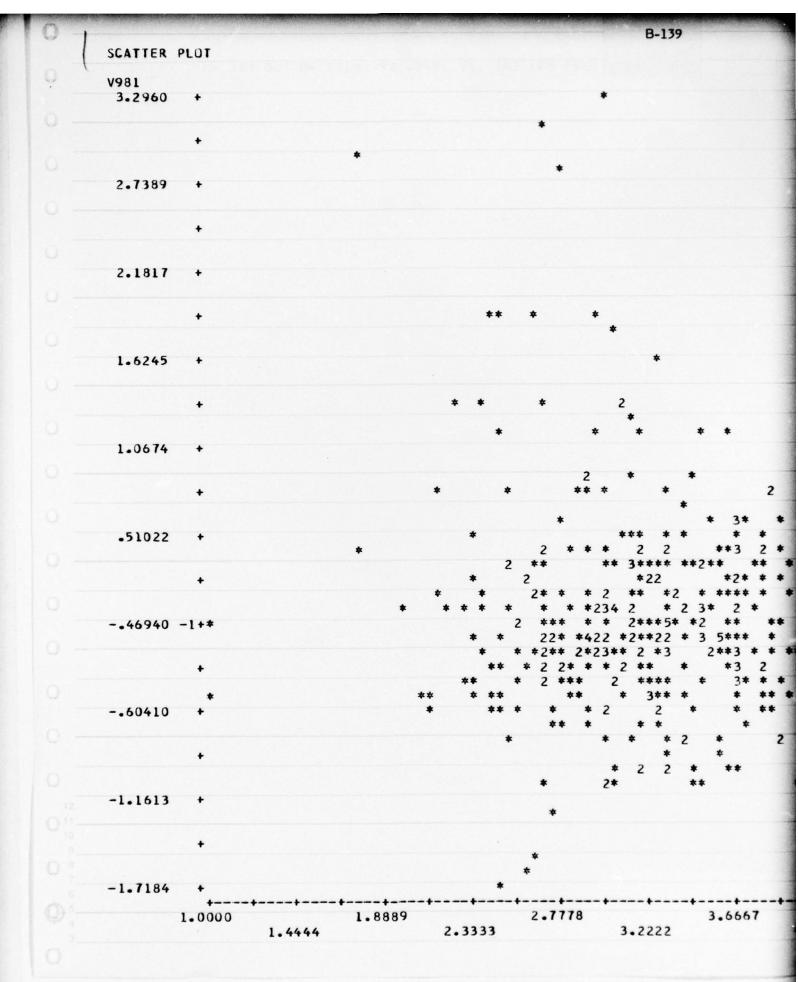
4.5556 184 PEER 5.0000



50F AD A045068



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-7



2.7778

1					B-14	10	
SCATTER	PLOT						
V981							
3.2960	+						
				*			
			*				
. 7					*		
2.7389	•						
	+						
2.1817	+						
	+			** *			
1.6245							
1.0245	•						
	•			* *	*2		
					* **	* *	
1.0674	+						
					* ** *	*	*
	+			*		2* *	
						*	
.51022				*	2 *	2 2 *	
•31022			*		2 * **	** * 2** * 2*	
				* * *	*22* **	* **2 **2*	*
	+		*	* ** *	* ** *	* ** * ** *	* 1
			*	2* * ***	*3 ** 2*2 2	2 *2 2 * *	
46940	-1+	*		* *	*2 *4 *	3*** *3 **	
				* *2*	2**3* 4 **	2*2 ***2 * 5 ** 2 * *3 *3	
	+		*		2 * 2	2 3 * 2 * *	* 1
			*	*	2 ** *32 *		
60410	.*			* *2	** *** 3*	*2 * * *	*
60410				*	* **	2	
				*	* * *	* **2	
	+				3	* * *	*
				* *	* *	* **	
-1.1613	+						
					*		
	+						
					•		
-1.7184	+	-++	·	·+	+	-++	-+
	1.0000		1.8889		2.7778	3.6667	
		1.4444		2.3333	3.	2222	4.

```
B-140
   *2
                                          ** * 2 *
      4 **2*2 ***2
    * 3232 2 *
* 2 2 3
 * *32 *
*** 3*
      2 2*
                                                         190 PEER
5.0000
                                           4.5556
                     3.6667
778
                                  4.1111
        3.2222
```

0	Section of the sectio						8-141	
	SCATTER P	TOP						
0	V981							
	3.2960	+						*
0						*		
		+						
							*	
	2.7389	+						
		+						
	2.1817	+						
						2**		
		+			*	2++		
	1.6245	+			*			
				*	*	2		
		+			*	2		*
						*	** *	
	1.0674	+						*
						*		
							**	* *
		+		*	*	* *		* * *
							* *	* * *
	.51022	+				*		* *
	•>1022				*	* * 4		3** 3
				*		* 2 * *	* **3 * 2	
		+			**	*	2 ** *	2 * ** 22
				*	* ** **	* * 2*	* 2** 2	* **2* 3 2
	46940	-1+		*	*	* 3 *	** 2* *2**	* * 3**
	• 40,40			*	* * *	* 222 22	22 *2***2*	*2*2 ** 3*
		*			*** *		2 23 4 *	4*2 ** **
		+		* *	*			* *** * *
				*	* *	* * *	2* * *32 * *	
	60410	+			*		2 **2	* **
	60410				*	*	2	*
			*			3	*	2 *
		+					*	*
					*	*	* * *	* **
	1 1412							
	-1.1613	+						
		+						
								*
						*	*	
	-1.7184	+			+	+	+	-+
		1.0000		1.8533		2.7067		3.5600
			1.4267		2.2800		3.1333	

```
3.5600
                                        4.4133
                                                  196 HUM.
4.8400
1067
        3.1333
                             3.9867
```

B-141

2 *2

22

3.5967 8811 3.2389

3.9544

4.3122 197 COMM 4.6700

3.1500 2.7800

3.8900

3.5200

-1.7184

1.6700

2.0400

2.4100

B-143

-						-					
	SCATTER	PLOT							B-144		
	W001										
	V981 3.2960	+					*				
	3.2900	•									
		+									
					*						
									*		
	2.7389	+									
	20130										
		+									
	2.1817	7 +									
		+			* 2		*				
				*							
	1.6245	+		*							
		+		2	* *	*					
						*					
					2*		*			*	
	1.0674	+ +									
								*			
					*	*	*		*	*	
		+		* *	*			*2*		* *	
										*	
						*		2 **	* *		
	.51022	+			**	** *			*	* **	
				* *	* *	22		*** *			
					* * *		*2* 3			* * *	
		+	*	*	* *		* * :			*	*
			*		* * * ***2 *	***2*			**	3 **	
	44046		*	*	***2		* **		* * 2		
	46940) -1+2		**			24 23	225+++2	** *		
		*	*		* **2*					* *	
		+			** 2			* * * *			
				* *			** *2		* 2	*	*
				* *		* * *2		** *			
	60410) +		* ** *		**		* *	-		
	•00 110			*	*			*		*	*
				* * :	*	*		* 4	***		
		+						* *			
				*	*		* ***	**			
							*	2	** 2		
	-1.1613	3 +									
		+									
								*			
						*					
	-1.7184	+			*						
		+-	+	+	-++-	+-		+	+	+	+
		1.000		1.8889			2.7778			3.6667	7
			1.4444		2.333	33		3.2	2222		4

2.7778

4.1111

4.5556 199 DEC. 5.0000

3.2222

*

3.0322

3.7633

4.1289

--+---+ •4944 200 SATI 4.8600

1	SCATTER	PLOT						B-	146		
,	V982										
	2.9526	+					*				
									*		
		•									
	2.4123	•									
									*		
	1.8721	+								*	•
		•									
									*		
	1.3318	+					*			*	
		+					*	*	*	*2	* *
											-
	-79153	+*		*						** *	* .
								. *			* *
		+	*		*	*		*	*** * *	*	*
						**	*	*	* *	* *2	3
	.25126	•				*	*	* *	* 21	2 *	
						*	* *		* *3**	* **2	
		+		*		*	*	* *	* * * *	* ** 2* *	2***
	22222					*	*		*		**
	28902	•		*	*	*	2	* *		2****	**2
							3 2		222	2 * 2	#2
		•		* :			* *	*	2		2
	82929						* *		*	**	*
	02929	•								•	
		+									
	-1.3696	+		•						*	
								*	*	**	
		+						•		*	
									*	*	
	-1.9098	+								*	
		1.0000	+	1.8889	·	2-	7778	+-	3.	6667	-+
			1.4444		2.3333			3.222	2		

\$

2.7778 3.6667 4.5556 176 SUP 3.2222 4.1111 5.0000

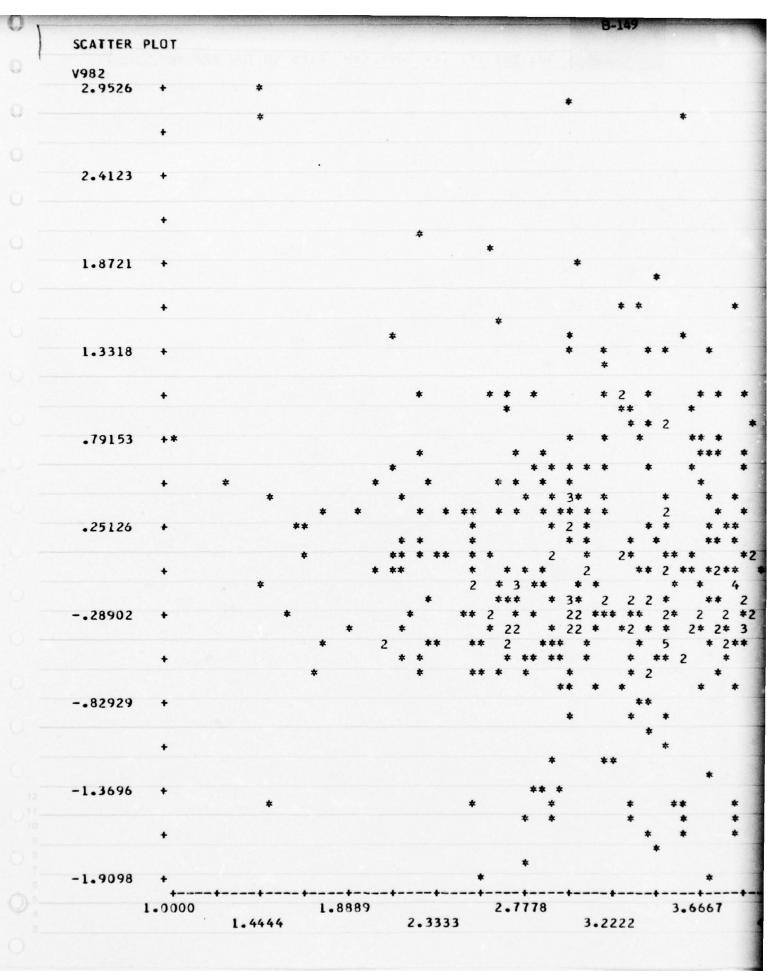
						B-14	7	
SCATTER	PLUI					D-14		
V982 2.9526								
2.9326	•					*		
	+			*				
2.4123	+							
244223								
	+							
					*		*	
1.8721	+						•	*
								*
	+							*
						*	*	* *
1.3318	•					*	* * *	2 *
	+					* *	2* *	4
							2	** *
.79153	+		*	*		*	*	** 2
	+*			*		** * *	2 *	k
	**		*			2	* **	4 ***
-25126	+		*	* * *	* 23	* *	*** *	**
					*	* * 2*		* *
	+			*	* *	* **2 2 *	* ** 22 2*2*2	** * 4
					* *	2 * **	* 2 3	** 2
28902	+			*	* *	* ** *	* **2 *2 **2 32	*222**
				*	* ** 2	2 2 **	****2 2 ** *4	**2 62 ** *2*
	+			*		** *2	* * *	* * *
			*	*	2	* *	*	* * 2*
82929	+						*	*
	+					*	*	*
-1.3696	•		*			* **	* .	***
					*	*	*	*
							*	
-1.9098	+					* *		
1	+	-+	++			· +	++	+
	1.1700	1.5956	2.0211	2.4467	2.8722	3.2978	3.7233	4.

2.8722 3.7233 3.2978

4.1489

178 SUP 5.0000

SCA	TTER	PLOT								B-14	В		
1 400	•												
V98	2												
2.	9526	•		*					*				
									*				
					*			*					
		+											
2.	4123	+											
		. +											
						*							
								*					
	8721	+								*			
1.	0121									*			
								*		*	,	*	
		+						*					
								•			*	*	
				*							*	•	
1.	3318	+			*		*		*	. *	*		
										*		*	
		+					*		2 ***		**	*	*
									*	*2	*	*	
								*	* *		2 *		* *
.7	9153	+*				*	*	*		* *		*	**
				*		*	*		*		*	*	*
						*	* 2			* **	**		7
		+*				* *	*		* *	* *	*		
				*			*	*	* *2	* 2 *	***	***	*
				***	* *		2	*	**	*	*	**	2
,	5126	+		* *		*			2 *		* *	,	* *
• 2	2120				*			2		*	**	**	* *
				*	* *					* **	2*		2
		7		•	**	* * *		* ***			3***	2	*
		+			**	*2			***	* *3*			**
				*			2			*2 2**		* *	
											2** 2		
2	8902	+		*	*								
				* *		*		**	* *	5	2* 3	3	*4
						2 2 *	** 2			***	* 2	**	
		+			*	2		**	2*	*	*2*		*
			*				2* *		* *	*	*		**
							*	*				*	*
8	2929	+							*		*		
				*			*					*	
											*		
		+									*		
									*2				
										* *	•		*
-1.	3696	+					*		*		*		*
				*			2	*	*	* *	*		
							*	* * *			*	*	
		+								2	*	*	
											*		
								*					
	9098	+						k			*		-
-1.	3030		-4				-+			+	-+	-+	
		1 0000		1 0000			2	7770			2	6667	
		1.0000		1.8889	-	2222	2.	7778	-	2222	3.	0001	
			1.4444		2.	.3333			3	. 2222			



2 *

2.7778 3.6667 4.5556 182 SUP 3.2222 4.1111 5.0000

						B-150	
SCATTER F	LOT						
V982							
2.9526	+					*	
							*
	•						
2.4123	+						
	+						
							*
1.8721	+						*
						**	*
	+					*	
						*	2
1.3318	+					*	- 1
	+				*	2 *	2 * *
						*	*
.79153	+	*				*	* *
					*	*	* *
					*	*	,
	+				* *	*	* *
				*	* *	***	* 2 *2
.25126	+		*		* *	** 2	
						* *	2 *
	+				3	* * 2	**** 3
						* **3 *	
28902	+				*	* *	* 2 **
•20,02							2 53 2
							2 2* *
	+				* **		*
					* *	*	* *
82929	*						
	•						
	+						
-1.3696	+						
-1.5070						* *	
							* *
	•						
						*	
-1.9098	•				++	+	-+
	1.0000	+	1.8889		2.7778		3.66
	2.0000	1.4444		2.3333		3.2222	

3.1944 3.9167 4.6389 186 PEER 3.5556 4.2778 5.0000

3.6667 4.5556 188 PEER 3.2222 4.1111 5.0000

2.7778 3.6667 190 PEER 5.0000

3.2222 4.1111

SCATTER	PLOT					B-154	
V982 2.9526	٠						
	•				*		
2.4123	•						
	٠				*		
					*		
1.8721	•			*	*		
	٠		*		*	*	•
				* *			•
1.3318				* *	*	* *	
	+				**	** 3	* * 2 *
					*	*	* * * * * * * * * * * * * * * * * * * *
.79153	+		*	*		* *	* 2 * 2
		*	*		** 2	* 2* *	** * *
	•		•		*	* 2* * *	5 2*2
25124	*			* * *	2 *	* * 2*	
.25126	•		* *	* *	* * 2	** * **	* 4* * 2* *
	+		*	* 2 *	2 **		2* 2* *** 2 2 * * **
			*	* * *	2	* 32 *	* * ***
29002				2 *		2 322 3*4**	
28902			*	* * *2	*** *	2 *2*2 **	2 * ** 4
	+	*	*	* *	2 22	2* ** * *	* * ** 2* * 2*
				* *		***	2 2
82929	+			*	*	* *	* *
02929			*				
	+						
							2
-1.3696	+				*	* *	* 2 ** *
					*	* * *	* 2*
						*	
-1.9098	+				*	*	
	1.0000	++	1.8533	++	2.7067	· ++	3.5600
	1.0000	1.4267	1.0773	2.2800	2.1001	3.1333	3.7000

Q

196 HUM. 4.8400

3.9867

3.1333

2 197 COMM 4.6700 4.3122 3.5967 2.8811 3.2389 3.9544

*
3.1500 3.8900 4.6300 198 MDTI
3.5200 4.2600 5.0000

SCATTER	PLOT			B-157	
V982					
2.9526	+		*		
			*	*	
	+				
2.4123	+				
	+				
			*		
1.8721	+		*		
1.0121			*		
				* * *	
	+	*		* * *	*
		*			** *
1.3318	+		* *	* *	* *
	+		* * *	* 2* * 2	4 * *
			*	** * * *	
.79153	+		*	* * ** 4	*
		*	* *	* * * * * * * * * * * * * * * * * * *	* *
	+	*	***	* * ***	
	*	*		* *****2*2** * * 2 * ** 2	* * 2
.25126	+		* * *	* * * **	* **
		* 2*	** 2 2* 2 *** **	* ** 2 2*2 2* 2 *	
	+	7 27		* * *** 3 ***3*	
		* * *	* * 2 *	* 2 2** 2*	
28902	+	* *		2*2*2 *** **2* * **22****2 2 * * *	
			2*** * * * 3	** 2 * *3*2****	*
	+	***		* 2* * * *2 *2 * 3* ** * *	2 *
		*	2 * *	***** * * *	
82929		*	*	* * *** *	
02929	*				*
					*
	•			* **	
					* 2
-1.3696	•	*	*	* * *	* *
			*	* * *	* *
	•			* * * **	
				*	
-1-9098	+		*	*	
	1.0000	1.888	9	2.7778	3.6667
		1.4444	2.3333	3.2222	

*

\$

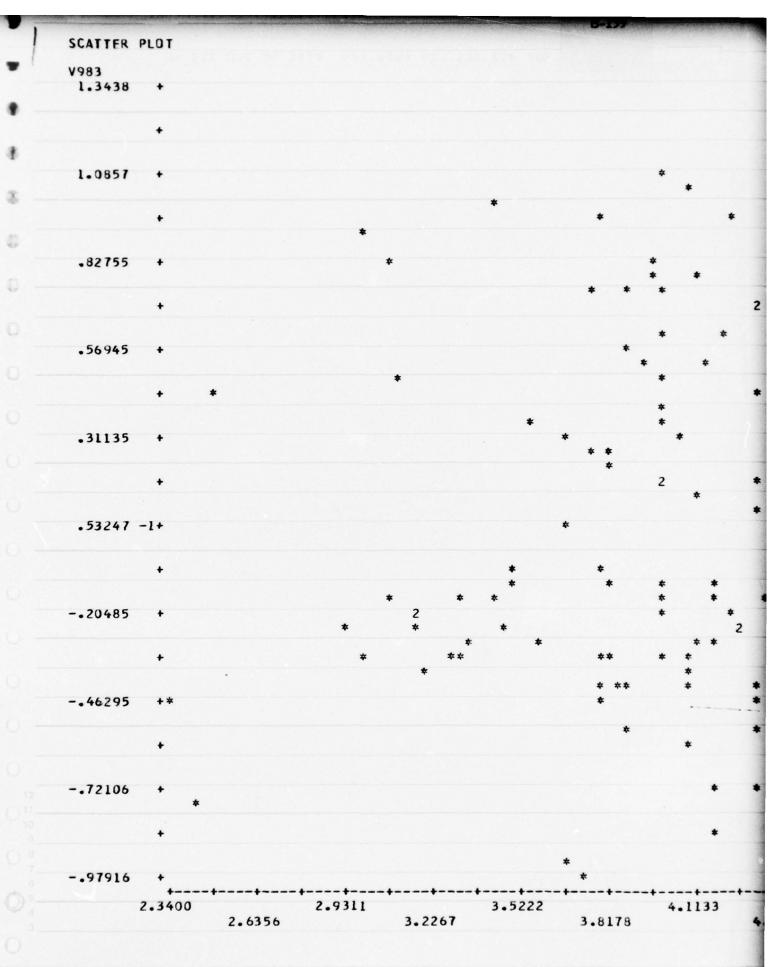
* ---+---+---+----+----+----+ 2.7778 3.6667 4.5556 199

3.2222

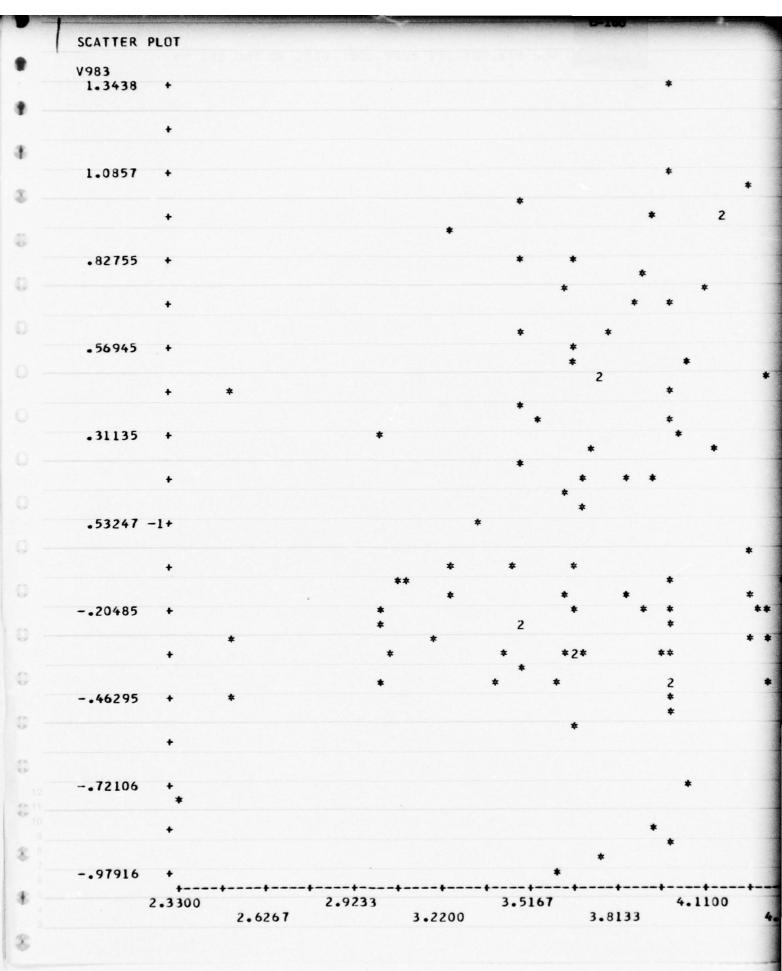
4.1111

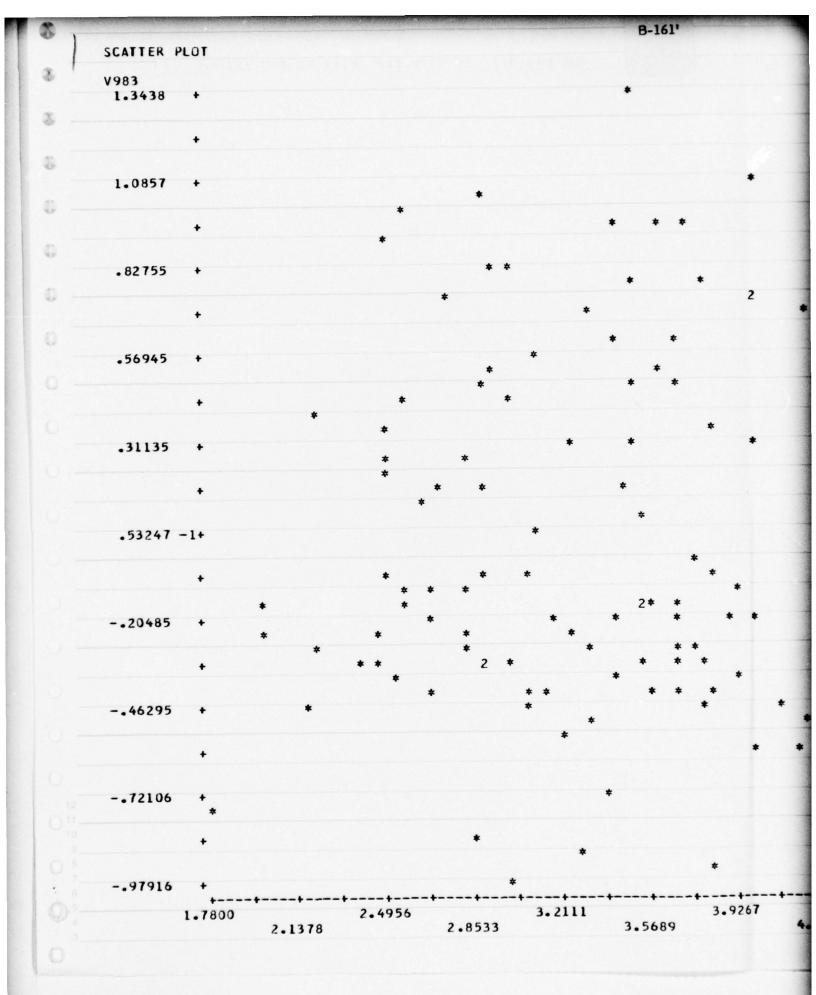
4.5556 199 DEC. 5.0000

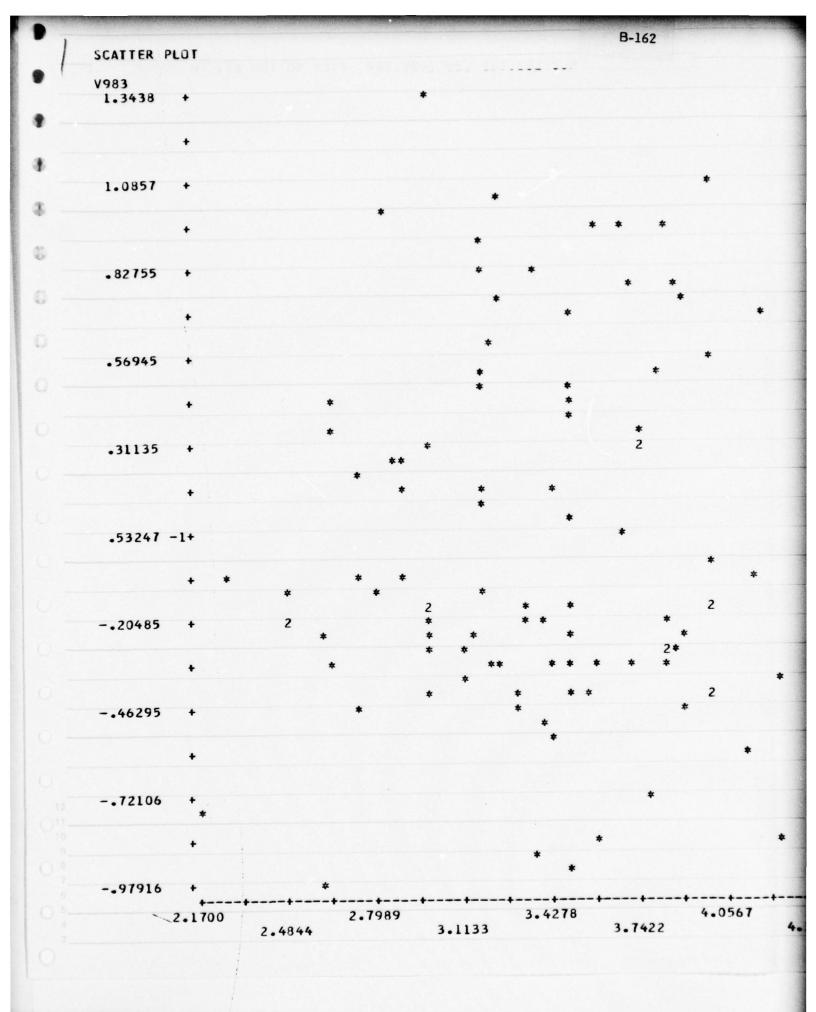
SCATTER	PLOT						B-	158	
	7201					ar safer			
V982 2.9526	•						•		
	+					*			
2.4123	e-+								
	٠								
1.8721							* *		
							*		
	•			*		*		* *	*
1.3318	+	3		*				* * *	*
	+					*	* *	* *	* * *
.79153	+*			*			*	*	* * **
	+			*			*	*** *	2 2
25124				* *	2	***	* * 2 2* *	*2 * *2	* 23 * ** 3
.25126				*	2	2 ;	*	* 2**2	* ** *
	•				*	* *	-	22*2	2 *2 *2
28902	•				*	* 2 * 3* **	* * 2* *2* 2	2 2 **	* *4 3
	+			* *	* *	2 * *	* * * *	2	** 2 *
82929								* 2	* *
						*			* *
						*		**	
-1.3696			*		*	*			* **
	•						*		***
-1.9098	+	-+	+t	+	+	+		**	+
	1.5700	1.9356	2.3011	2.6667	3	3.0322	3.397		3.7633



3.5222 3.8178 4.4089







1	SCATTER	PLOT					B-163	
,	V983							
	1.3438	+						*
		•						
	1.0857	•				*		
		٠				*	2	
	02755						* *	
	.82755						**	*
		•					*	
						*	*	
	•56945						*	
		•		*	*	* *		
						*		*
	.31135	+*						2
		+			*			. *
					*			*
	.53247	-1+			*			
		+					*	
				*	*	*	*	* * *
	20485	•	*	*	*	*	* *	* * *
					*		* * * * * * * * *	* *
		+				2		*
	46295	+			* *		* *	** *
	40293				*			* 2
		٠			*			•
	72106	•					* *	*
							*	
	97916	+				+	*	
		2.0000		2.6667		3.3333		4.0000
			2.3333		3.0000		3.6667	

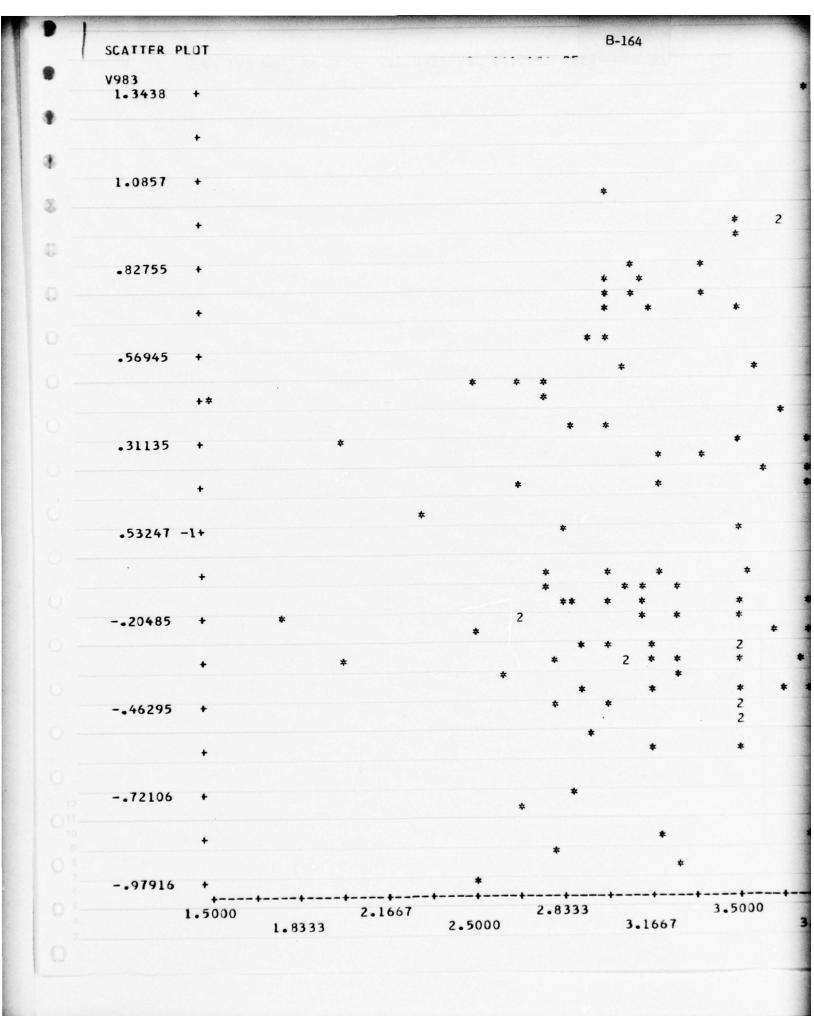
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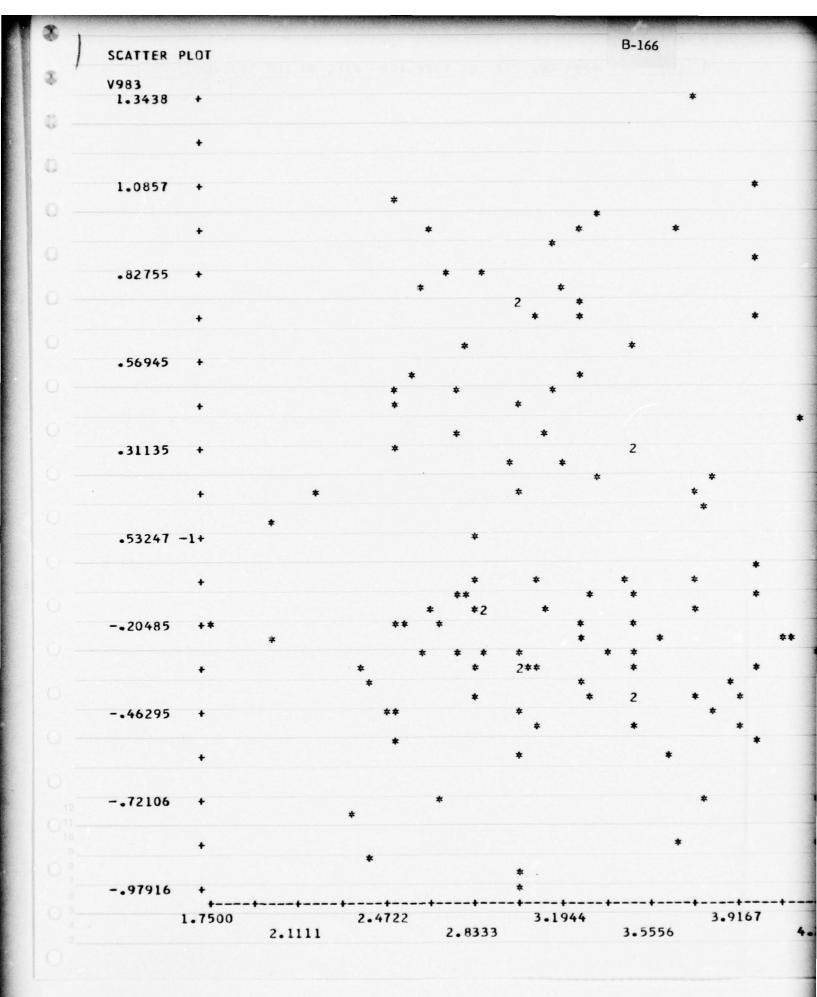
3.3333 4.0000 4.6667 184 PEER 3.6667 4.3333 5.0000

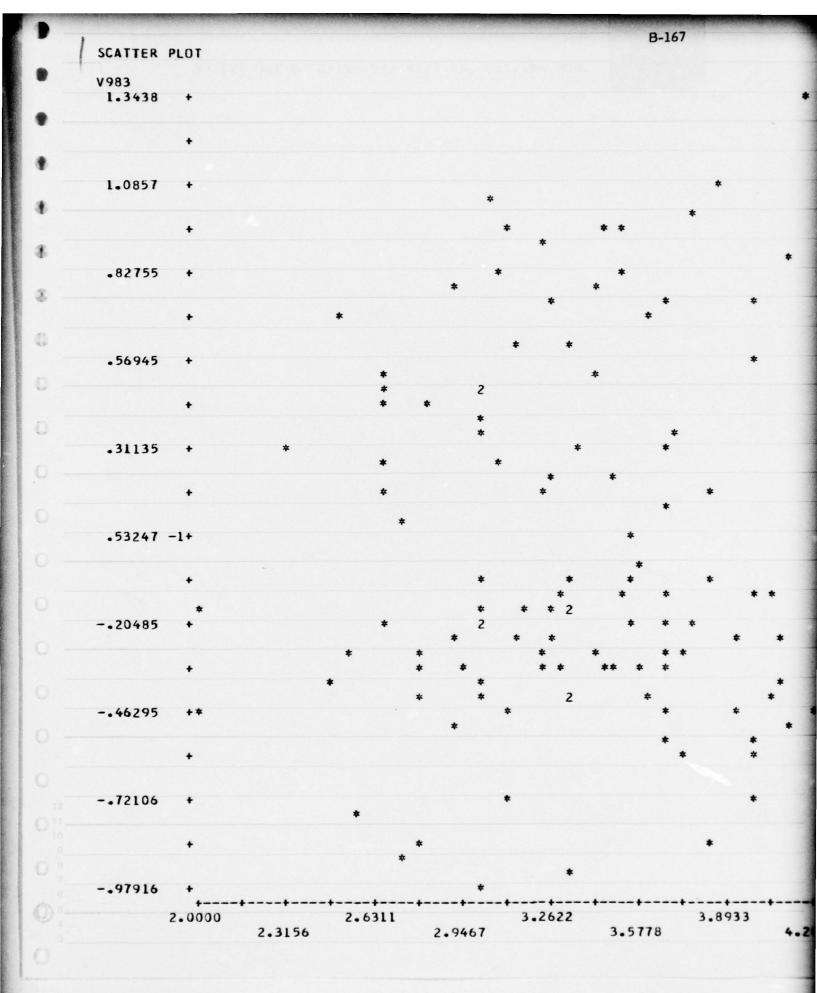


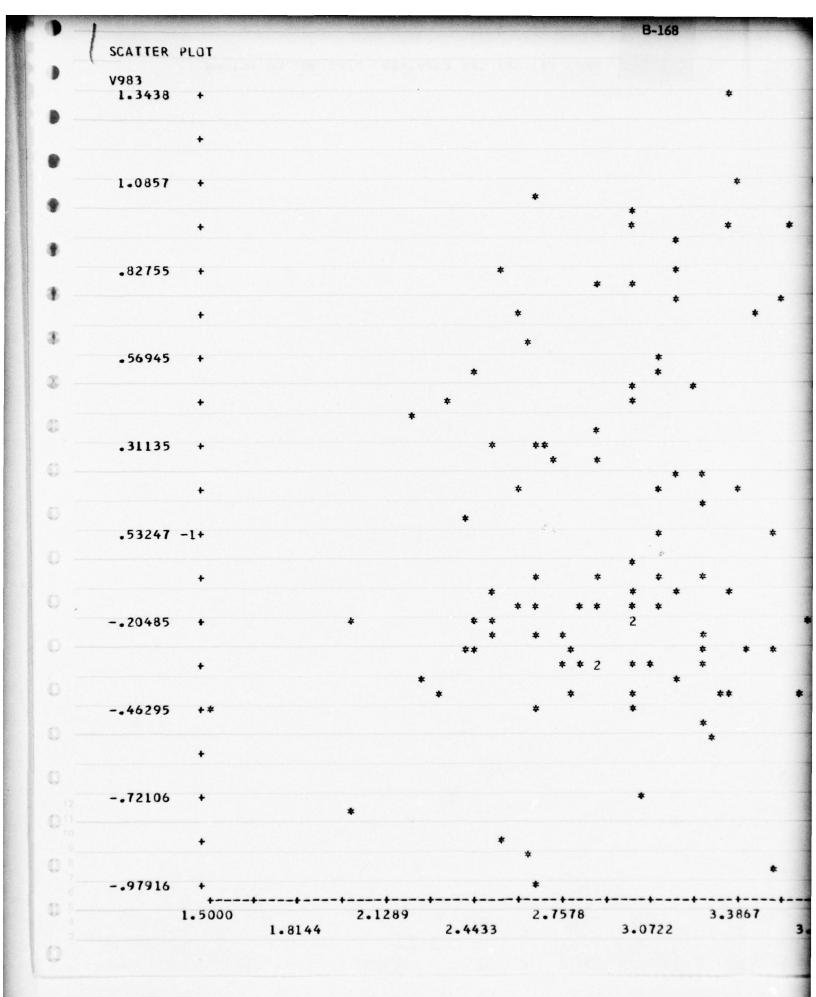
1							D 1/5		
1	SCATTER	PLOT					B-165		
	V983								
	1.3438	•					*		
		+							
	1.0857	+				*		*	
				*		**			
		•		•		*			
	.82755			*		*			
	•02133				* *				
		+			*	*	*		
				*			*		
	.56945	+							
				*	* *	*			
		+			2				
				*	*	*			
	-31135	+*			* *				
			*				*		
		+ *		*			*		
	50047		*			*			*
	.53247	-1+							
		+		*	*		* *		
				*	*	* *			
	20485	+ *		* *	* * *	* *	*		
			*		*		** * *	*	
		+		* * 2	** *			**	
				*	* * *		* *3		
	46295	+	*	*	* *		* *		
					*	*		*	
		+					*	*	
	72106	+			*		*		
							*		
		•					*		•
	97916				*	*			
	91916	+	-++	-++	++	+	-+		-+-
		2.0000	2.3333	2.6667	3.0000	3.3333	3.6667	4.0000	

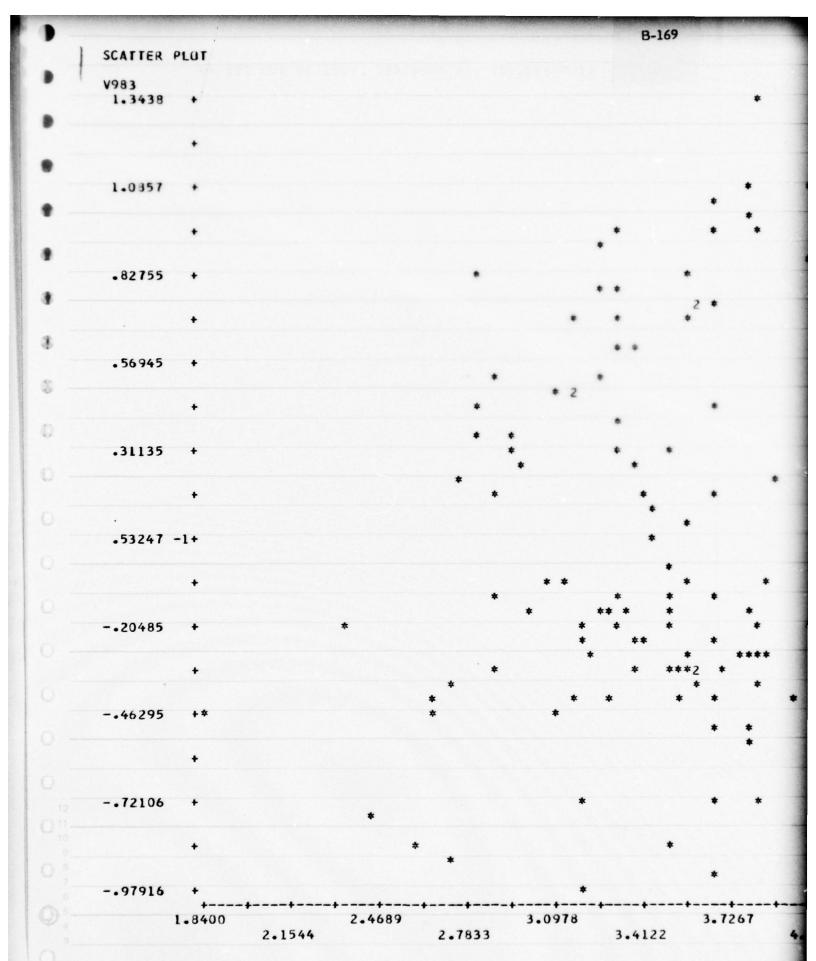
4.3333

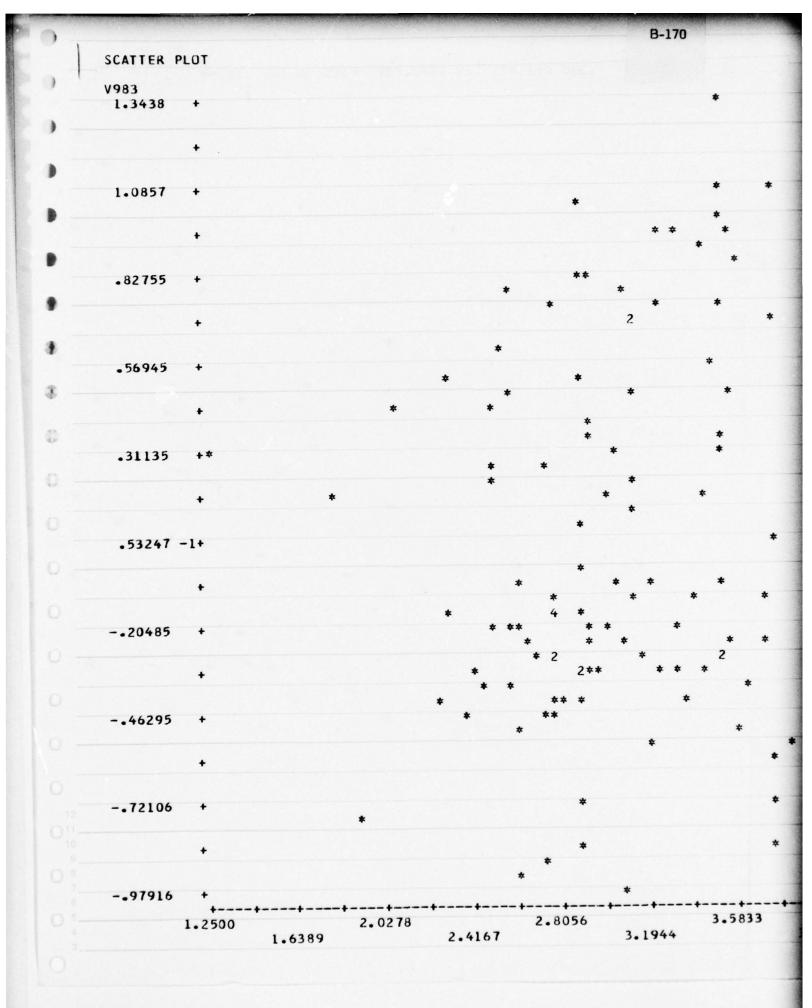
3.6667

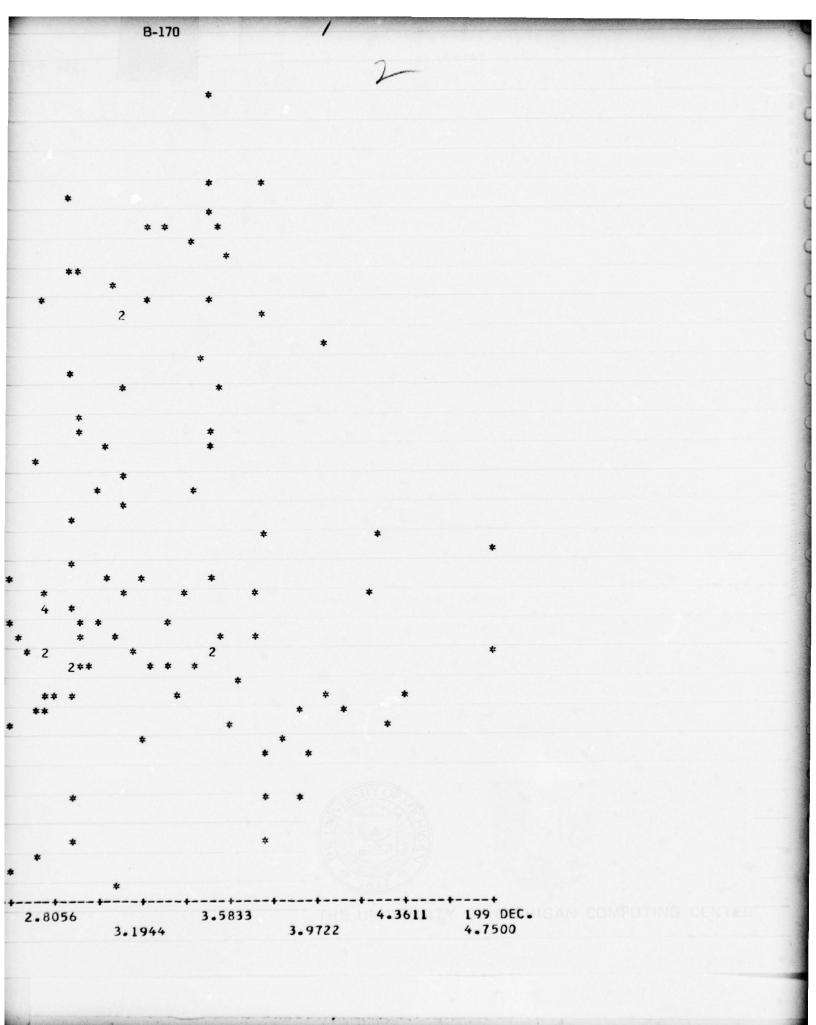












							0 171	
	SCATTER	DIOT					B-171	
	CHITER	PLUI						
D	V983							
	1.3438	+						*
		+						
	1.0857	+						
	1.0031						*	
							*	
		+				*	* *	
						*		
	00755							
	.82755	+		*				
						*	*	
		+		*				
*							*	
	-56945	+					*	
3						*		*
			*	*				* *
		•	*				*	*
3						* *		
	•31135	+					2	*
53					*	*		
0					*		*	
		+			*	*		*
0						*		
	.53247	_14	*			*		
	•33241							
0							*	
		+				*	*	*
0					*	*		* *
**	20105			*	* *	* *		*
	20485	+*			* *	* *	* *	
				*	* *	*		* *
		+			* *	* * *	* * *	* * *
					*		*	*
0					*	* :	* *	*
	46295	+	*				*	* *
0							*	
		+					*	
	72106	+				*		
0		*						
10								
		+				*		
0					*			
7	97916					,	*	
etho.		+	-++	+	+	+	-+	+
4		2.6500		3.1722		3.6944		4.2167
			2.9111		3.4333		3.9556	4
0								

3.6944 4.2167 4.7389 200 SATI 3.9556 4.4778 5.0000

SCATTER P	LOT					B-17:	2
V984							
2.8686	•		•				
	+						*
2.3234	+				*		
	+						*
1.7782	+						
						*	
					*	* * *	
	+				*		2
					*	* * *	*
1.2330	+			*	*	*	* :
				*		*	
	+					*	** * *
					*	* * *2	2* 2*
-68774	+						* * :
						* *	*2 * * *
	+*	*		*		*	**
			*		* *	*	* **
			*		**	* * *	* *2*
•14251	•				**	*	*
					*	*	*
	+		*			* *	* *
			T			*	
40271	+					*	* 2 *
					*	*	*
	+						*
					* *	*	* * *
94794	+					* * *	* **
• / • / •					*		*
					*;	2 *	* **
	•					**	*
							* * *
-1.4932	•		*	*		* * *	**
			7		*		
	+					*	*
							*
-2.0384	+						*
	++	+		+	+	-++	2 666
	1.0000	1.4444	1.8889	2.3333	2.7778	3.2222	3.666

2.7778 3.6667 4.5556 176 SUP 5.0000

SCATTER	PLOT				B-173	
2.8686	•			*		*
					*	*
						*
2.3234	•				*	
	•				*	
1.7782					*	
	+				* *	
				*		
1.2330			*		*	
	+		•		* * 2 2*	* *2 *
					2 * * *	4 **** *2
.68774	•				* * *	* * *** 3 *323 4
	+*		*	*		2 * 3
			*		* * * * *	* 2 * * 2
.14251				* *	2 * ***	2 2
	+				2 * * **	
(0.371					* ** *2	* * * *
40271				*	* * * **	* ***
	•				* * *	* **
_ 04704					2	** * 2 2 3** ** *2
94194				*	* * * *	* *
	•				2 **	* ** *
-1-4932	, ,			*	** * * *	* * * * * * * *
			*		*	2 *
	٠				*	
-2.0384						*
64	1.1700	1.5956	2.0211	2.4467	2.8722	3.7233
	V984 2.8686 2.3234 1.7782 1.2330 .68774 40271 94794	2.8686 + + 2.3234 + + 1.7782 + + 1.2330 + + -68774 + + 40271 + + 94794 + + -1.4932 + + -2.0384 +	V984 2.8686 + + 2.3234 + + 1.7782 + + 1.2330 + + .68774 + + 40271 + + 94794 + + -1.4932 + + -2.0384 + ++	V984 2.8686 + - 1.7782 + - 1.2330 + + - .68774 + + - -40271 + - -94794 + + - -1.4932 + + - -1.4932 + + - -2.0384 +	V984 2.8686	V984 2.8686 * 2.3234 * 1.7782 * 1.2330 * 1.2330 * 1.2331 * 1

178 SUP 5.0000 2.8722

3.2978 4.1489

B-174 3

2.7778 3.6667 4.5556 180 SUP 3.2222 4.1111 5.0000

V98- 2.3686 + 1.7782 + 1.2330 + 2***********************************	SCATTER PLOT	B-175
2.3234 +		
2.3234	2.8686 +	
2.3234	•	
1.7782 + * * * * * * * * * * * * * * * * * *		*
1.7782 +	2.3234 +	*
1.2330 +	+	*
1.2330 +		•
1.2330 +	1.7782 +	
1.2330 +	•	
1.2330		2* * * * * *
+	1.2330 +	* * * *2 2 *
* 2 4 2 3 * 2 * * * * * * * * * * * * * * * *	+	* 2 **** ** * 2*
* * * * * 2 * * * * * * * * * * * * * *	.69774	* 242 3*2 * *
** * * * * * * * * * * * * * * * * * *	•00114	* * * * 2 ** * * *
* * * * * * * * * * * * * * * * * * *	+*	* * * * * * *
+ * * * * * * * * * * * * * * * * * * *	14251	* * * * * * *
+	•14291 +	* * * * * * * * *
40271 +	+	* * ** *
* * * * * * * * * * * * * * * * * * *		
+	40271 +	* * * * * * * * * * *
94794 +	+	* ** **
94794 +		
+	94794 +	** ** 2* ** 2** **
-1.4932 +	+	
-1.4932 +		* ** * *
* * * * ***2* * -2.0384 +	-1.4932 +	* * * * * * * * * * * * * * * * * * * *
-2.0384 +	•	* * * ***2*
-2.0384 +		
	-2.0384 +	
	1.0000	1.8889 2.7778 3.6667 1.4444 2.3333 3.2222 4

7778 3.6667 4.5556 182 SUP 3.2222 4.1111 5.0000

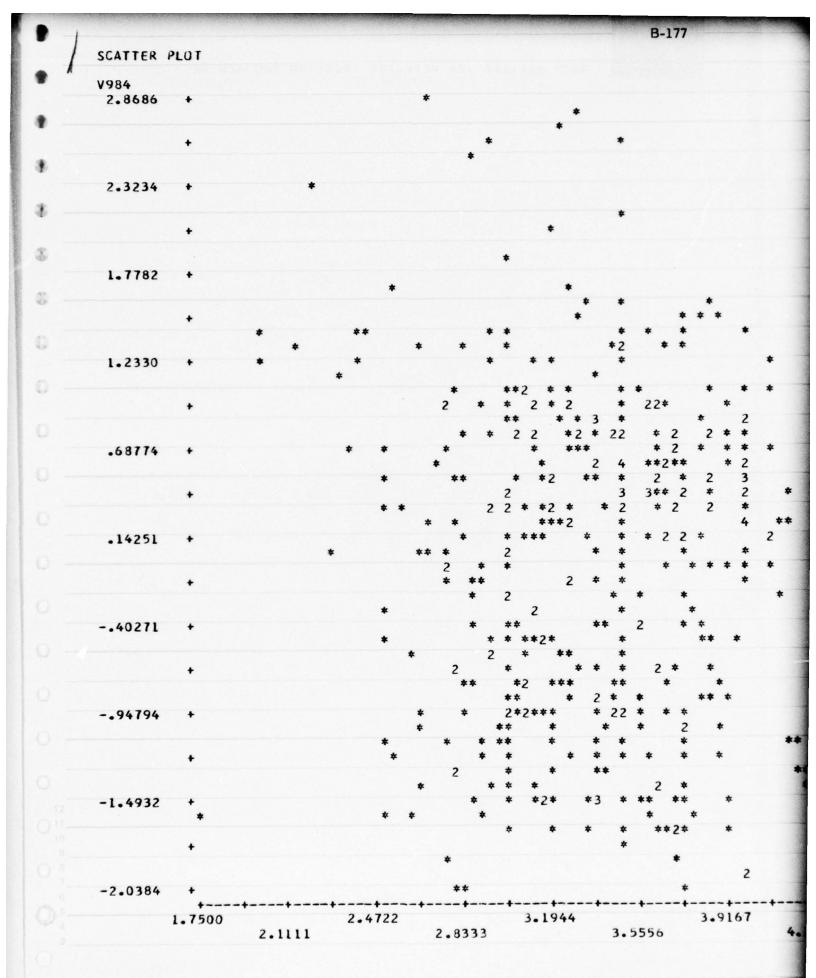
	V984							
	2.8686	•					*	
		+						*
4								*
40	2.3234	•					*	
8 -								
0								
	1.7782	•						
0 -		+					*	* * *
0				*	*	*	*** *	* **
	1.2330	+*					* *	*** *
0 -						*	2 * 2	2 * 3
0						*		* **** * *** 2**;
	-68774	•				*		2 2
		•	*			*	*	
							* 2* 2* ** *	* ** 22 2 2 2 * * 222 2 2 2
	.14251	•				*	** ****	2 2 2
		•					* * **	
							* *	2 *
	40271	+				*		* * *
							* 2 *	** **
							*	**** 2
	94794	•						3* *2 3
						* *		2 * *2
						**	* *	* *
	-1.4932	•				*	* *	* 22* 2 **
						*	*	2 2 *
							*	*
	-2.0384	+	++		.+	*	+	*
		1.0000	1.4444	1.8889	2.3333	2.7778		3.6667
			10777		2.3333		3.2222	

```
2 2 * 222 3 2* 2 2 3 ** * 2 2
```

3.6667

2.7778

4.5556 184 PEER 5.0000



2 2 186 PEER 5.0000 3.9167 3.1944 333 3.5556 4.2778

2.7778 3.6667 4.5556 188 PEER 3.2222 4.1111 5.0000

2.3333

2.7778 3.6667 4.5556 190 PEER 3.2222 4.1111 5.0000

** *

2.7067 3.5600 3.1333

3.9867

.4133 196 HUM. 4.8400

2.8686 + 2.3234 + 1.7782 1.2330 .68774 .14251 -.40271 -.94794 -1.4932 -2.0384 3.5967 2.1656 1.4500 2.8811 3.2389 1.8078 2.5233

SCATTER PLOT

V984

2.8811 3.5967 4.3122 197 COMM 3.2389 3.9544 4.6700 . .

* * * * * * * 2 * * * * * * * * * * 3 * 2 * * *** 2 * 3 * *

* * 2 * **3 ** * ** ** * 3**** 2 * 2* * 2 ** 2 *

* * * * * * *

* * *

3.1500 3.8900 4.6300 198 MOTI 3.5200 4.2600 5.0000

1.8889

2.3333

2.77/8

3.6667

-2.0384

1.0000

1.4444

2.7778

3.6667 3.2222 4.1111

199 DEC. 5.0000 4.5556

)	-			
	SCATTER	PLOT		B-184
	JOHITER	FLUT		
)	V984			
	2.8686	+		*
D				*
				* *
_				*
	2.3234	•		*
		+		*
*				
	1.7782	+		
*				•
4				* * *
		+		* * * * * * *
10				
	1.2330	•		* * * * 2
0				*
40				* ** 2*2** *
		+		* * * * * * * * * * * * * * * * * * * *
				* ** * ** 2 * * *** ** 2 *2***
	.68774	+		* * 2 2 *2 **
				* * * 2 * 2 2 *
				** *** 2 2 * *2
		+*		* * * * * * * * * * * * * * * * * * * *
				* * 2 2 ** * *2** * * * * * * * * * * *
	.14251	+		* * * **2 * ** 2 * 1
				* * * ** *
				* * * 2* * *
		+		* * **
				* * * 2
	40271	+		* * *** * *
				3 * ** * 3* *
				* *** *
		+		2* * 2 2
				* 2 * * * * * * * * * * * * * * * * * *
	94794	+		* * *** *24 * ** 2*
	• > 71 > 7			* 2 ** * *
				* * * * * * *
		+		2 * * *
				** * *
	-1.4932	+		* * * * * * * * * * * * * * * * * * * *
	1.4732			* * * * * *
				* * * *** * 2 *
		+		
				*
	2 020/			
	-2.0384	++	+	* * *
		1.5700	2.3011	3.0322 3.7633
		1.935	6	2.6667 3.3978 4.

4.1289

3.3978

SCATTER PLOT				B-	185
V985					
2.6545 +					* *
			*	*	
2.1781 +			*	•	
+					
1.7017 +					
+					*
1.2254 +					
			*		•
•					
.74898 +				*	* ***
+				* * *	* 3 * ** * **
		*	*	* 2**	* * * *
-27261 +		*	*		* * * * *
+			*	*	2 ** *
			*	* *	2* * 2 2
20376 +				*	* * **
•					* * 2 * ***2 *
		*	*	* *	* * **
68014 +*				*	* * *
•	*			* * 2	** 2*
				*	3 * *
-1.1565 +			*		* **
•					
-1.6329 +					*
+	-++	+	++-	++	++
1.0000	1.4444	1.8889	2.3333	2.7778	3.6667

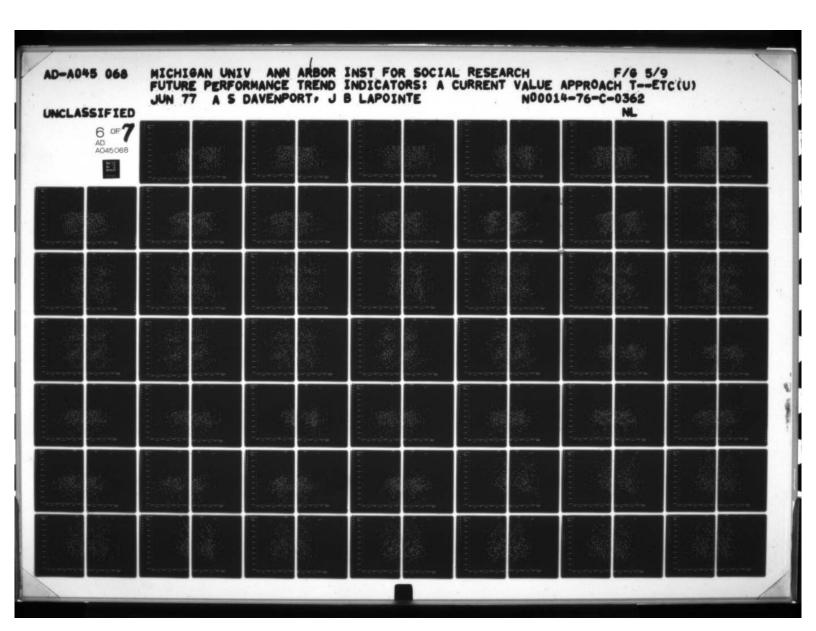
* ---+---+---+----+ 3.6667 4.5556 176 SU

3.2222

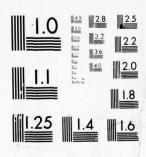
7778

4.1111

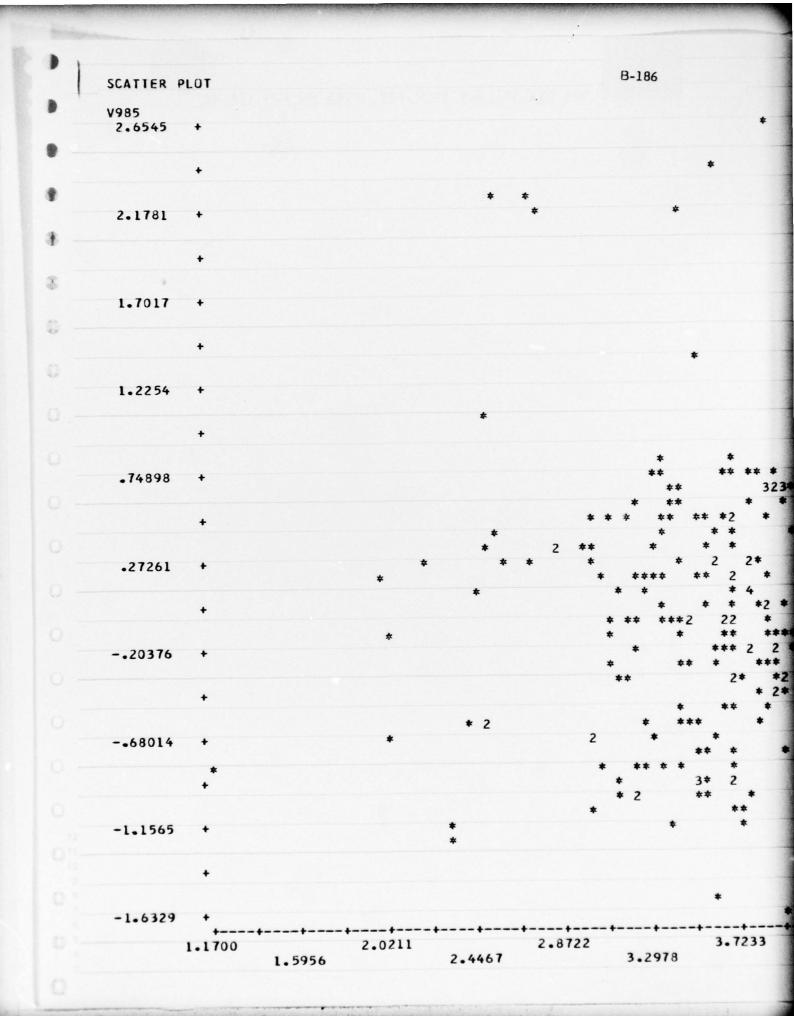
176 SUP 5.0000



6 OF AD A045068



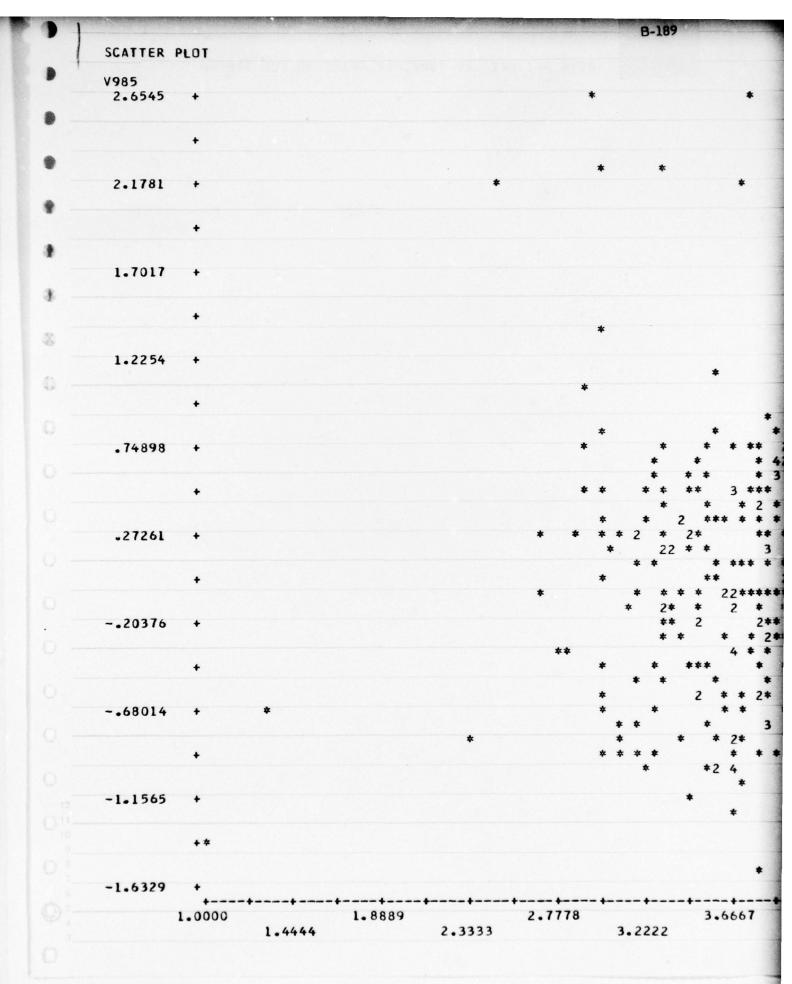
MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-7



178 SUP 5.0000 3.7233 2.8722 4.5744

4.1489 3.2978

3.2222 4.1111



184 PEER 5.0000 4.5556 2.7778 3.6667

3.2222 4.1111

*

*

* * * * * * * 2* 3 ** * *** * * * * 2 * * 2 2 * 2 * * * * * * * * * * * * 2 22 3

* * * 2*2* * * 2*2* ** 2** * * 2 * * * 2 ** ** 2 * *

2 ** 2 * **2* ** * * ** 2 ** * * * * 3 ** * * 2 *

* *

3.0556 3.8333

4.2222

4.6111 186 PEER 5.0000

```
B-191
                                                        188 PEER
5.0000
2.7778
                       3.6667
                                  4.1111
           3.2222
```

1	,						9.1	
	SCATTER F	PLOT					B-1	92
)	V985							
	2.6545	+			*		*	*
D								
		+					*	*
9				*	*			
	2.1781	•		*		*		
8								
		+						
*	1.7017	+						
8 -	1.7517						*	
0							*	
45	1.2254	+						
0 -							*	
		+						
						*	2	**
	.74898	+				*	****	* 4 2 ** *
					* * 2	* 2 2*	2 **:	* * *
		+			* * *	* 3 * *	2 * *2	2 * * * * * * * * * * * * * * * * * * *
					* 2	* *	* *	** **
	-27261	+		* *	* * *	**	** 2** * 3 *2 * 2	** * *
					*	* *	* ***	2* *
		+			*	* * * * 2 **	** * *2 * 3 *	# 2 # #
				*				2** *
	20376	+			*	* * * 2	** **	* *
					* *	** **	2 2 *	2* * *
						*	* **	*
	68014	+*			*	* * *	3 * 2	2 **
					*	*		3 * *
		+		*	* 2		** *	**
					*	* 2 *	**	2 *
	-1.1565	+					* **	
					*	*	*	
		+	*					
							*	
	-1.6329	+				+	_4	*
0 %		1.0000	+	1.8889		2.7778	-,,	3.6667
3			1.4444		2.3333		3.2222	

•	SCATTER	PLOT						3-193	
	V985								
	2.6545	•					*	*	
		•				*	*		
1	2.1781				* *	*			
3	201101								
8		•							
40	1.7017	+							
-		+							
0									*
0	1.2254	. •						*	
		+					*		*
	.74898	+				*	*	* *	*2 2 *
							*2**		3****
		+		*			2 2 ** * * * *	2 * *	
	•27261	+			* 2	*2 **	2	2 3	*
					*	2	* ** **	* *** 2* *	
					*	* 3 *	* ** * **2 *		* *2
	20376					* *			2 **
		+					*	* * *	****
	68014	٠		* *	*	* *	* *	*	* * *
		+	*			* * * *	* * * *2	2 2	* * 2 *
				*	*	* **		* *	*
		•				* *	* *	*	*
		+		*					
	-1.6329						*		
	5	1.0000	+	1.8533	+	2.7067	++-	3.5	600
			1.4267		2.2800		3.133	3	

2.9089 3.6133 4.3178 197 COMM 3.2611 3.9656 4.6700

1			
SCATTER	PLOT		B-195
V985			
2.6545	+		* *
			•
	•		•
2.1781	+		**
	+		
1.7017	+	*	
		*	
	+		
1.2254	+		*
			*
	+		•
			* * *
.74898	+		* * * * * 3 *2 * * * *2 2 2**2* 2 *
			* *2 * 2 * ** * 2*
	+	*	** 2 2*
		*	2 2 * * * 3 3 * *
.27261	+	* *	* * * * * * * * * * * * * * * * * * * *
		•	* 2 * 2 2 * * * *
	+	*	* ** ** * 2 * * * * * * * * * * * * * *
			** * *2 * ** 3 * *
20376	+		* * 4 * 3 * * * * * * * * * * * * * * *
			* * ** ** 2* *
	+		* * 2 * *** *
	*		* * * * 2 * 2 * 2
68014	+	*	* * * 3 2 * *
		*	* 2 * ** **
	+		**
			2 * * 2 * * * * * * * * * * * * * * * *
-1.1565	+	*	* * * *
	+		
			*
-1.6329	٠	*	
	1.8400	0 2.5422	3.2444 3.9467
		2.1911	2.8933 3.5956

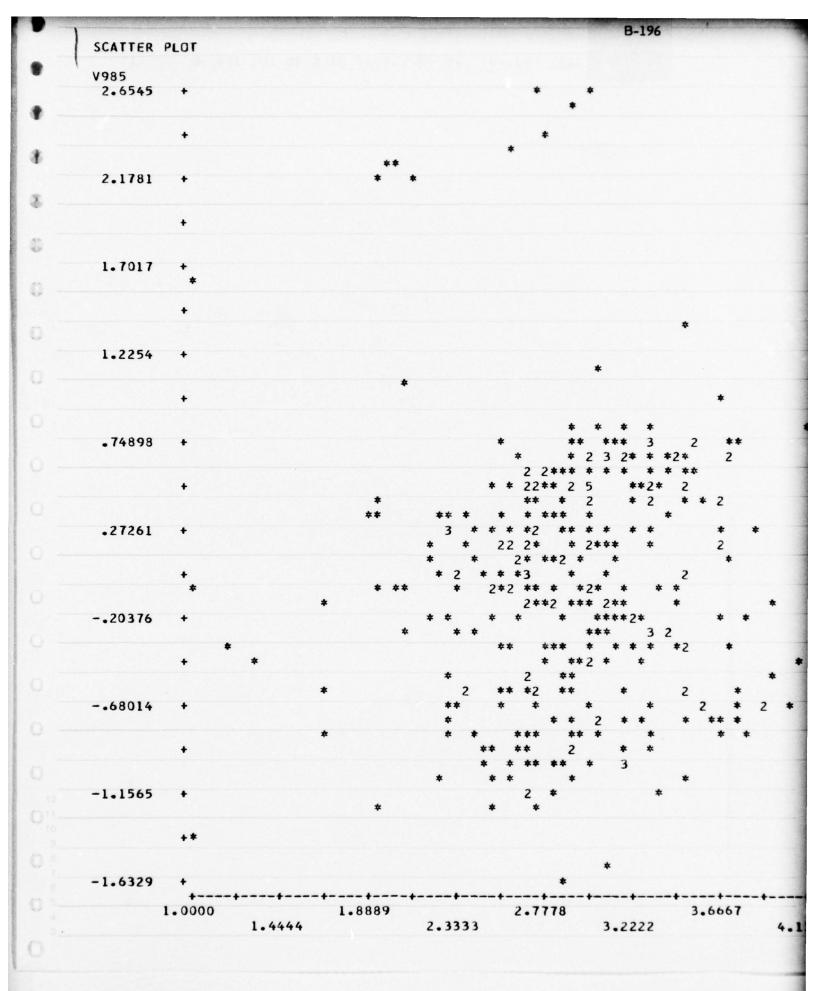
Ö

2

933

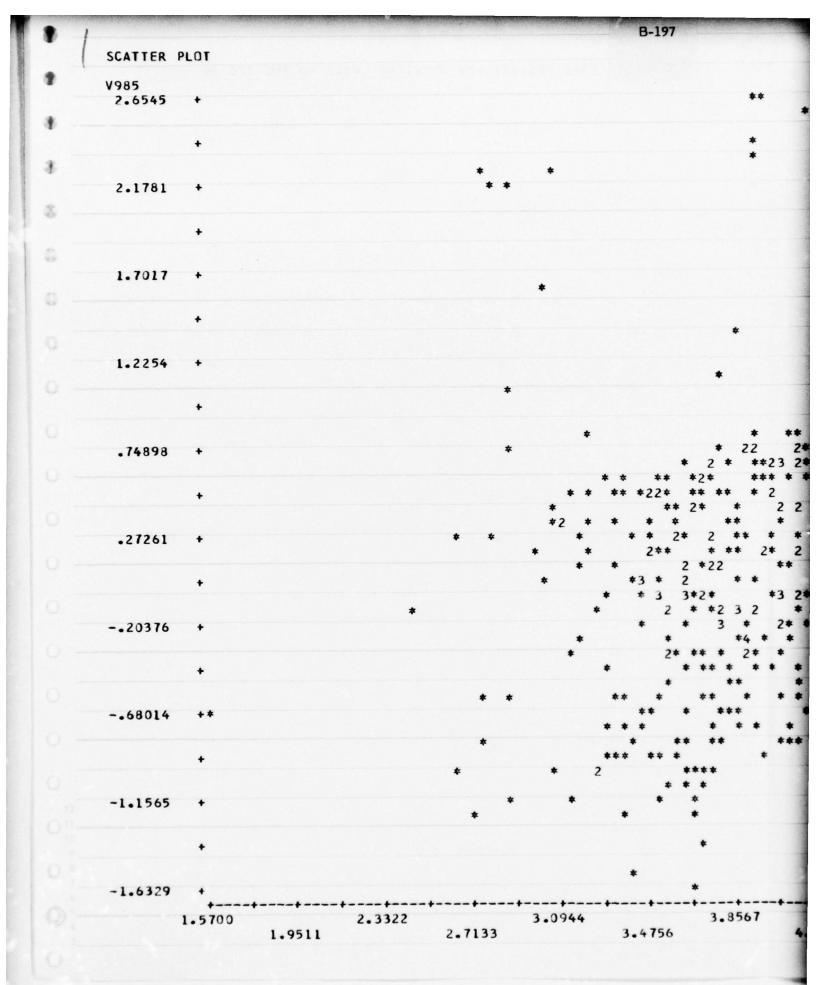
198 MOTI 5.0000

3.5956 4.2978

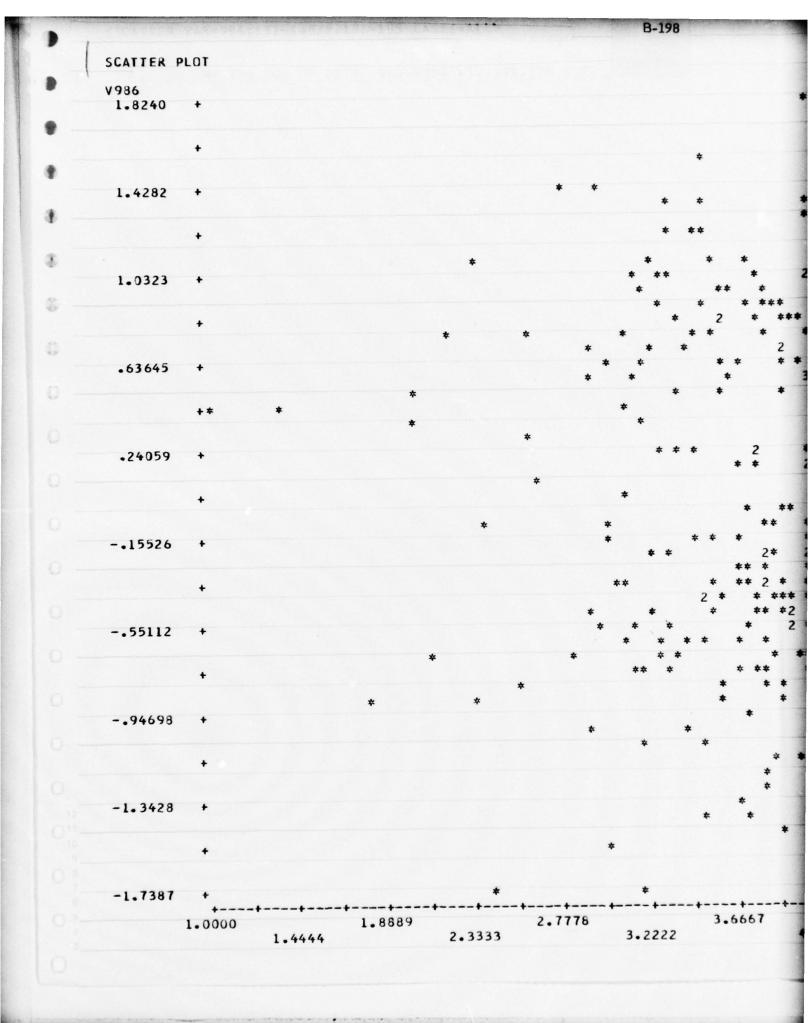


3.6667

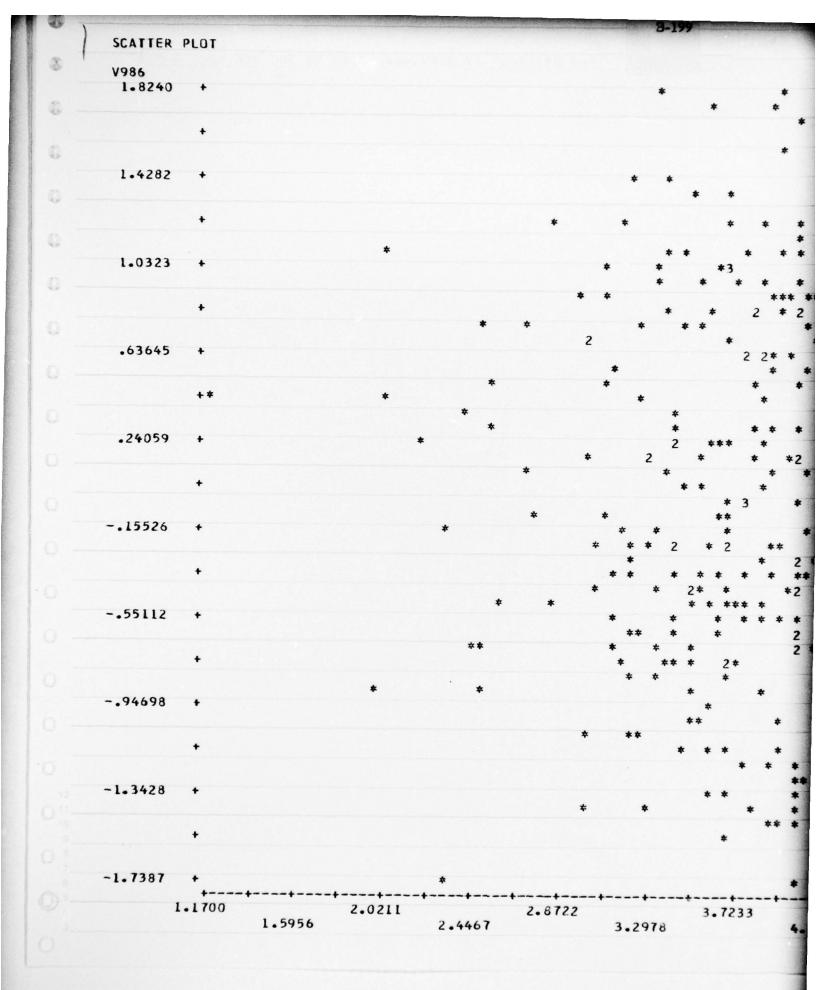
4.5556 199 DEC. 5.0000 2.7778 3.2222 4.1111

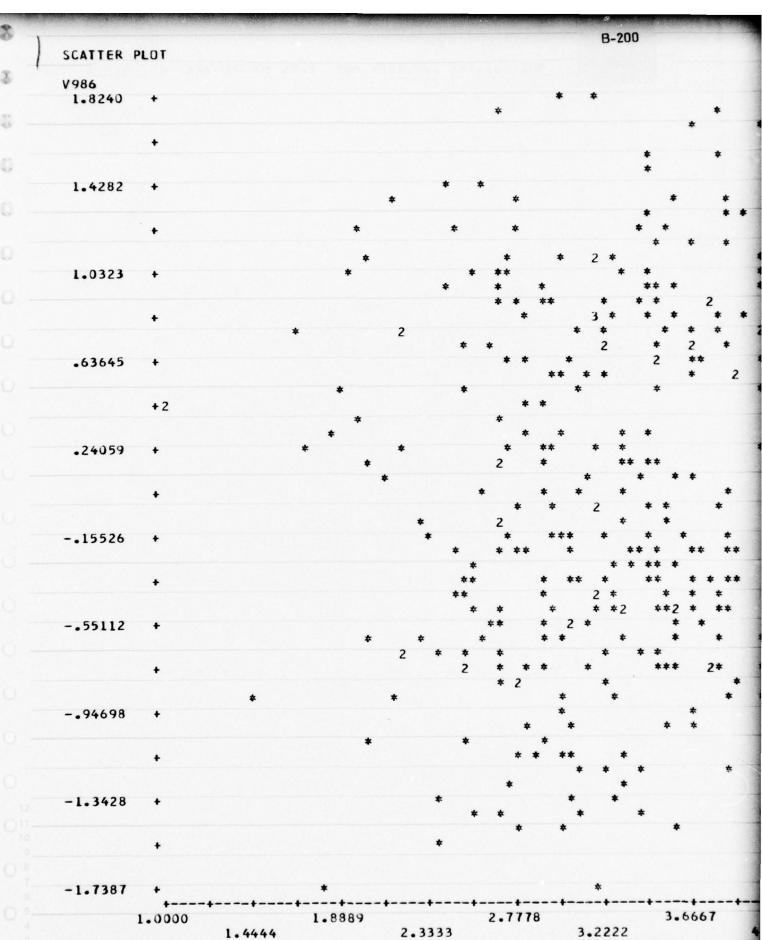


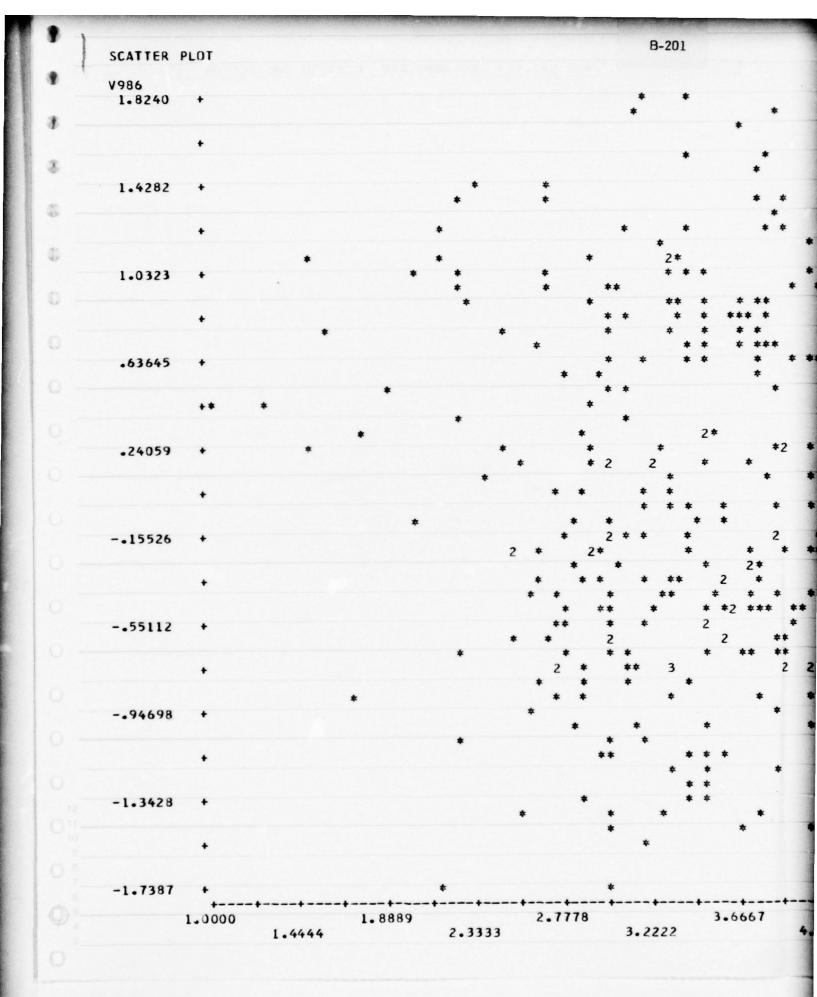
200 SATI 5.0000 3.8567 4.2378 3.4756



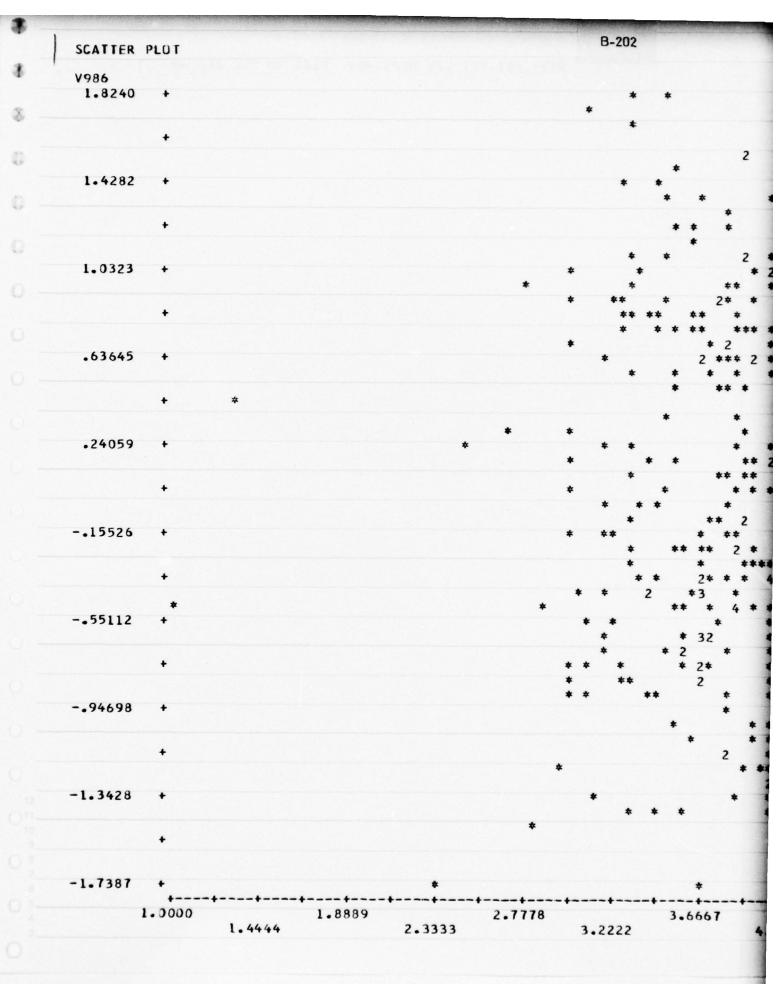
2.7778 176 SUP 5.0000 3.2222 4.1111







7778 3.6667 4.5556 182 SUP 3.2222 4.1111 5.0000



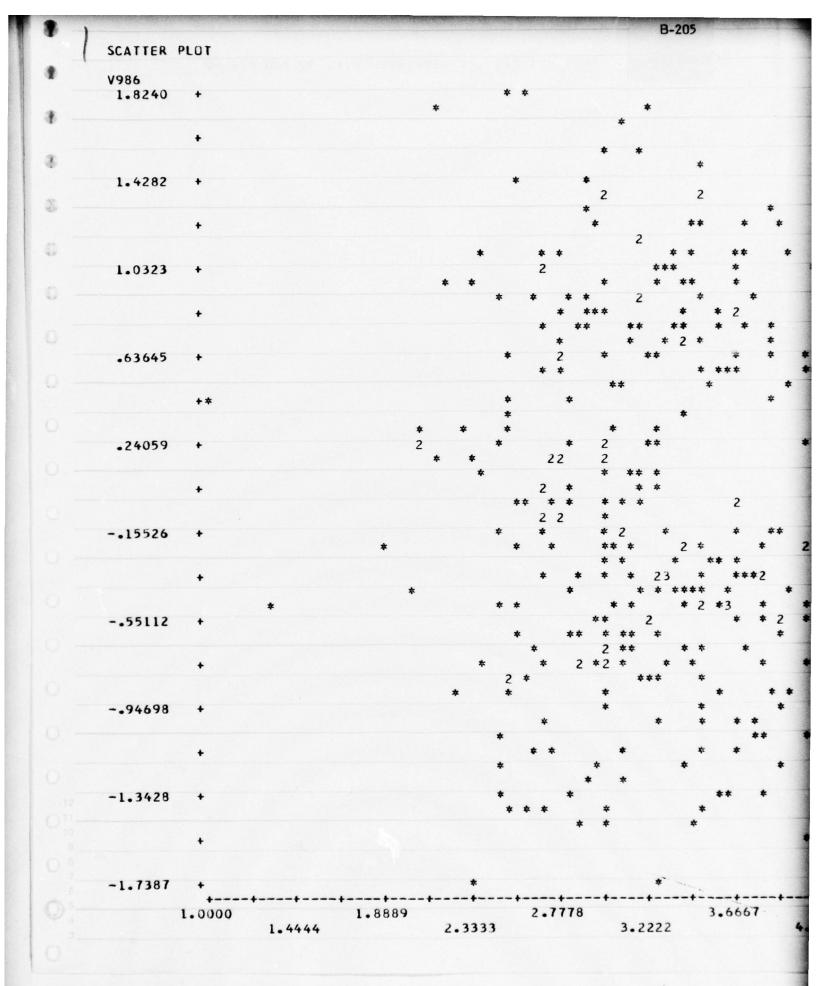
-+--7778 4.1111 3.2222

3.0556 3.8333 4.6111 186 PEER 3.4444 4.2222 5.0000

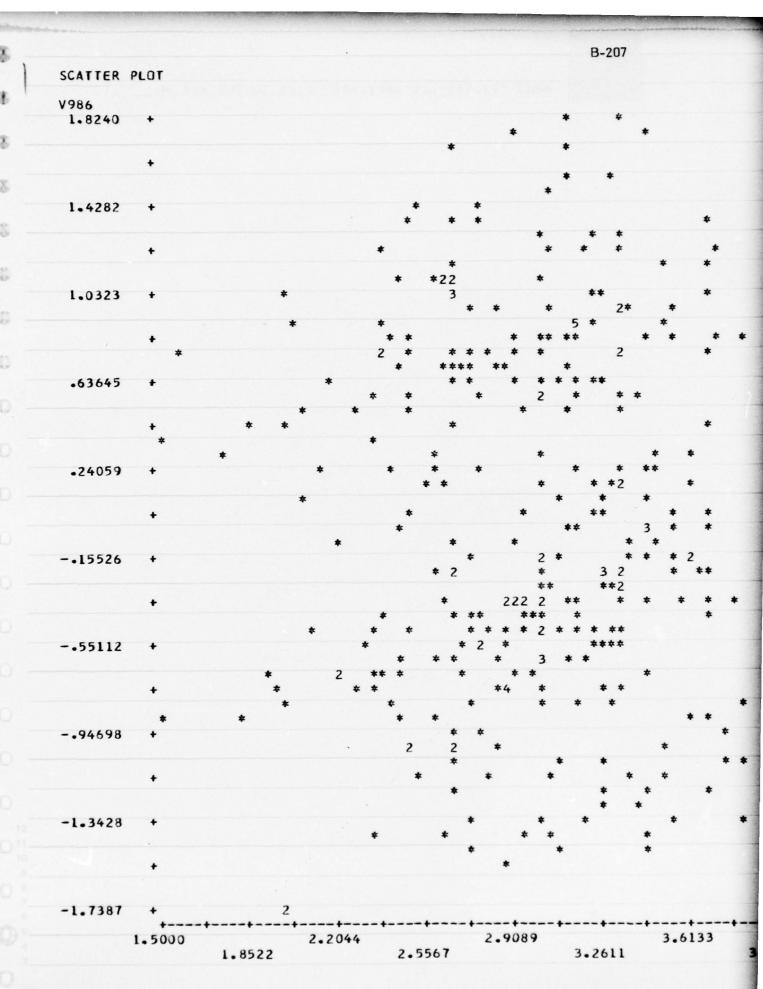
1						B-	204	
SCATTER	PLOT							
V986								
1.8240	+				**			
				*		*		
	+					*		
						2		
							*	
1.4282	+			*	*	*	*	
						*	*	*
	+					* 2	**	
				* *	*	*	* *	
1.0323	+				*	*	* 3 *	*
						** *	*** *	
	+				* *	* **	*** * 2	
					* *	2 ** *	2 *	
.63645	+				* * *	* *	** * *	*
.03047					*	2	* * *	k
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	+*			* :	*		*	
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.24059	+			* *		2 * *	*	-
				*	* *	2 2 *		
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15526	+				* 2		** *	*
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	+					* *** *	* * *	* 2
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55113	*				*	** 2	**2** *	
55112	•		*		* ** 2	* *	* 2 * *	
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	+				* * 3		* 2 *	
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94698	+					*	* *	*
					*		* 2 2*	*
	+				* *		* **	
				*	*		**	
-1.3428	+					* *		*
1.5420				*		2 **		
						*	* *	١.
	+							*
-1.7387	+				*	*		
	1.0000		1.8889	·	2.7778	-+	3.6667	
		1.4444		2.3333		3.2222		4.

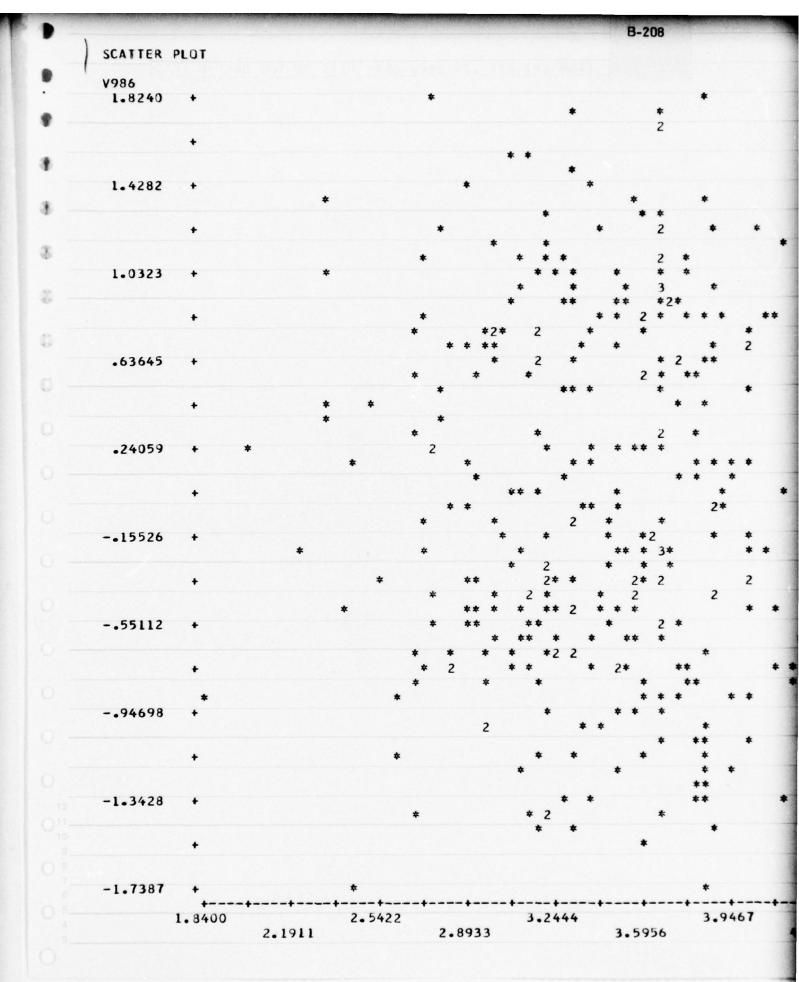
6.9

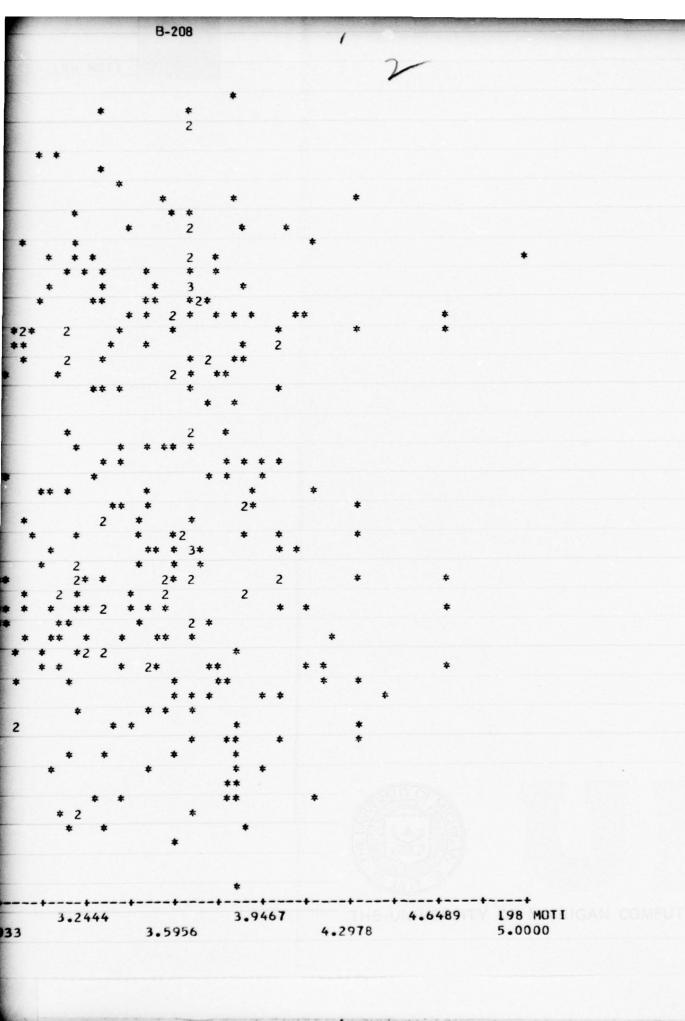
2.7778 3.6667 4.5556 188 PEER 3.2222 4.1111 5.0000

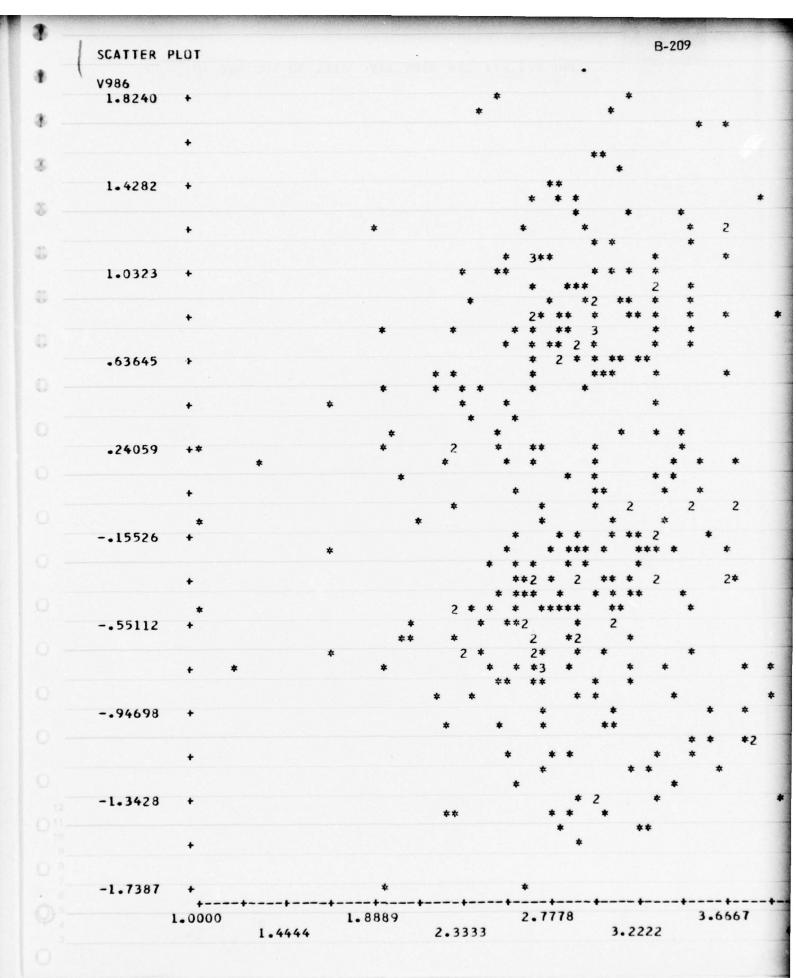


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196 HUM.
4.8400
                        3.5600
                                                4.4133
2.7067
                                    3.9867
            3.1333
```

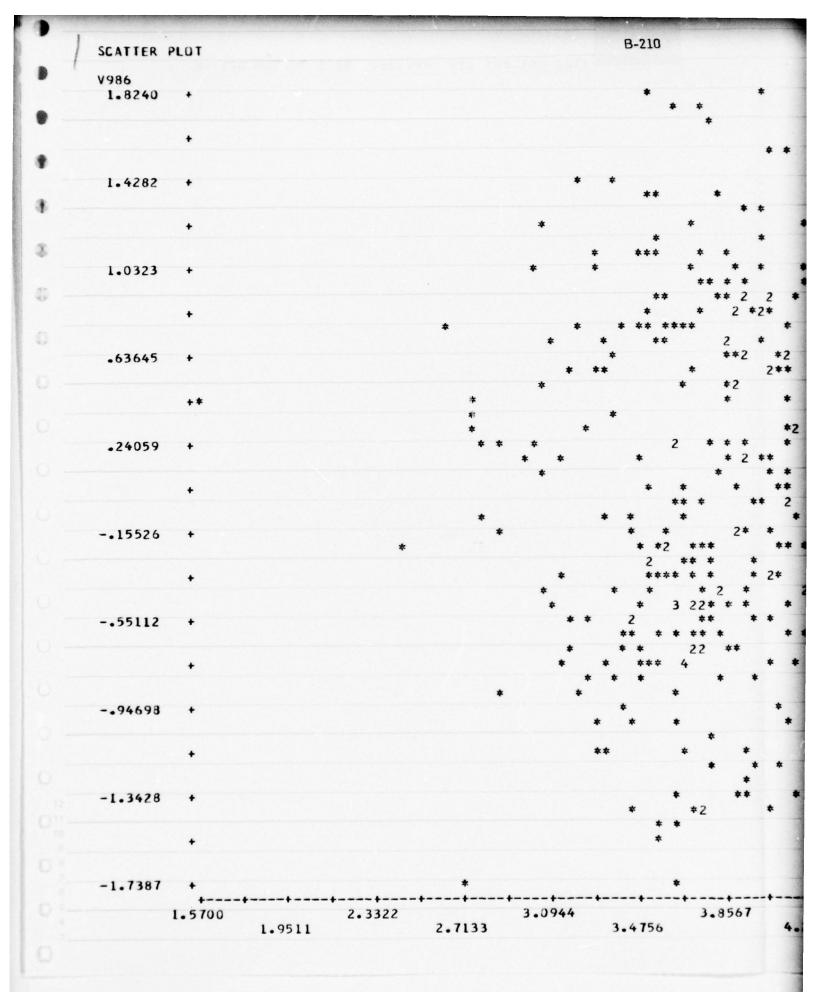








2.7778 3.6667 4.5556 199 DEC. 3.2222 4.1111 5.0000



SCATTER	PLOT					В	-211
V987							
2.5678	+						
	+						
2 1007							
2.1097	•						
	•						
1.6516	+						
	+						
							*
1.1936	+						
1.1730							2
	+						*
						*	
.73550	+						* * *
						*	* ****
	+					* * * *	* * ** *
					*	**	* ** * *
-27744	+					*	3 * 2 *
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18063			*	*		* * * **	* * **
			*			*	* ** *2*
		*				2	* * * 2
		*					
63869	+					* *	*
							*
	+						*
							* *
1 2043	+						*
-1.0968							*
	+						*
							* *
-1.5548	+						
	1.0000	-+	1.8889	+	2.7778		3.6667
	1.0000	1.4444		2.3333		3.2222	

2 2.7778 3.6667 3.2222

4.1111

176 SUP 5.0000

SCATTER PLOT			B-212
V987			
2.5678 +			
+			
2.1097 +			
+			
1 4514			
1.6516 +			
+			*
1.1936 +			*
			* * *
+			*
.73550 +			* * * *
		*	* * * 2 *
+			* 2 * 2 * * * * * * * * * * * * * * * *
.27744 +		* *	* * ** *2 * ** * * *2 3 *
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18063 +	*	* *	* * * * * ***
•	*	*	** *** 2 ** *
*			**
63869 +		*	* * * *
•			
			* *
-1.0968 +			* * **
•			* **
			* *
-1.5548 +	-+++-	+++	++++-
1.1700	2.0211	2.872	3.2978

178 SUP 5.0000

4.5744

.8722 3.2978

3.7233

•	1								B	-213	
	SCATTER	PLOT									
9	V987										
	2.5678	•							*		
0											
	2.1097	+									
		+									
3	1.6516										
3	1.0010	•									
		+									
3						*					
	1.1936	+				*			*	*	
0		+									
0						*		*			*
	.73550	+						* :	*	*	*
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	277//				** *		* 2 *	**	*2 *	2 *	* 2 2*
	•27744				** *	**	2 2	3*		**	
		+				**	2 2		*2* **	1.	* * 2
			*	*	*	* **	*	*	2**	*22 * 2*	2*
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		*		•		*	2	*	*	2	*
	63869	•					22		*	*	*
										*	*
		+				*			*	*	*
	-1.0968					*	*		*	*	*
		•					*				
		+					*	*	*		
						*		*			*
	-1.5548	+	++	++	+	++	+	*	+	-+	-++
		1.0000	1.4444	1.8889	2.2	333	2.7778	3	.2222	3.	6667
			1.4444		2.3	333		,			

4.1111 3.2222

```
SCATTER PLOT
 V987
 2.5678 +
  2.1097 +
  1.6516 +
  1.1936
  .73550
  .27744 +*
 -.18063
-.63869
-1.0968 +
-1.5548
                     1.8889 2.7778
       1.0000
              1.4444
                                                     3.6667
                             2.3333
                                             3.2222
```

4.1111

3.2222

184 PEER 5.0000

* *** -1.5548 + * 2.0000 2.6667 3.333 4.0000 2.3333 3.0000 3.6667

3333 4.0000 4.6667 186 PEER 3.6667 4.3333 5.0000

1.8889 2.7778 2.3333

3.6667

3.2222

-1.5548

1.0000

```
188 PEER
5.0000
778
                     3.6667
                                 4.1111
        3.2222
```

```
2
                                2
                                         4.5556 190 PEER
5.0000
2.7778
                     3.6667
                               4.1111
          3.2222
```

SCATTER PLOT				В-	219	
V987						
2.5678 +			+			
•						
2.1097 +						
1.6516 +						
100310						
+						
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1 1024					*	
1.1936 +				* *	*	
					*	•
+					*	
				*		
.73550 +			*	* 2	****	
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+			* * *	** ** 22 3* 22 *	* * * 2 *	
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.27744 +		*	* * * * 2 *	** **	* * *	2
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18063 +		*	* 2*	* *	*2 2 * **	* *
	*		***	* *	2 ***	
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			*		** * *	*
63869 +			** *	*	*	
			*	* *		
•				*		*
			* *	*	*	**
-1.0968 +					*	*
				*	*	*
						*
			*	*	* *	
-1.5548 +				*		
1.3400		2.1178	2.8956	+	3.67	733
1.3400	1.7289	2.1110	2.5067	3.2844	3.01	33

3.2844

4.0622

196 HUM. 4.8400 9

SCATTER	PLOT			B-220)
V987					
2.5678	+		*		
	+				
2.1097	+				
	•				
1.6516	•				
	•				
			*		
1,1936	+		*		
			*	*	*
	+			*	
				*	* 2
.73550			* *	* *	* *
	+		* 2 **	** 3	* *
			** * * 3* * * * * * * * * * * * * * * *		*
-27744	+	*	* 2 2 2*	*2 2 * **	* *
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	•	* * *	* * * *	* * ** ** *2 2 * *	2 2
100/0	*		* * * *		*2* *
18063	*		* * * * * * * * * * * * * * * * * * *	* * * *	* * *
	+	* *	* * * ****	*	2 2 * *
		* *		* * * *	2 *
63869	+		* ** *	*	
			4	* *	
	•		*	* *	
-1.0968	+		**	*	
1.0700			*		*
	+		*	* *	*
			*	*	*
-1.5548	+		*		+
	1.5000	2.2044	2.9	9089	3.6133
	1	.8522	2.5567	3.2611	

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2.9089 3.6133 4.3178 197 CCMM 3.2611 3.9656 4.6700

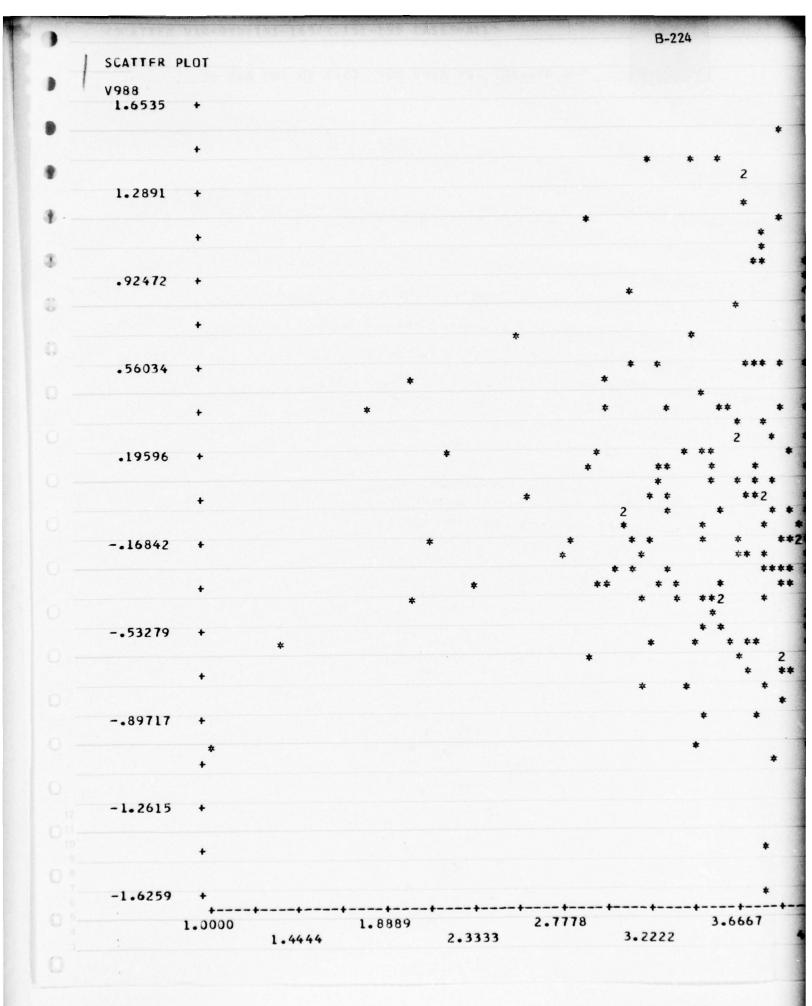
198 MOTI 5.0000 4.0733 3.4556 4.3822 3.7644

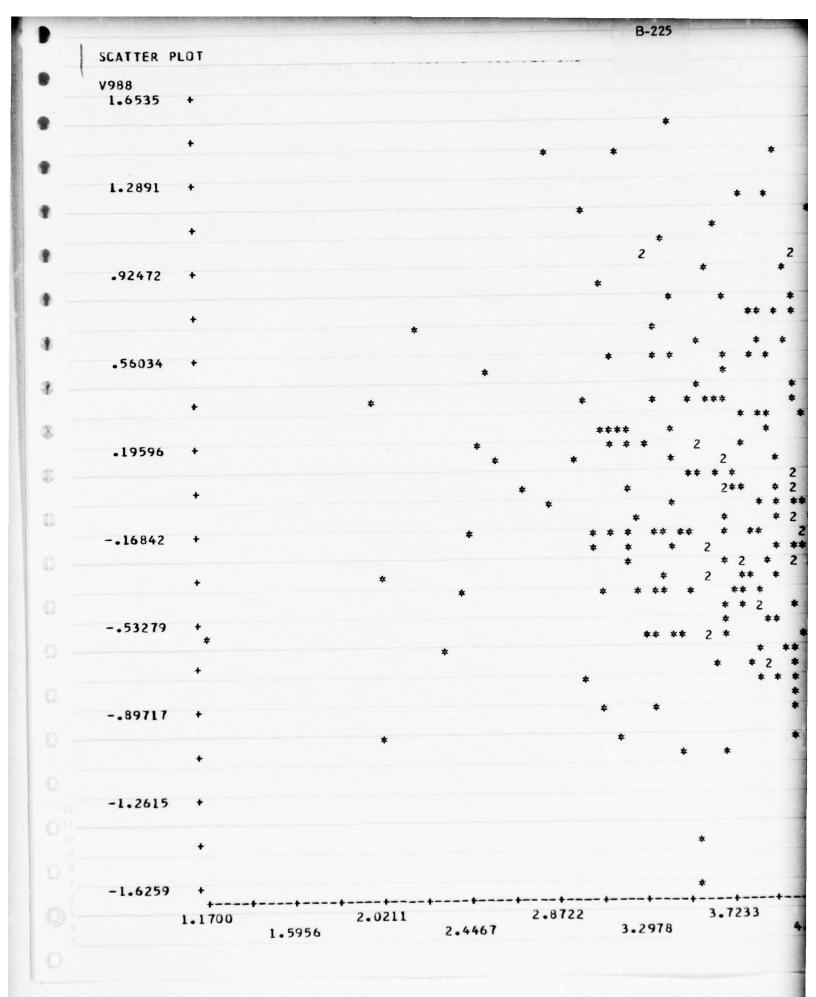
```
SCATTER PLOT
V987
 2.5678 +
 2.1097
 1.6516
  1.1936
                                                                 * 2
  .73550
  .27744
 -.18063
 -.63869
-1.0968
-1.5548
                                                                 3.6667
                                              2.7778
                            1.8889
         1.0000
                                                        3.2222
                 1.4444
                                    2.3333
```

2.7778 3.6667 4.5556 199 DEC. 3.2222 4.1111 5.0000 3

| B-223 | | | | |
|----------------------------------|--------|--------|--------|---------|
| | | | PLOT | SCATTER |
| | | | | V987 |
| • | | | • | 2.5678 |
| | | | | |
| | | | • | |
| | | | + | 2.1097 |
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| | | | | 1 4514 |
| | | | • | 1.6516 |
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| * | | | | |
| * * | | | + | 1.1936 |
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| * 2 | * | | + | .27744 |
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| * * * *** 2** | | | + | |
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* * * * * * 3* | * | | | 18063 |
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| * ** 2 | | | + | 63869 |
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| | + | | + | ~1.5548 |
| 3.0944 3.4756 | 2.7133 | 2.3322 | 1.5700 | |

200 SATI 5.0000 3.8567 4.2378 3.4756





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1.8889

1.4444

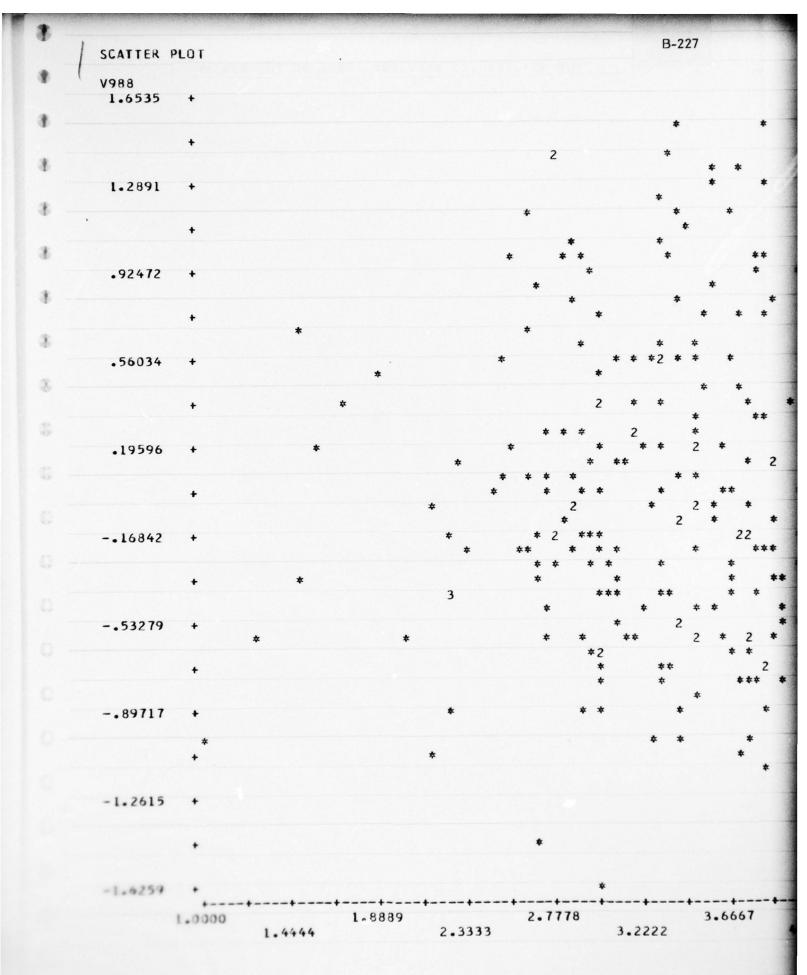
2.3333

3.6667

3.2222

2.7778

-1.6259

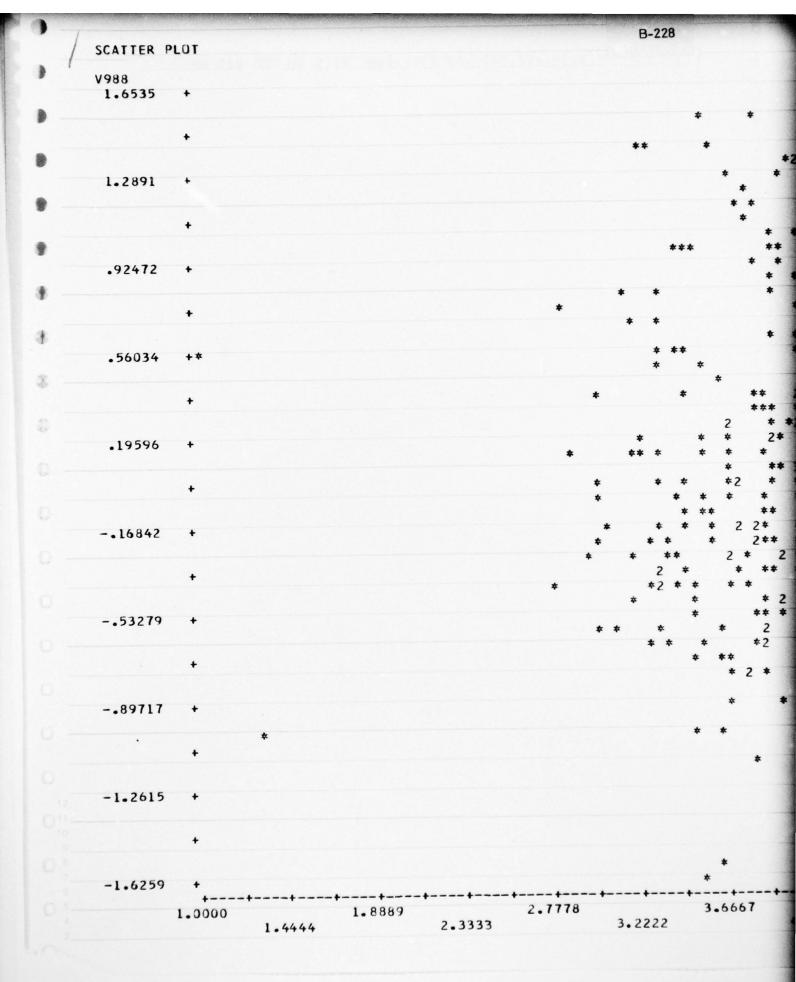


3.6667

4.1111

3.2222

4.5556



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2

4.5556 2.7778 3.6667

184 PEER 5.0000 4.1111 3.2222

3

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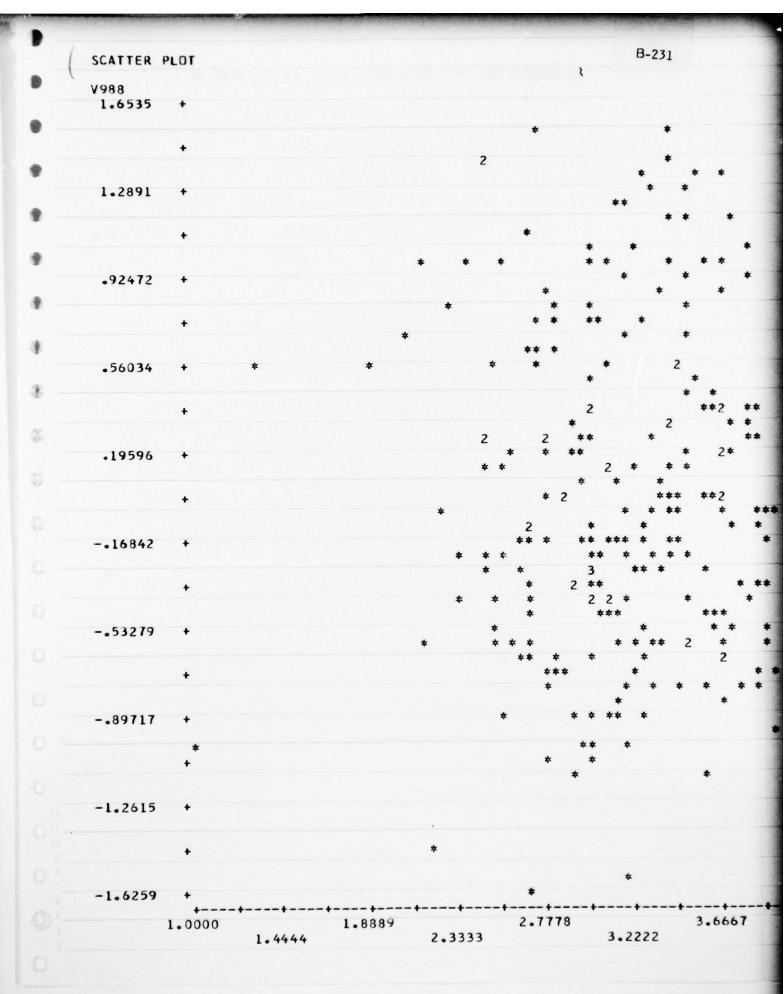
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| SCATTER | PLOT | | | | | | B-230 | | |
|----------------|--------|--------|--------|--------|-------|-------------|-----------|------------------|------|
| | | | | | | | | | |
| V988
1.6535 | + | | | | | | | | |
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| 1.2891 | • | | | | | * | 2 ** | | |
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| 89717 | + | | | | | 3* | * | * | |
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| -1.2615 | • | | | | | | | | |
| | • | | | | | * | | | |
| | | | | | | | | | |
| -1.6259 | + | + | + | tt | ++- | + | * | + | + |
| | 1.0000 | 1.4444 | 1.8889 | 2.3333 | 2.777 | | | 3.6667 | |

2.7778 3.6667 4.5556 188 PEER 5.0000



190 PEER 5.0000 3.2222 4.1111

SCATTER PLOT V988 1.6535 + 1.2891 .92472 .56034 .19596 -.16842 -.53279 -.89717 -1.2615 -1.6259 1.3400 2.1178 2.8956 3.6733

2.5067

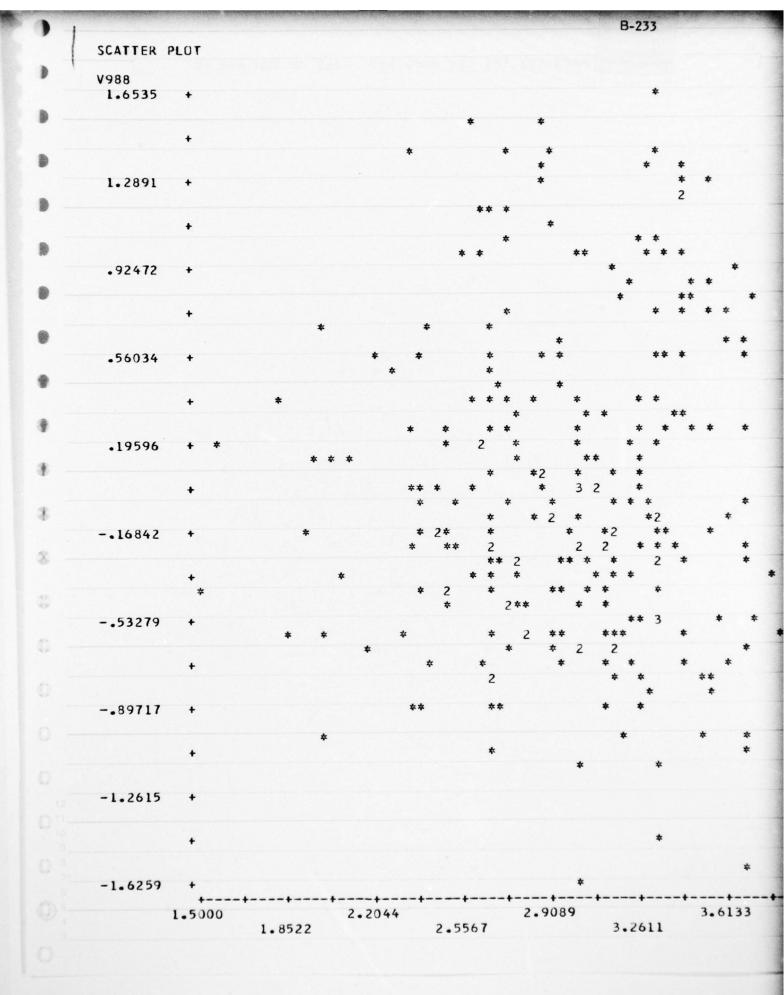
3.2844

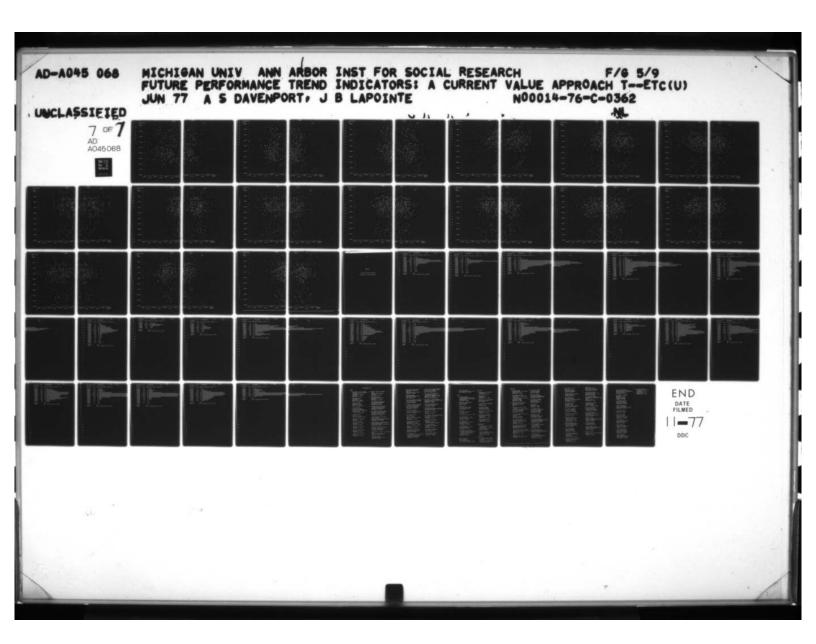
1.7289

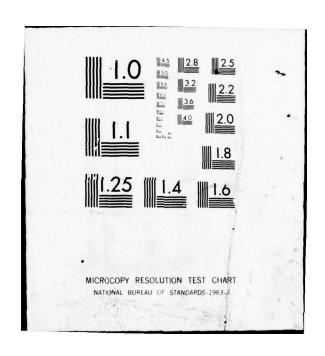
3

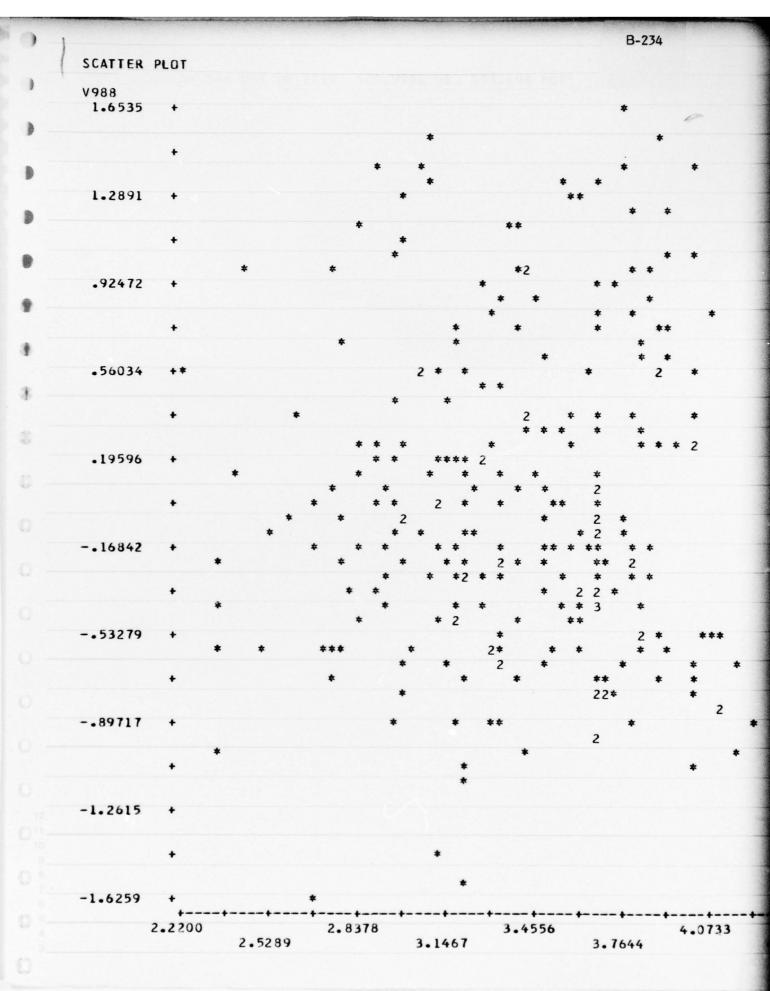
8

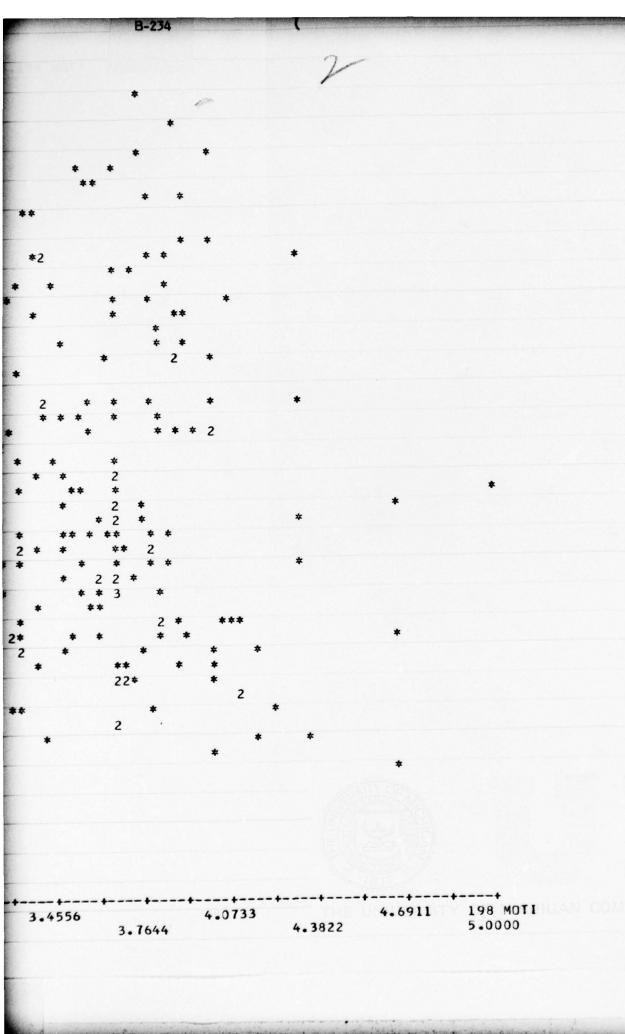
3.2844 3.6733 4.4511 196 HUM. 3.2844 4.0622 4.8400

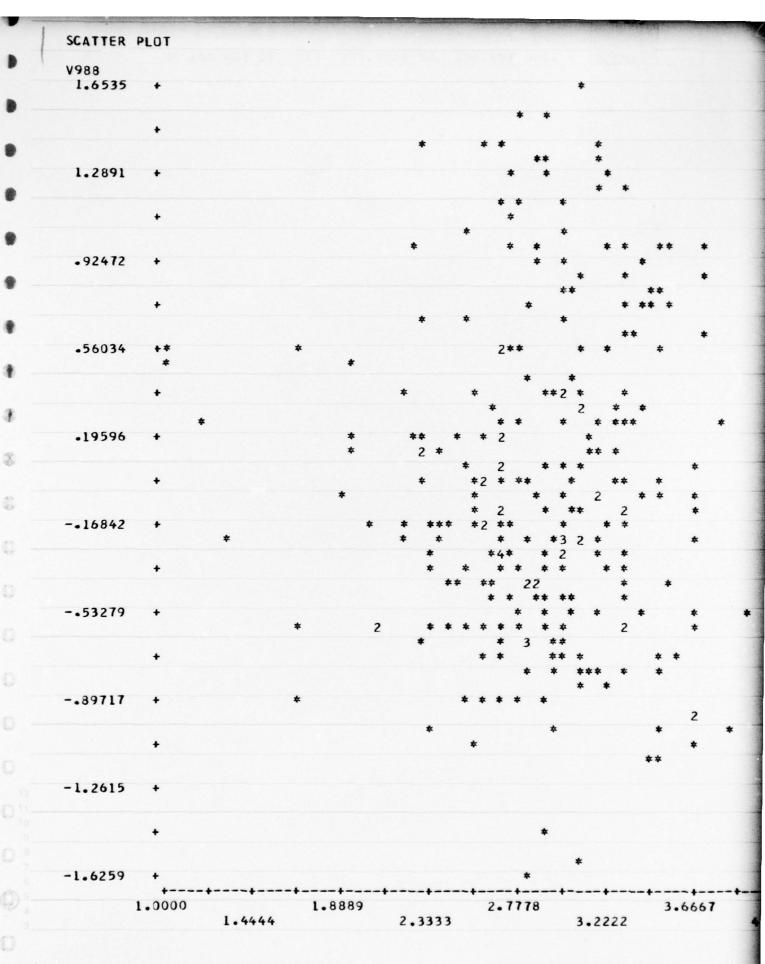


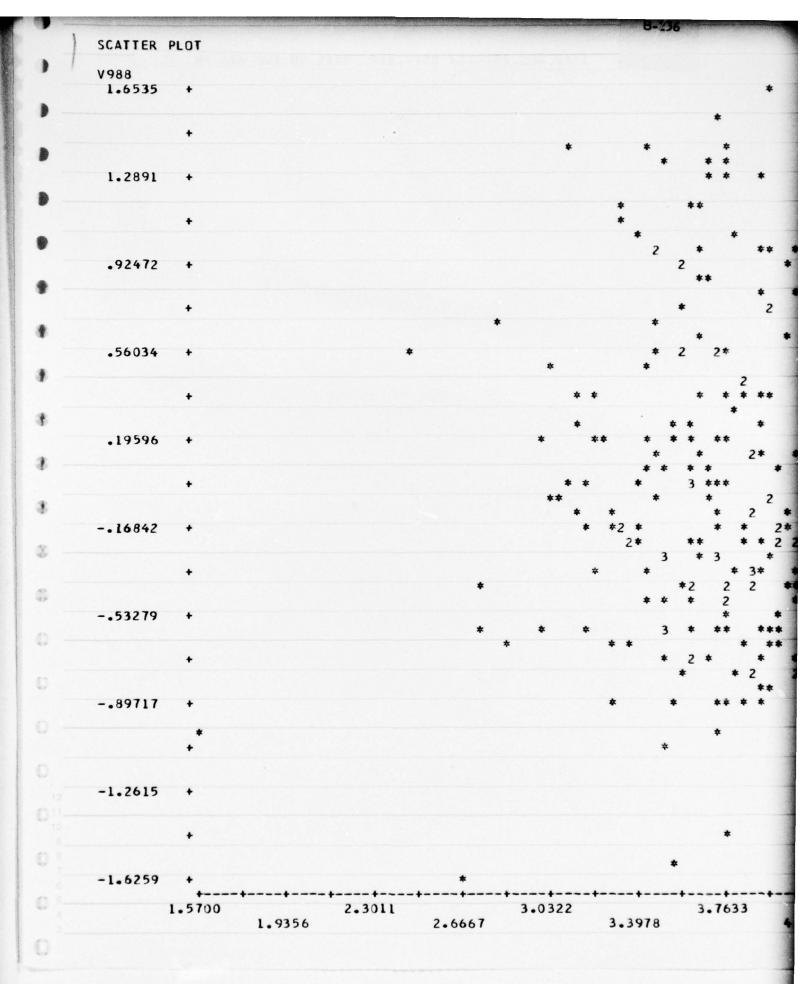




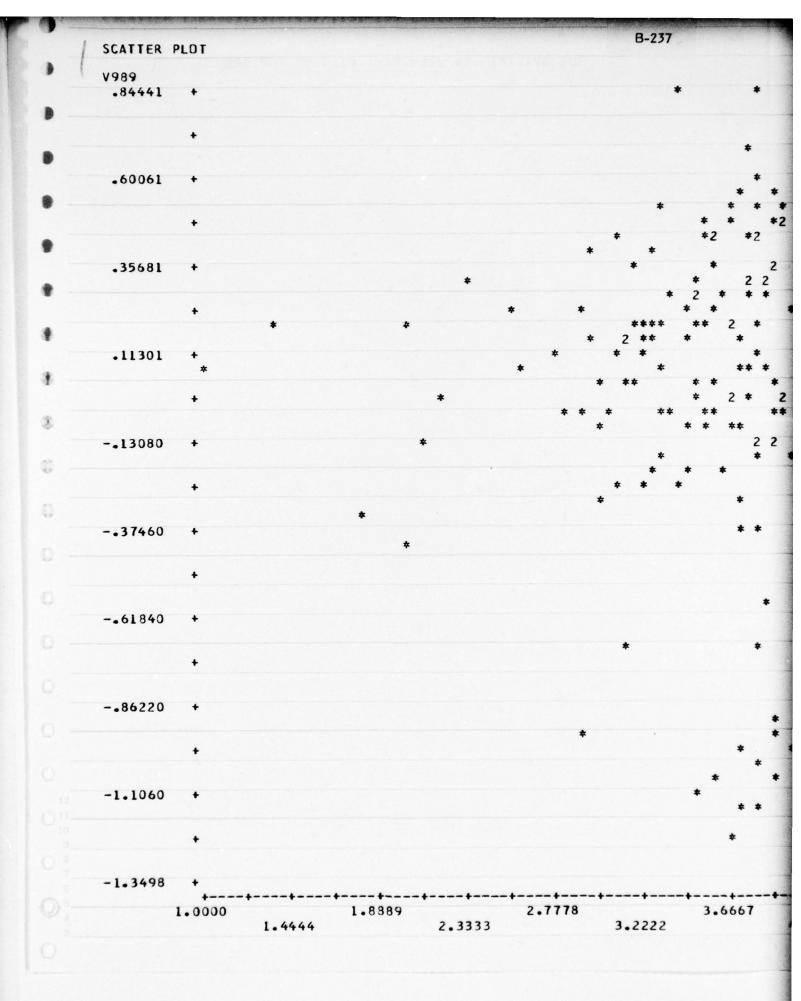






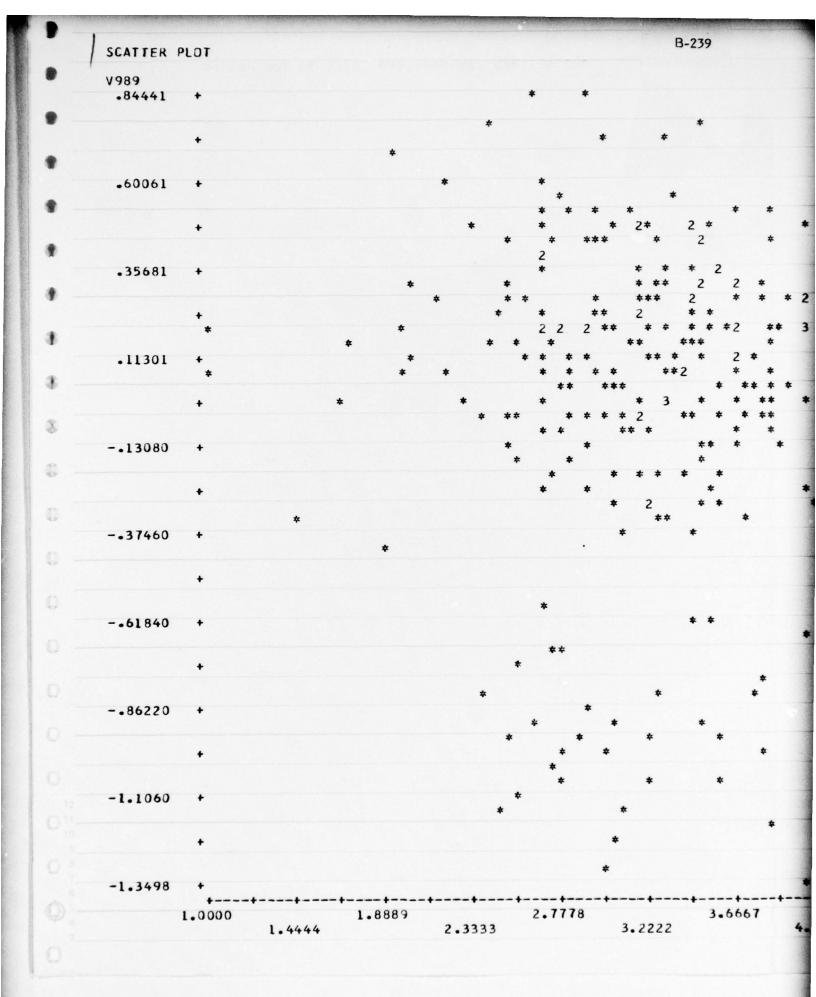


3.0322 3.7633 4.4944 200 SAT1 4.8600



3.6667 4.5556 176 SUP 3.2222 4.1111 5.0000

2.8722 3.7233 4.1489 5.0000



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| | SCATTER | PLOT | | | | | 6-241 | |
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| | | 1.0000 | 1 4444 | 1.8889 | 2.3333 | 2.7778 | 3.2222 | 3.6667 |
| | | | 1.4444 | | 2.3333 | | | |

-1.3498 + *
2.0000 2.6667 3.3333 4.0000
2.3333 3.0000 3.6667

3.6667

3.2222

+
-.86220 +
+
-1.1060 +

SCATTER PLOT

.84441 +

.60061 +

.35681

.11301

-.13080

-.37460

-.61840

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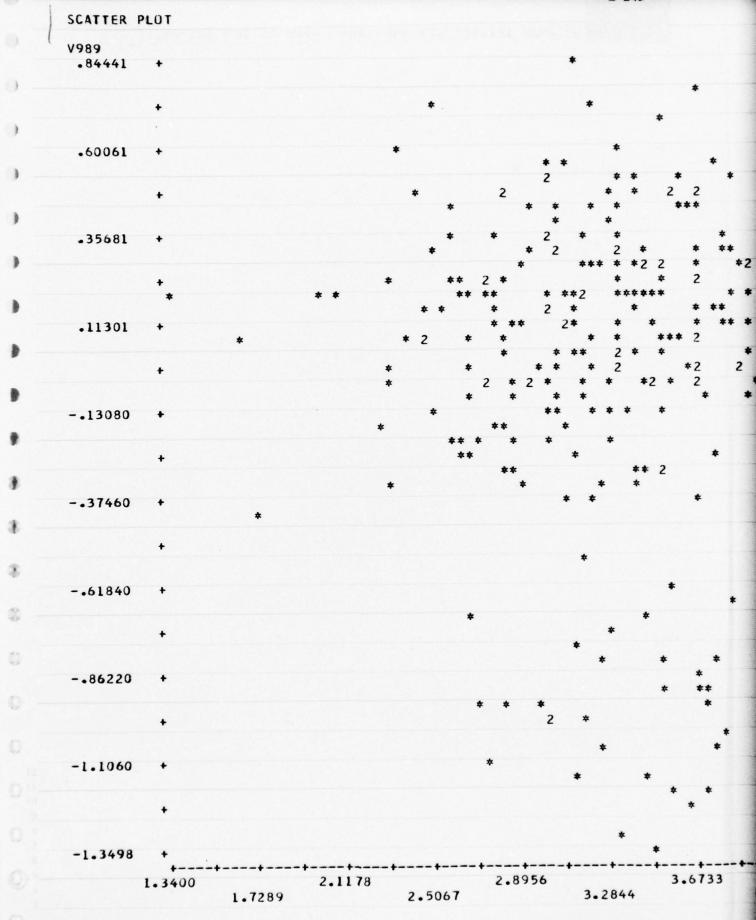
8

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V989

*

1.4444 2.3333



2.8378

3.4556

3.1467

4.0733

3.7644

3

-1.3498

2.2200

2.5289

3.4556 4.0733 4.3822 4.6911 198 MOTI 5.0000

| SCATTER | PLOT | | | | | B-249 | |
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| V989 | | | | | | | |
| .84441 | + | | | | | | |
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| 13080 | + | | | | | * * | 2 |
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| | + | | | | | ** | * |
| | | | | | | _ | 2 |
| 37460 | + | | | | | * | |
| | | | | | * | | |
| | + | | | | | | |
| | | | | | | | |
| 61840 | + | | | | | | |
| | | | | | | | |
| | + | | | | | * | * |
| | | | | | | | • |
| 86220 | | | | | | | * * |
| 65220 | + | | | | | * | |
| | | | | | | * | 2 * |
| | • | | | | | * * | * |
| | | | | | | | |
| -1.1060 | + | | | | | * | * |
| | | | | | | | |
| | + | | | | | | |
| | | | | | | | * |
| -1.3498 | + | | | | | | |
| | 1.5700 | | 2.3011 | + | 3.0322 | + | 3. |
| | | 1.9356 | | 2.6667 | | 3.3978 | |
| | | | | | | | |

APPENDIX C

HISTOGRAM OF RESIDUAL VALUES FOR
TVE PERIODS A-I AND ABS PERIODS A-J.

| HISTOGRAM | | TVE | PERIOD A | | | C-2 | |
|-----------|-------|-------|---------------|-----------|----------|--------------------|---|
| MIDPOINT | HISTS | COUNT | FOR 941.V941 | (EACH X | = 1) | | |
| -1.2412 | .5 | 1 | +X | | | | |
| 99121 | 1.6 | 3 | +XXX | | | | |
| 74121 | 6.4 | 12 | +XXXXXXXXXXXX | | | | |
| 49121 | 13.3 | 25 | +XXXXXXXXXXXX | XXXXXXXXX | XXXX | | |
| 24121 | 23.4 | 44 | +XXXXXXXXXXXX | XXXXXXXXX | XXXXXXXX | XXXXXXXXXXXXX | |
| .87933 -2 | 25.5 | 48 | +XXXXXXXXXXXX | XXXXXXXX | XXXXXXXX | XXXXXXXXXXXXXXXXXX | X |
| .25879 | 12.2 | 23 | +XXXXXXXXXXXX | XXXXXXXX | XX | | |
| .50879 | 9.6 | 18 | +XXXXXXXXXXXX | XXXXXX | | | |
| .75879 | 2.1 | 4 | +XXXX | | | | |
| 1.0088 | 1.6 | 3 | +XXX | | | | |
| 1.2588 | 1.1 | 2 | +XX | | | | |
| 1.5088 | .5 | 1 | +X | | | | |
| 1.7588 | 0. | 0 | + | | | | |
| 2.0088 | 0. | 0 | + | | | | |
| 2.2588 | .5 | 1 | +X | | | | |
| 2.5088 | 1.1 | 2 | +XX | | | | |
| 2.7588 | •5 | 1 | +X | | | | |
| MISSING | | 2131 | | | | | |
| TOTAL | | 2319 | (INTERVAL WI | DTH= .250 | 1001 | | |

| HISTOGRAM | | | _ _ _ | 000 | C-3 |
|-----------|-------|-------|-----------|------------|--|
| MIDPOINT | HIST% | COUNT | FOR | 942.V942 | (EACH X= 1) |
| -1.0830 | .8 | 1 | +X | | |
| 83301 | 1.6 | 2 | +XX | | |
| 58301 | 3.9 | 5 | +XXX | XX | |
| 33301 | 22.0 | 28 | +XXX | XXXXXXXXX | XXXXXXXXXXXXX |
| 83015 -1 | | 56 | +XXX | XXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| .16699 | 17.3 | 22 | +XXX | XXXXXXXXX | XXXXXXXX |
| .41699 | 5.5 | 7 | +XXX | XXXX | |
| .66699 | 0. | 0 | + | | |
| .91699 | 1.6 | 2 | +XX | | |
| 1.1670 | 0. | 0 | + | | |
| 1.4170 | 0. | 0 | + | | |
| 1.6670 | 0. | 0 | + | | |
| 1.9170 | 0. | 0 | + | | |
| 2.1670 | 0. | 0 | + | | |
| 2.4170 | . 8 | 1 | +X | | |
| 2.6670 | 0. | 0 | + | | |
| 2.9170 | 1.6 | 2 | +XX | | |
| 3.1670 | . 8 | 1 | +X | | |
| MISSING | | 2192 | | | |
| TOTAL | | 2319 | (IN | TERVAL WIE | OTH= .25000) |
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| - | HISTOGRAM | | IVE | FLITT | DC . | C-4 |
|---|-----------|-------|-------|-------|------------|--|
| - | MIDPOINT | HIST% | COUNT | FOR | 943.4943 | (EACH X= 1) |
| | -1.7102 | .2 | 1 | +X | | |
| | -1.4602 | 0. | 0 | + | | |
| | -1.2102 | .7 | 3 | +XXX | | |
| | 96021 | 3.2 | 14 | +XXXX | XXXXXXXXXX | X |
| | 71021 | 13.1 | 58 | +XXX | XXXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | 46021 | 16.7 | 74 | +XXX | XXXXXXXXX | ************************************** |
| | 21021 | 18.1 | 80 | +XXX | XXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | -39789 -1 | 13.3 | 59 | +XXX | XXXXXXXXXX | xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx |
| | .28979 | 10.9 | 48 | +XXX | XXXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| | •53979 | 9.3 | 41 | +XXX | XXXXXXXXX | ***** |
| | .78979 | 5.0 | 22 | +XXX | XXXXXXXXX | XXXXXXXX |
| | 1.0398 | 3.2 | 14 | +XXX | XXXXXXXXXX | X |
| | 1.2898 | 2.9 | 13 | + XXX | XXXXXXXXX | |
| | 1.5398 | 2.5 | 11 | +XXX | XXXXXXX | |
| | 1.7898 | .7 | 3 | +XXX | | |
| | 2.0398 | • 2 | 1 | +X | | |
| | MISSING | | 1877 | | | |
| | TOTAL | | 2319 | (IN | TERVAL WID | TH= .25000) |

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| HISTUGRAM | | | | | | | C-) | | |
|-----------|-------|-------|------|------------|---------|----------------|-------------|----------|--|
| MIDPOINT | HIST% | COUNT | FOR | 944.V944 | (EACH | X= 1) | | | |
| -2.2612 | .2 | 1 | +X | | | | | | |
| -2.0112 | .4 | 2 | +XX | | | | | | |
| -1.7612 | 1.2 | 6 | +XXX | XXX | | | | | |
| -1.5112 | 2.6 | 13 | +XXX | XXXXXXXXXX | (| | | | |
| -1.2612 | 2.0 | 10 | +XXX | XXXXXX | | | | | |
| -1.0112 | 8.1 | 41 | +XXX | XXXXXXXXXX | XXXXXXX | XXXXXX | XXXXXXXXXX | XXXX | |
| 76123 | 12.1 | 61 | +XXX | XXXXXXXXX | XXXXXX | XXXXXX | XXXXXXXXXXX | XXXXXXXX | (XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 51123 | 10.9 | 55 | +XXX | XXXXXXXXX | XXXXXX | XXXXXX | XXXXXXXXXXX | XXXXXXXX | XXXXXXXXX |
| 26123 | 15.2 | 77 | +XXX | XXXXXXXXXX | XXXXXX | XXXXXXX | XXXXXXXXXX | XXXXXXX | (XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 11226 -1 | 13.5 | 68 | +XXX | XXXXXXXXX | XXXXXX | XXXXXXX | XXXXXXXXXX | XXXXXXXX | (XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| .23877 | 8.3 | 42 | +XXX | XXXXXXXXX | XXXXXX | XXXXXX | XXXXXXXXXXX | XXXXX | |
| .48877 | 4.2 | 21 | +XXX | XXXXXXXXX | XXXXXX | XX | | | |
| .73877 | 3.2 | 16 | +XXX | XXXXXXXXX | XXXX | | | | |
| .98877 | 2.4 | 12 | +XXX | XXXXXXXX | | | | | |
| 1.2388 | 4.2 | 21 | +XXX | XXXXXXXXX | XXXXXX | XX | | | |
| 1.4888 | 2.8 | 14 | +XXX | XXXXXXXXX | (X | | | | |
| 1.7388 | 2.6 | 13 | +XXX | XXXXXXXXXX | K | | | | |
| 1.9888 | 1.4 | 7 | +XXX | XXXX | | | | | |
| 2.2388 | 2.4 | 12 | +XXX | XXXXXXXX | | | | | |
| 2.4888 | 2.0 | 10 | +XXX | XXXXXX | | | | | |
| 2.7388 | .4 | 2 | +XX | | | | | | |
| 2.9888 | • 2 | 1 | +X | | | | | | |
| MISSING | | 1814 | | | | | | | |
| TOTAL | | 2319 | (IN | TERVAL WIE | OTH= .2 | 5000) | | | |

XXXXXX ******** XXXXXXXXXXXXXXXXXX XXXXXXX

| - | MISTOOKAN | | | | | | | | | | | | |
|---|-----------|-------|-------|------|-------------------|----------|----------|----------|---------|-------|-------|--------|-------------------------|
| | MIDPOINT | HIST% | COUNT | FOR | 945. 1945 | (EACH | x= 1 | 1) | | | | | |
| | -2.0255 | .7 | 3 | +XXX | | | | | | | | | |
| | -1.7755 | .5 | 2 | +XX | | | | | | | | | |
| | -1.5255 | .2 | 1 | +X | | | | | | | | | |
| | -1.2755 | 1.6 | 7 | +XXX | XXXX | | | | | | | | |
| | -1.0255 | 7.0 | 31 | +XXX | XXXXXXXXX | (XXXXXX | XXXXX | XXXXXXX | | | | | |
| | 77547 | 12.4 | 55 | +XXX | XXXXXXXXX | (XXXXXX | KXXXX | (XXXXXXX | XXXXXXX | XXXXX | XXXXX | XXXXXX | X |
| | 52547 | 17.6 | 78 | +XXX | XXXXXXXXX | (XXXXXXX | XXXXX | XXXXXXX | XXXXXXX | XXXXX | XXXXX | XXXXXX | XX |
| | 27547 | 15.8 | 70 | +XXX | XXXXXXXXX | XXXXXXX | XXXXX | (XXXXXXX | XXXXXX | XXXXX | XXXXX | XXXXXX | XX |
| | 25467 -1 | 13.6 | 60 | +XXX | XXXXXXXXXX | (XXXXXX | KXXXX | (XXXXXXX | XXXXXXX | XXXXX | XXXXX | XXXXXX | X |
| | .22453 | 7.0 | 31 | +XXX | XXXXXXXXX | XXXXXXX | XXXXX | XXXXXXX | | | | | |
| | .47453 | 2.5 | 11 | +XXX | XXXXXXX | | | | | | | | |
| | •72453 | 2.7 | 12 | +XXX | XXXXXXXX | | | | | | | | |
| | .97453 | 1.8 | 8 | +XXX | XXXXX | | | | | | | | |
| | 1.2245 | 3.6 | 16 | +XXX | XXXXXXXXXX | (XXX | | | | | | | |
| | 1.4745 | 4.5 | 20 | +XXX | x x x x x x x x x | (XXXXXX | K | | | | | | |
| | 1.7245 | 2.7 | 12 | +XXX | XXXXXXXX | | | | | | | | |
| | 1.9745 | .9 | 4 | +XXX | X | | | | | | | | |
| | 2.2245 | 1.8 | 8 | +XXX | XXXXX | | | | | | | | |
| | 2.4745 | 1.8 | 8 | +XXX | XXXXX | | | | | | | | |
| | 2.7245 | .9 | - | +XXX | X | | | | | | | | |
| | 2.9745 | • 2 | 1 | +X | | | | | | | | | Selection of the second |
| | MISSING | | 1877 | | | | | | | | | | Sec. |
| | TOTAL | | 2319 | (IN | TERVAL WI | OTH= .2! | 5000) | | | | | | The state of |
| | | | | | | | | | | | | | |

| HISTOGRAM | | TVE | PERIO | DD F | | | C |
|-----------|-------|-------|-------|-------------|---------|-------|--------|
| | | | | | | | |
| MIDPOINT | HISTS | COUNT | FOR | 946. 4946 | (EACH | x= 1) | |
| -1.7586 | .5 | , | +X | | | | |
| -1.5086 | 1.0 | _ | +XX | | | | |
| -1.2586 | 4.0 | | | CXXXX | | | |
| -1.0086 | 5.6 | | | XXXXXXX | | | |
| 75856 | 10.1 | | | XXXXXXXXXX | | | |
| 50856 | 9.6 | | | (XXXXXXXXXX | | | |
| | | - | | XXXXXXXXX | | vvvv | |
| 25856 | 12.1 | | | | | | VVVVVV |
| 85557 -2 | | | | XXXXXXXXX | | | |
| -24144 | 14.6 | | | XXXXXXXXX | | | XXX |
| .49144 | 11.6 | | | XXXXXXXXX | XXXXXXX | XXX | |
| .74144 | 6.1 | 12 | +XXXX | XXXXXXXX | | | |
| .99144 | 1.5 | 3 | +XXX | | | | |
| 1.2414 | 1.5 | 3 | +XXX | | | | |
| 1.4914 | .5 | 1 | +X | | | | |
| 1.7414 | 1.0 | 2 | +XX | | | | |
| 1.9914 | 1.0 | 2 | +XX | | | | |
| 2.2414 | .5 | 1 | +X | | | | |
| 2.4914 | .5 | 1 | + X | | | | |
| 2.7414 | 0. | 0 | + | | | | |
| 2.9914 | 0. | 0 | + | | | | |
| 3.2414 | 1.0 | 2 | +XX | | | | |
| 3.4914 | .5 | | +X | | | | |
| 201721 | | | , | | | | |
| MISSING | | 2121 | | | | | |
| TOTAL | | 2319 | LIN | TERVAL WIG | TH= .25 | 0001 | |
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| HISTOGRAM | | 1 | /E PER | ח טטנו | | | | |
|-----------|-------|-------|--------|----------|--------|-----|------|----|
| MIDPOINT | HIST% | COUNT | FOR | 948.V | 948 (E | ACH | X= | 1) |
| -1.0402 | 4.4 | 2 | +XX | | | | | |
| 79020 | 0. | 0 | + | | | | | |
| 54020 | 8.9 | 4 | +XXXX | (| | | | |
| 29020 | 15.6 | 7 | +XXX | XXXX | | | | |
| 40200 -1 | 28.9 | 13 | +XXX | XXXXXX | XXXX | | | |
| -20980 | 31.1 | 14 | +XXX | XXXXXX | XXXXX | | | |
| .45980 | 4.4 | 2 | +XX | | | | | |
| .70980 | 2.2 | 1 | +X | | | | | |
| .95980 | 2.2 | 1 | +X | | | | | |
| 1.2098 | 2.2 | 1 | + X | | | | | |
| MISSING | | 2274 | | | | | | |
| TOTAL | | 2319 | (IN | TERVAL | WIDTH= | . 2 | 5000 |)) |
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| HISTUGRAM | | | VE PERIOD I | |
|-----------|---|---|--|--|
| MIDPOINT | HIST & | COUNT | FOR 949. V949 (EACH | X= 1) |
| -1.5805 | .2 | 1 | +X | |
| -1.3305 | .7 | 3 | +XXX | |
| -1.0805 | 5.9 | 24 | +XXXXXXXXXXXXXXXXXXX | XXXXX |
| 83051 | 10.3 | 42 | +XXXXXXXXXXXXXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXX |
| 58051 | 8.3 | 34 | +XXXXXXXXXXXXXXXXXXXX | XXXXXXXXXXXXX |
| 33051 | 13.0 | 53 | +XXXXXXXXXXXXXXXXXXX | ********** |
| 80511 -1 | 21.5 | 88 | +XXXXXXXXXXXXXXXXXXXX | ******** |
| .16949 | 16.9 | 69 | +XXXXXXXXXXXXXXXXXXX | XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| .41949 | 5.9 | 24 | +XXXXXXXXXXXXXXXXXXX | XXXXX |
| .66949 | 3.2 | 13 | +XXXXXXXXXXXX | |
| -91949 | | | | |
| | | | | |
| | | | | xxxxxxx |
| 1.6695 | 2.7 | | | |
| MISSING | | 1910 | | |
| TOTAL | | 2319 | (INTERVAL WIDTH= .2 | 5000) |
| | MIDPOINT -1.5805 -1.3305 -1.08058305158051330518051116949 .41949 .66949 .91949 1.1695 1.4195 1.6695 MISSING | MIDPOINT HIST% -1.5805 .2 -1.3305 .7 -1.0805 .5.983051 10.358051 8.333051 13.080511 -1 21.5 .16949 16.9 .41949 5.9 .66949 3.2 .91949 1.0 1.1695 3.9 1.4195 6.6 1.6695 2.7 MISSING | MIDPOINT HIST% COUNT -1.5805 .2 1 -1.3305 .7 3 -1.0805 5.9 2483051 10.3 4258051 8.3 3433051 13.0 5380511 -1 21.5 88 .16949 16.9 69 .41949 5.9 24 .66949 3.2 13 .91949 1.0 4 1.1695 3.9 16 1.4195 6.6 27 1.6695 2.7 11 MISSING 1910 | MIDPOINT HIST% COUNT FOR 949.V949 (EACH -1.5805 |

| HISTOGRAM | | AB | S PER | IOD A | | C-1 |
|-----------|-------|------|-------|------------|-------------|-----------|
| MIDPOINT | HIST% | COUN | T FOR | 980. V980 | (EACH X= 1) | |
| -2 1422 | | | | | | |
| -2.1432 | 1.2 | | +XXX | | | |
| -1.8932 | . 8 | | +XX | | | |
| -1.6432 | 4.3 | | | XXXXXXX | | |
| -1.3932 | 2.4 | | +XXX | 100000 | | |
| -1.1432 | 5.9 | 15 | + XXX | XXXXXXXXXX | XX | |
| 89323 | 5.9 | 15 | + XXX | xxxxxxxxx | XX | |
| 64323 | 8.3 | 21 | +XXX | XXXXXXXXX | XXXXXXXX | |
| 39323 | 8.7 | 22 | +XXX | XXXXXXXXX | XXXXXXXXX | |
| 14323 | 13.0 | 33 | +XXX | XXXXXXXXX | XXXXXXXXXXX | XXXXXXX |
| .10677 | 13.8 | 35 | +XXX | XXXXXXXXX | XXXXXXXXXXX | XXXXXXXXX |
| .35677 | 9.1 | 23 | +XXX | XXXXXXXXX | XXXXXXXXX | |
| -60677 | 8.3 | 21 | +XXX | xxxxxxxxx | XXXXXXX | |
| .85677 | 5.9 | 15 | +XXX | XXXXXXXXX | XX ' | |
| 1.1068 | . 4 | 1 | +X | | | |
| 1.3568 | 3.1 | 8 | +XXX | XXXXX | | |
| 1.6068 | 3.1 | 8 | +XXX | XXXXX | | |
| 1.8568 | 2.0 | 5 | +XXX | XX | | |
| 2.1068 | 2.4 | 6 | +XXX | XXX | | |
| 2.3568 | . 8 | 2 | +XX | | | |
| 2.6068 | . 8 | | +XX | | | |
| | | | | | | |
| MISSING | | 2065 | | | | |
| TOTAL | | 2319 | (IN | TERVAL WID | TH= .25000) | |

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(INTERVAL WIDTH= .25000)

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| HISTOGRAM | | 1 | ABS PE | RIOD C | | | | C-13 | | | |
|-----------|-------|-------|--------|-------------|----------|------|-------|---------|---------|---------|---------|
| MIDPOINT | HISTE | COUNT | FOR | 982.V982 | (EACH | X= | 1) | | | | |
| -1.9098 | .7 | 3 | +XXX | | | | | | | | |
| -1.6598 | 2.5 | 11 | +XXXX | XXXXXXX | | | | | | | |
| -1.4098 | 3.7 | 16 | +XXXX | XXXXXXXXX | CXXX | | | | | | |
| -1.1598 | 1.2 | 5 | +XXXX | (X | | | | | | | |
| 90983 | 1.6 | 7 | +XXXX | XXXX | | | | | | | |
| 65983 | 7.4 | 32 | + XXXX | XXXXXXXXX | XXXXXXX | XXXX | XXXXX | XXXX | | | |
| 40983 | 17.3 | 75 | +XXXX | (XXXXXXXXX | (XXXXXX | XXXX | XXXXX | XXXXXXX | XXXXXX | (XXXXXX | XXXXXXX |
| 15983 | 18.4 | 80 | +XXXX | XXXXX XXXXX | XXXXXXX | XXXX | XXXXX | XXXXXXX | XXXXXX | CXXXXXX | XXXXXX |
| .90166 -1 | 13.6 | 59 | +XXX | XXXXXXXXX | XXXXXXX | XXXX | XXXXX | XXXXXXX | (XXXXXX | XXXXXX | XXXXXX |
| .34017 | 11.5 | 50 | +XXXX | XXXXXXXXX | XXXXXXX | XXXX | XXXXX | XXXXXXX | XXXXXX | (XXXXXX | XX |
| .59017 | 6.0 | 26 | + XXXX | XXXXXXXXX | (XXXXXXX | XXXX | XXX | | | | |
| .84017 | 6.2 | 27 | +XXXX | XXXXXXXXX | XXXXXX | XXXX | XXXX | | | | |
| 1.0902 | 3.9 | 17 | +XXXX | XXXXXXXXX | XXXXX | | | | | | |
| 1.3402 | 3.0 | 13 | +XXXX | XXXXXXXXX | (| | | | | | |
| 1.5902 | 1.2 | 5 | +XXXX | ΚX | | | | | | | |
| 1.8402 | .5 | 2 | +XX | | | | | | | | |
| 2.0902 | .5 | 2 | +XX | | | | | | | | |
| 2.3402 | 0. | 0 | + | | | | | | | | |
| 2.5902 | 0. | 0 | + | | | | | | | | |
| 2.8402 | . 9 | 4 | +XXXX | K | | | | | | | |
| MISSING | | 1885 | | | | | | | | | |
| TOTAL | | 2319 | IIN | TERVAL WID | OTH= .25 | 5000 |) | | | | |

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(INTERVAL WIDTH= .25000)

| | | 400 | S PERIOD F C-15 |
|-----------|--------|-------|---|
| HISTOGRAM | | ABS | S PERIOD E |
| | | | |
| MIDPOINT | HIST & | COUNT | T FOR 984.V984 (EACH X= 1) |
| | | | |
| -2.0384 | 1.2 | - | +XXXXX |
| -1.7884 | 1.6 | 7 | +XXXXXXX |
| -1.5384 | 7.6 | 33 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| -1.2884 | 5.1 | 22 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| -1.0384 | 7.6 | 33 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 78839 | 7.6 | 33 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 53839 | 5.8 | 25 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 28839 | 4.4 | 19 | +XXXXXXXXXXXXXXXXXX |
| 38389 -1 | 6.7 | 29 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| .21161 | 10.1 | 44 | +xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx |
| -46161 | 11.3 | 49 | +xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx |
| .71161 | 11.5 | 50 | +xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx |
| .96161 | 8.8 | 38 | +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX |
| 1.2116 | 3.7 | 16 | +XXXXXXXXXXXXXXX |
| 1.4616 | 3.5 | 15 | +XXXXXXXXXXXXXX |
| 1.7116 | 1.2 | 5 | ÷XXXXX |
| 1.9616 | .7 | 3 | +XXX |
| 2.2116 | .5 | 2 | +XX |
| 2.4616 | . 2 | 1 | +X |
| 2.7116 | .9 | 4 | +XXXX |
| 2.9616 | .2 | 1 | +X |
| MISSING | | 1885 | |
| TOTAL | | 2319 | (INTERVAL WIDTH= .25000) |

| | | | | | _ | _ | | | | |
|-----------|-------|------|-----------|--------|----------|--------|--------|---------|---------|------------|
| HISTOGRAM | | ABS | PERIOD F | | | | | | | |
| MIDPOINT | HIST% | COUN | T FOR 985 | ·V985 | (EACH | X= 1) | | | | |
| -1.6329 | .6 | 2 | +XX | | | | | | | |
| -1.3829 | .6 | 2 | +XX | | | | | | | |
| -1.1329 | 5.1 | 18 | +XXXXXXX | XXXXXX | XXXXX | | | | | |
| 88288 | 8.3 | 29 | +XXXXXXX | XXXXXX | (XXXXXXX | XXXXXX | XXXX | | | |
| 63288 | 10.3 | 36 | +XXXXXXX | XXXXXX | (XXXXXX | (XXXXX | XXXXXX | XXXXX | | |
| 38288 | 10.5 | 37 | +XXXXXXX | XXXXXX | (XXXXXX) | XXXXXX | XXXXXX | XXXXXX | | |
| 13288 | 15.4 | 54 | +XXXXXXX | XXXXXX | (XXXXXXX | XXXXXX | XXXXXX | XXXXXXX | XXXXXX | XXXXXXXXXX |
| .11712 | 13.4 | 47 | +XXXXXXX | XXXXXX | (XXXXXXX | XXXXXX | XXXXXX | XXXXXX | (XXXXX) | CXXX |
| .36712 | 12.0 | 42 | + XXXXXXX | XXXXXX | (XXXXXX) | XXXXXX | XXXXXX | XXXXXXX | XXXX | |
| .61712 | 15.4 | 54 | +XXXXXXX | XXXXXX | (XXXXXXX | XXXXXX | XXXXXX | XXXXXXX | XXXXXX | XXXXXXXXXX |
| .86712 | 4.6 | 16 | +XXXXXXX | XXXXXX | XXX | | | | | |
| 1.1171 | . 9 | 3 | +XXX | | | | | | | |
| 1.3671 | .3 | 1 | +X | | | | | | | |
| 1.6171 | .3 | 1 | +X | | | | | | | |
| 1.8671 | 0. | 0 | + | | | | | | | |
| 2.1171 | .9 | 3 | +XXX | | | | | | | |
| 2.3671 | .9 | 3 | +XXX | | | | | | | |
| 2.6171 | . 9 | 3 | +XXX | | | | | | | |
| | | | | | | | | | | |
| MISSING | | 1968 | | | | | | | | |
| TOTAL | | 2319 | (INTERV | AL WID | TH= .25 | 0000) | | | | |
| | | | | | | | | | | |

| HISTOGRAM | | A | D3 PER | NOD G | | | | |
|-----------|-------|-------|--------|------------|----------|------|--------------|-------|
| MIDPOINT | HISTS | COUNT | FOR | 986.V986 | (EACH | X= | 1) | |
| -1.7387 | .6 | 2 | +XX | | | | | |
| -1.4887 | 3.0 | 10 | +XXX | XXXXXXX | | | | |
| -1.2387 | 4.5 | 15 | +XXX | XXXXXXXXX | (XX | | | |
| 98869 | 6.3 | 21 | +XXX | XXXXXXXXX | (XXXXXXX | XX | | |
| 73869 | 11.9 | 40 | +XXX | XXXXXXXXX | (XXXXXX | XXXX | XXXXXXXXXXXX | XXXX |
| 48869 | 12.2 | 41 | +XXX | XXXXXXXXX | XXXXXXX | XXXX | XXXXXXXXXXXX | XXXXX |
| 23869 | 11.6 | 39 | +XXX | XXXXXXXXX | (XXXXXX | XXX | XXXXXXXXXXXX | XXX |
| .11305 -1 | 7.7 | 26 | +XXX | XXXXXXXXX | (XXXXXX | XXXX | XXX | |
| .26131 | 7.1 | 24 | +XXX | XXXXXXXXX | (XXXXXXX | XXXX | X | |
| .51131 | 7.1 | 24 | +XXX | XXXXXXXXX | XXXXXXX | XXXX | X | |
| .76131 | 11.6 | 39 | +XXX | XXXXXXXXX | (XXXXXX | XXXX | XXXXXXXXXXXX | XXX |
| 1.0113 | 8.3 | 28 | +XXX | XXXXXXXXX | XXXXXXX | XXXX | XXXXX | |
| 1.2613 | 4.8 | 16 | +XXX | XXXXXXXXX | XXX | | | |
| 1.5113 | 1.5 | 5 | +XXXX | XX | | | | |
| 1.7613 | 1.8 | 6 | +XXX | XXX | | | | |
| MISSING | | 1983 | | | | | | |
| TOTAL | | 2319 | (IN | TERVAL WIE | TH= .25 | 5000 | 1) | |
| | | | | | | | | |

TOTAL

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2319 (INTERVAL WIDTH= .25000)

(INTERVAL WIDTH= .25000)

TOTAL

| HISTOGRAM | | - | IBS PEI | KIOD I | | | | | -17 | |
|-----------|-------|-------|---------|---------|------|---------|--------|-------|--------|-------|
| MIDPOINT | HISTE | COUNT | r FOR | 988.V | 988 | (EACH | X= 1) | | | |
| -1.6259 | .8 | 2 | +XX | | | | | | | |
| -1.3759 | .4 | 1 | +X | | | | | | | |
| -1.1259 | 3.0 | 8 | +XXXX | XXXX | | | | | | |
| 87593 | 6.0 | 16 | +XXXX | (XXXXX) | XXXX | XXX | | | | |
| 62593 | 13.9 | 37 | +XXXX | (XXXXX) | XXXX | XXXXXX | XXXXX | XXXXX | XXXXXX | K |
| 37593 | 15.4 | 41 | +XXXX | CXXXXX | XXXX | XXXXXX | XXXXX | XXXXX | XXXXXX | XXXXX |
| 12593 | 15.4 | 41 | +XXXX | (XXXXX) | XXXX | XXXXXX | XXXXX | XXXXX | XXXXXX | XXXXX |
| -12407 | 13.5 | 36 | +XXXX | XXXXXX | XXXX | XXXXXX | XXXXXX | XXXXX | XXXXXX | |
| -37407 | 8.3 | 22 | +XXXX | XXXXXX | XXXX | XXXXXX | (XX | | | |
| .62407 | 7.1 | 19 | +XXXX | XXXXXX | XXXX | XXXXXX | | | | |
| .87407 | 6.4 | 17 | +XXX | XXXXXX | XXXX | XXXX | | | | |
| 1.1241 | 4.9 | 13 | +XXXX | XXXXXX | XXXX | | | | | |
| 1.3741 | 3.8 | 10 | +XXXX | XXXXXX | X | | | | | |
| 1.6241 | 1.1 | 3 | +XXX | | | | | | | |
| MISSING | | 2053 | | | | | | | | |
| TOTAL | | 2319 | (IN | TERVAL | WID | TH= .25 | 5000) | | | |
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(INTERVAL WIDTH= .25000)

2319

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